

FACTORS FOR UNIT CONVERSIONS

| Quantity | Equivalent Values |
|-----------------|--|
| Mass | $1 \text{ kg} = 1000 \text{ g} = 0.001 \text{ metric ton} = 2.20462 \text{ lb}_m = 35.27392 \text{ oz}$ $1 \text{ lb}_m = 16 \text{ oz} = 5 \times 10^{-4} \text{ ton} = 453.593 \text{ g} = 0.453593 \text{ kg}$ |
| Length | $1 \text{ m} = 100 \text{ cm} = 1000 \text{ mm} = 10^6 \text{ microns } (\mu\text{m}) = 10^{10} \text{ angstroms } (\text{\AA})$ $= 39.3701 \text{ in} = 3.28084 \text{ ft} = 1.09361 \text{ yd} = 0.000621371 \text{ mile}$ $1 \text{ ft} = 12 \text{ in.} = 1/3 \text{ yd} = 0.3048 \text{ m} = 30.48 \text{ cm}$ |
| Volume | $1 \text{ m}^3 = 1000 \text{ liters} = 10^6 \text{ cm}^3 = 10^6 \text{ ml}$ $= 35.31467 \text{ ft}^3 = 219.969 \text{ imperial gallons} = 264.172 \text{ gal}$ $= 1056.69 \text{ qt}$ $1 \text{ ft}^3 = 1728 \text{ in}^3 = 7.48052 \text{ gal} = 0.028317 \text{ m}^3 = 28.3168 \text{ liters}$ $= 28,316.8 \text{ cm}^3$ |
| Force | $1 \text{ N} = 1 \text{ kg}\cdot\text{m}/\text{s}^2 = 10^5 \text{ dynes} = 10^5 \text{ g}\cdot\text{cm}/\text{s}^2 = 0.22481 \text{ lb}_f$ $1 \text{ lb}_f = 32.174 \text{ lb}_m\cdot\text{ft}/\text{s}^2 = 4.4482 \text{ N} = 4.4482 \times 10^5 \text{ dynes}$ |
| Pressure | $1 \text{ atm} = 1.01325 \times 10^5 \text{ N}/\text{m}^2 \text{ (Pa)} = 101.325 \text{ kPa} = 1.01325 \text{ bars}$ $= 1.01325 \times 10^6 \text{ dynes}/\text{cm}^2$ $= 760 \text{ mm Hg at } 0^\circ \text{ C (torr)} = 10.333 \text{ m H}_2\text{O at } 4^\circ \text{ C}$ $= 14.696 \text{ lb}_f/\text{in}^2 \text{ (psi)} = 33.9 \text{ ft H}_2\text{O at } 4^\circ \text{ C}$ $100 \text{ kPa} = 1 \text{ bar}$ |
| Energy | $1 \text{ J} = 1 \text{ N}\cdot\text{m} = 10^7 \text{ ergs} = 10^7 \text{ dyne}\cdot\text{cm}$ $= 2.778 \times 10^{-7} \text{ kW}\cdot\text{h} = 0.23901 \text{ cal}$ $= 0.7376 \text{ ft}\cdot\text{lb}_f = 9.47817 \times 10^{-4} \text{ Btu}$ |
| Power | $1 \text{ W} = 1 \text{ J}/\text{s} = 0.23885 \text{ cal}/\text{s} = 0.7376 \text{ ft}\cdot\text{lb}_f/\text{s} = 9.47817 \times 10^{-4} \text{ Btu}/\text{s} = 3.4121 \text{ Btu}/\text{h}$ $= 1.341 \times 10^{-3} \text{ hp (horsepower)}$ |
| Viscosity | $1 \text{ Pa}\cdot\text{s} = 1 \text{ N}\cdot\text{s}/\text{m}^2 = 1 \text{ kg}/\text{m}\cdot\text{s}$ $= 10 \text{ poise} = 10 \text{ dynes}\cdot\text{s}/\text{cm}^2 = 10 \text{ g}/\text{cm}\cdot\text{s}$ $= 10^3 \text{ cp (centipoise)}$ $= 0.67197 \text{ lb}_m/\text{ft}\cdot\text{s} = 2419.088 \text{ lb}_m/\text{ft}\cdot\text{h}$ |
| Density | $1 \text{ kg}/\text{m}^3 = 10^{-3} \text{ g}/\text{cm}^3$ $= 0.06243 \text{ lb}_m/\text{ft}^3$ $10^3 \text{ kg}/\text{m}^3 = 1 \text{ g}/\text{cm}^3 = 62.428 \text{ lb}_m/\text{ft}^3$ |
| Volumetric Flow | $1 \text{ m}^3/\text{s} = 35.31467 \text{ ft}^3/\text{s} = 15,850.32 \text{ gal}/\text{min (gpm)}$ $1 \text{ gpm} = 6.30902 \times 10^{-5} \text{ m}^3/\text{s} = 2.228009 \times 10^{-3} \text{ ft}^3/\text{s} = 3.7854 \text{ liter}/\text{min}$ $1 \text{ liter}/\text{min} = 0.26417 \text{ gpm}$ |

| | |
|-------------------------------------|---|
| Temperature | $T(^{\circ}C) = \frac{5}{9}[T(^{\circ}F) - 32]$ $T(^{\circ}F) = \frac{9}{5}T(^{\circ}C) + 32 = 1.8T(^{\circ}C) + 32$ |
| Absolute Temperature | $T(K) = T(^{\circ}C) + 273.15$ $T(^{\circ}R) = T(^{\circ}F) + 459.67$ |
| Temperature Interval (ΔT) | $1 C^{\circ} = 1 K = 1.8 F^{\circ} = 1.8 R^{\circ}$ $1 F^{\circ} = 1 R^{\circ} = (5/9) C^{\circ} = (5/9) K$ |

USEFUL QUANTITIES

$$SG = \rho(20^{\circ}C) / \rho_{\text{water}}(4^{\circ}C)$$

$$\rho_{\text{water}}(4^{\circ}C) = 1000 \text{ kg/m}^3 = 62.43 \text{ lb}_m/\text{ft}^3 = 1.000 \text{ g/cm}^3$$

$$\rho_{\text{water}}(25^{\circ}C) = 997.08 \text{ kg/m}^3 = 62.25 \text{ lb}_m/\text{ft}^3 = 0.99709 \text{ g/cm}^3$$

$$g = 9.8066 \text{ m/s}^2 = 980.66 \text{ cm/s}^2 = 32.174 \text{ ft/s}^2$$

$$\mu_{\text{water}}(25^{\circ}C) = 8.937 \times 10^{-4} \text{ Pa}\cdot\text{s} = 8.937 \times 10^{-4} \text{ kg/m}\cdot\text{s}$$

$$= 0.8937 \text{ cp} = 0.8937 \times 10^{-2} \text{ g/cm}\cdot\text{s} = 6.005 \times 10^{-4} \text{ lb}_m/\text{ft}\cdot\text{s}$$

| | | |
|---------------------|---------------------------------|--------------|
| Composition of air: | N ₂ | 78.03% |
| | O ₂ | 20.99% |
| | Ar | 0.94% |
| | CO ₂ | 0.03% |
| | H ₂ , He, Ne, Kr, Xe | <u>0.01%</u> |
| | | 100.00% |

$$M_{\text{air}} = 29 \text{ g/mol} = 29 \text{ kg/kmol} = 29 \text{ lb}_m/\text{lbmole}$$

$$\hat{C}_{p,\text{water}}(25^{\circ}C) = 4.182 \text{ kJ/kg}\cdot\text{K} = 0.9989 \text{ cal/g}\cdot\text{C} = 0.9997 \text{ Btu/lb}_m\cdot\text{F}$$

$$R = 8.314 \text{ m}^3\cdot\text{Pa/mol}\cdot\text{K} = 0.08314 \text{ liter}\cdot\text{bar/mol}\cdot\text{K} = 0.08206 \text{ liter}\cdot\text{atm/mol}\cdot\text{K}$$

$$= 62.36 \text{ liter}\cdot\text{mm Hg/mol}\cdot\text{K} = 0.7302 \text{ ft}^3\cdot\text{atm/lbmole}\cdot\text{R}$$

$$= 10.73 \text{ ft}^3\cdot\text{psia/lbmole}\cdot\text{R}$$

$$= 8.314 \text{ J/mol}\cdot\text{K}$$

$$= 1.987 \text{ cal/mol}\cdot\text{K} = 1.987 \text{ Btu/lbmole}\cdot\text{R}$$

A.2-9 Properties of Saturated Steam and Water (Steam Table), SI Units

| Temperature (°C) | Vapor Pressure (kPa) | Specific Volume (m ³ /kg) | | Enthalpy (kJ/kg) | | Entropy (kJ/kg·K) | |
|---------------------|----------------------------|---|-------------|---------------------|-------------|----------------------|-------------|
| | | Liquid | Sat'd Vapor | Liquid | Sat'd Vapor | Liquid | Sat'd Vapor |
| 0.01 | 0.6113 | 0.0010002 | 206.136 | 0.00 | 2501.4 | 0.0000 | 9.1562 |
| 3 | 0.7577 | 0.0010001 | 168.132 | 12.57 | 2506.9 | 0.0457 | 9.0773 |
| 6 | 0.9349 | 0.0010001 | 137.734 | 25.20 | 2512.4 | 0.0912 | 9.0003 |
| 9 | 1.1477 | 0.0010003 | 113.386 | 37.80 | 2517.9 | 0.1362 | 8.9253 |
| 12 | 1.4022 | 0.0010005 | 93.784 | 50.41 | 2523.4 | 0.1806 | 8.8524 |
| 15 | 1.7051 | 0.0010009 | 77.926 | 62.99 | 2528.9 | 0.2245 | 8.7814 |
| 18 | 2.0640 | 0.0010014 | 65.038 | 75.58 | 2534.4 | 0.2679 | 8.7123 |
| 21 | 2.487 | 0.0010020 | 54.514 | 88.14 | 2539.9 | 0.3109 | 8.6450 |
| 24 | 2.985 | 0.0010027 | 45.883 | 100.70 | 2545.4 | 0.3534 | 8.5794 |
| 25 | 3.169 | 0.0010029 | 43.360 | 104.89 | 2547.2 | 0.3674 | 8.5580 |
| 27 | 3.567 | 0.0010035 | 38.774 | 113.25 | 2550.8 | 0.3954 | 8.5156 |
| 30 | 4.246 | 0.0010043 | 32.894 | 125.79 | 2556.3 | 0.4369 | 8.4533 |
| 33 | 5.034 | 0.0010053 | 28.011 | 138.33 | 2561.7 | 0.4781 | 8.3927 |
| 36 | 5.947 | 0.0010063 | 23.940 | 150.86 | 2567.1 | 0.5188 | 8.3336 |
| 40 | 7.384 | 0.0010078 | 19.523 | 167.57 | 2574.3 | 0.5725 | 8.2570 |
| 45 | 9.593 | 0.0010099 | 15.258 | 188.45 | 2583.2 | 0.6387 | 8.1648 |
| 50 | 12.349 | 0.0010121 | 12.032 | 209.33 | 2592.1 | 0.7038 | 8.0763 |
| 55 | 15.758 | 0.0010146 | 9.568 | 230.23 | 2600.9 | 0.7679 | 7.9913 |
| 60 | 19.940 | 0.0010172 | 7.671 | 251.13 | 2609.6 | 0.8312 | 7.9096 |
| 65 | 25.03 | 0.0010199 | 6.197 | 272.06 | 2618.3 | 0.8935 | 7.8310 |
| 70 | 31.19 | 0.0010228 | 5.042 | 292.98 | 2626.8 | 0.9549 | 7.7553 |
| 75 | 38.58 | 0.0010259 | 4.131 | 313.93 | 2635.3 | 1.0155 | 7.6824 |
| 80 | 47.39 | 0.0010291 | 3.407 | 334.91 | 2643.7 | 1.0753 | 7.6122 |
| 85 | 57.83 | 0.0010325 | 2.828 | 355.90 | 2651.9 | 1.1343 | 7.5445 |
| 90 | 70.14 | 0.0010360 | 2.361 | 376.92 | 2660.1 | 1.1925 | 7.4791 |
| 95 | 84.55 | 0.0010397 | 1.9819 | 397.96 | 2668.1 | 1.2500 | 7.4159 |
| 100 | 101.35 | 0.0010435 | 1.6729 | 419.04 | 2676.1 | 1.3069 | 7.3549 |
| 105 | 120.82 | 0.0010475 | 1.4194 | 440.15 | 2683.8 | 1.3630 | 7.2958 |
| 110 | 143.27 | 0.0010516 | 1.2102 | 461.30 | 2691.5 | 1.4185 | 7.2387 |
| 115 | 169.06 | 0.0010559 | 1.0366 | 482.48 | 2699.0 | 1.4734 | 7.1833 |
| 120 | 198.53 | 0.0010603 | 0.8919 | 503.71 | 2706.3 | 1.5276 | 7.1296 |
| 125 | 232.1 | 0.0010649 | 0.7706 | 524.99 | 2713.5 | 1.5813 | 7.0775 |
| 130 | 270.1 | 0.0010697 | 0.6685 | 546.31 | 2720.5 | 1.6344 | 7.0269 |
| 135 | 313.0 | 0.0010746 | 0.5822 | 567.69 | 2727.3 | 1.6870 | 6.9777 |
| 140 | 316.3 | 0.0010797 | 0.5089 | 589.13 | 2733.9 | 1.7391 | 6.9299 |
| 145 | 415.4 | 0.0010850 | 0.4463 | 610.63 | 2740.3 | 1.7907 | 6.8833 |
| 150 | 475.8 | 0.0010905 | 0.3928 | 632.20 | 2746.5 | 1.8418 | 6.8379 |
| 155 | 543.1 | 0.0010961 | 0.3468 | 653.84 | 2752.4 | 1.8925 | 6.7935 |
| 160 | 617.8 | 0.0011020 | 0.3071 | 675.55 | 2758.1 | 1.9427 | 6.7502 |
| 165 | 700.5 | 0.0011080 | 0.2727 | 697.34 | 2763.5 | 1.9925 | 6.7078 |
| 170 | 791.7 | 0.0011143 | 0.2428 | 719.21 | 2768.7 | 2.0419 | 6.6663 |
| 175 | 892.0 | 0.0011207 | 0.2168 | 741.17 | 2773.6 | 2.0909 | 6.6256 |
| 180 | 1002.1 | 0.0011274 | 0.19405 | 763.22 | 2778.2 | 2.1396 | 6.5857 |
| 190 | 1254.4 | 0.0011414 | 0.15654 | 807.62 | 2786.4 | 2.2359 | 6.5079 |
| 200 | 1553.8 | 0.0011565 | 0.12736 | 852.45 | 2793.2 | 2.3309 | 6.4323 |
| 225 | 2548 | 0.0011992 | 0.07849 | 966.78 | 2803.3 | 2.5639 | 6.2503 |
| 250 | 3973 | 0.0012512 | 0.05013 | 1085.36 | 2801.5 | 2.7927 | 6.0730 |
| 275 | 5942 | 0.0013168 | 0.03279 | 1210.07 | 2785.0 | 3.0208 | 5.8938 |
| 300 | 8581 | 0.0010436 | 0.02167 | 1344.0 | 2749.0 | 3.2534 | 5.7045 |

Source: Abridged from I. H. Keenan, F. G. Keyes, P. G. Hill, and J. G. Moore, *Steam Tables—Metric Units*. New York: John Wiley & Sons, Inc., 1969. Reprinted by permission of John Wiley & Sons, Inc.

A.3-3 Physical Properties of Air at 101.325 kPa (1 Atm Abs), SI Units

| T (°C) | T (K) | ρ (kg/m ³) | c_p (kJ/kg·K) | $\mu \times 10^5$ (Pa·s, or kg/m·s) | k (W/m·K) | N_{Pr} | $\beta \times 10^3$ (1/K) | $g\beta\rho^2/\mu^2$ (1/K·m ³) |
|-------------|------------|--------------------------------|--------------------|---|----------------|----------|------------------------------|---|
| -17.8 | 255.4 | 1.379 | 1.0048 | 1.62 | 0.02250 | 0.720 | 3.92 | 2.79×10^8 |
| 0 | 273.2 | 1.293 | 1.0048 | 1.72 | 0.02423 | 0.715 | 3.65 | 2.04×10^8 |
| 10.0 | 283.2 | 1.246 | 1.0048 | 1.78 | 0.02492 | 0.713 | 3.53 | 1.72×10^8 |
| 37.8 | 311.0 | 1.137 | 1.0048 | 1.90 | 0.02700 | 0.705 | 3.22 | 1.12×10^8 |
| 65.6 | 338.8 | 1.043 | 1.0090 | 2.03 | 0.02925 | 0.702 | 2.95 | 0.775×10^8 |
| 93.3 | 366.5 | 0.964 | 1.0090 | 2.15 | 0.03115 | 0.694 | 2.74 | 0.534×10^8 |
| 121.1 | 394.3 | 0.895 | 1.0132 | 2.27 | 0.03323 | 0.692 | 2.54 | 0.386×10^8 |
| 148.9 | 422.1 | 0.838 | 1.0174 | 2.37 | 0.03531 | 0.689 | 2.38 | 0.289×10^8 |
| 176.7 | 449.9 | 0.785 | 1.0216 | 2.50 | 0.03721 | 0.687 | 2.21 | 0.214×10^8 |
| 204.4 | 477.6 | 0.740 | 1.0258 | 2.60 | 0.03894 | 0.686 | 2.09 | 0.168×10^8 |
| 232.2 | 505.4 | 0.700 | 1.0300 | 2.71 | 0.04084 | 0.684 | 1.98 | 0.130×10^8 |
| 260.0 | 533.2 | 0.662 | 1.0341 | 2.80 | 0.04258 | 0.680 | 1.87 | 0.104×10^8 |

A.2-11 Heat-Transfer Properties of Liquid Water, SI Units

| T (°C) | T (K) | ρ (kg/m ³) | c_p (kJ/kg·K) | $\mu \times 10^3$ (Pa·s, or kg/m·s) | k (W/m·K) | N_{Pr} | $\beta \times 10^4$ (1/K) | $(g\beta\rho^2/\mu^2) \times 10^{-8}$ (1/K·m ³) |
|-------------|------------|--------------------------------|--------------------|---|----------------|----------|------------------------------|--|
| 0 | 273.2 | 999.6 | 4.229 | 1.786 | 0.5694 | 13.3 | -0.630 | |
| 15.6 | 288.8 | 998.0 | 4.187 | 1.131 | 0.5884 | 8.07 | 1.44 | 10.93 |
| 26.7 | 299.9 | 996.4 | 4.183 | 0.860 | 0.6109 | 5.89 | 2.34 | 30.70 |
| 37.8 | 311.0 | 994.7 | 4.183 | 0.682 | 0.6283 | 4.51 | 3.24 | 68.0 |
| 65.6 | 338.8 | 981.9 | 4.187 | 0.432 | 0.6629 | 2.72 | 5.04 | 256.2 |
| 93.3 | 366.5 | 962.7 | 4.229 | 0.3066 | 0.6802 | 1.91 | 6.66 | 642 |
| 121.1 | 394.3 | 943.5 | 4.271 | 0.2381 | 0.6836 | 1.49 | 8.46 | 1300 |
| 148.9 | 422.1 | 917.9 | 4.312 | 0.1935 | 0.6836 | 1.22 | 10.08 | 2231 |
| 204.4 | 477.6 | 858.6 | 4.522 | 0.1384 | 0.6611 | 0.950 | 14.04 | 5308 |
| 260.0 | 533.2 | 784.9 | 4.982 | 0.1042 | 0.6040 | 0.859 | 19.8 | 11 030 |
| 315.6 | 588.8 | 679.2 | 6.322 | 0.0862 | 0.5071 | 1.07 | 31.5 | 19 260 |

Source: Geankoplis, Transport Processes and Separation Process Principles, 4th Edition, Prentice Hall, 2003

Typo in value of α_{Cu} corrected, 24Feb2019.

Appendix H

Physical Properties of Solids

| Material | ρ | | c_p | | α | | k (Btu/h ft °F) | | | (W/m · K) | | |
|-------------------------------------|---|---------------------------------|-------------------------------------|--|--------------------------------|---|----------------------|-------------|-------------|------------|------------|------------|
| | (lb _m /ft ³) (68°F) | (kg/m ³) (293 K) | (Btu/lb _m °F) (293 K) | (J/kg · 1K) × 10 ⁻² (293K) | (ft ² /h) (68°F) | (m ² /s) · 10 ⁵ (293k) | °F (68) | °F (212) | °F (572) | K (293) | K (373) | K (573) |
| Metals | | | | | | | | | | | | |
| Aluminum | 168.6 | 2,701.1 | 0.224 | 9.383 | 3.55 | 9.16 | 132 | 133 | 133 | 229 | 229 | 230 |
| Copper | 555 | 8,890 | 0.092 | 3.854 | 3.98 | 11.27 | 223 | 219 | 213 | 386 | 379 | 369 |
| Gold | 1206 | 19,320 | 0.031 | 1.299 | 4.52 | 11.66 | 169 | 170 | 172 | 293 | 294 | 298 |
| Iron | 492 | 7,880 | 0.122 | 5.110 | 0.83 | 2.14 | 42.3 | 39 | 31.6 | 73.2 | 68 | 54 |
| Lead | 708 | 11,300 | 0.030 | 1.257 | 0.80 | 2.06 | 20.3 | 19.3 | 17.2 | 35.1 | 33.4 | 29.8 |
| Magnesium | 109 | 1,750 | 0.248 | 10.39 | 3.68 | 9.50 | 99.5 | 96.8 | 91.4 | 172 | 168 | 158 |
| Nickel | 556 | 8,910 | 0.111 | 4.560 | 0.87 | 2.24 | 53.7 | 47.7 | 36.9 | 93.0 | 82.6 | 63.9 |
| Platinum | 1340 | 21,500 | 0.032 | 1.340 | 0.09 | 0.23 | 40.5 | 41.9 | 43.5 | 70.1 | 72.5 | 75.3 |
| Silver | 656 | 10,500 | 0.057 | 2.388 | 6.42 | 16.57 | 240 | 237 | 209 | 415 | 410 | 362 |
| Tin | 450 | 7,210 | 0.051 | 2.136 | 1.57 | 4.05 | 36 | 34 | — | 62 | 59 | — |
| Tungsten | 1206 | 19,320 | 0.032 | 1.340 | 2.44 | 6.30 | 94 | 87 | 77 | 160 | 150 | 130 |
| Uranium | 1167 | 18,700 | 0.027 | 1.131 | 0.53 | 1.37 | 16.9 | 17.2 | 19.6 | 29.3 | 29.8 | 33.9 |
| Zinc | 446 | 7,150 | 0.094 | 3.937 | 1.55 | 4.00 | 65 | 63 | 58 | 110 | 110 | 100 |
| Alloys | | | | | | | | | | | | |
| Aluminum 2024 | 173 | 2,770 | 0.230 | 9.634 | 1.76 | 4.54 | 70.2 | | | 122 | | |
| Brass (70% Cu, 30% Ni) | 532 | 8,520 | 0.091 | 3.812 | 1.27 | 3.28 | 61.8 | 73.9 | 85.3 | 107 | 128 | 148 |
| Constantan (60% Cu, 40% Ni) | 557 | 8,920 | 0.098 | 4.105 | 0.24 | 0.62 | 13.1 | 15.4 | | 22.7 | 26.7 | |
| Iron, cast | 455 | 7,920 | 0.100 | 4.189 | 0.65 | 1.68 | 29.6 | 26.8 | | 51.2 | 46.4 | |
| Nichrome V | 530 | 8,490 | 0.106 | 4.440 | 0.12 | 0.31 | 7.06 | 7.99 | 9.94 | 12.2 | 13.8 | 17.2 |
| Stainless steel | 488 | 7,820 | 0.110 | 4.608 | 0.17 | 0.44 | 9.4 | 10.0 | 13 | 16 | 17.3 | 23 |
| Steel, mild (1% C) | 488 | 7,820 | 0.113 | 4.733 | 0.45 | 1.16 | 24.8 | 24.8 | 22.9 | 42.9 | 42.9 | 39.0 |
| Nonmetals | | | | | | | | | | | | |
| Asbestos | 36 | 580 | 0.25 | 10.5 | | | 0.092 | 0.11 | 0.125 | 0.159 | 0.190 | 0.21 |
| Brick (fire clay) | 144 | 2,310 | 0.22 | 9.22 | | | | 0.65 | | | 1.13 | |
| Brick (masonry) | 106 | 1,670 | 0.20 | 8.38 | | | 0.38 | | | 0.66 | | |
| Brick (chrome) | 188 | 3,010 | 0.20 | 8.38 | | | | 0.67 | | | 1.16 | |
| Concrete | 144 | 2,310 | 0.21 | 8.80 | | | 0.70 | | | 1.21 | | |
| Corkboard | 10 | 160 | 0.4 | 17 | | | 0.025 | | | 0.043 | | |
| Diatomaceous earth, powdered | 14 | 220 | 0.2 | 8.4 | | | 0.03 | | | 0.05 | | |
| Glass, window | 170 | 2,720 | 0.2 | 8.4 | | | 0.45 | | | 0.78 | | |
| Glass, Pyrex | 140 | 2,240 | 0.2 | 8.4 | | | 0.63 | 0.67 | 0.84 | 1.09 | 1.16 | 1.45 |
| Kaolin firebrick | 19 | 300 | | | | | | | 0.052 | | | 0.09 |
| 85% Magnesia | 17 | 270 | | | | | 0.038 | 0.041 | | 0.066 | 0.071 | |
| Sandy loam, 4% H ₂ O | 104 | 1,670 | 0.4 | 17 | | | 0.54 | | | 0.94 | | |
| Sandy loam, 10% H ₂ O | 121 | 1,940 | | | | | 1.08 | | | 1.87 | | |
| Rock wool | 10 | 160 | 0.2 | 8.4 | | | 0.023 | 0.033 | | 0.040 | 0.057 | |
| Wood, oak ⊥ to grain | 51 | 820 | 0.57 | 23.9 | | | 0.12 | | | 0.21 | | |
| Wood, oak to grain | 51 | 820 | 0.57 | 23.9 | | | 0.23 | | | 0.40 | | |

Stokes-Einstein equation (for diffusion of a sphere):

$$D_{AB} = \frac{kT}{6\pi R\mu}$$

Lumped parameter analysis characteristic length:

$$D_{char} = \frac{V}{A}$$

Mass-Transfer Diffusion Coefficients in Binary Systems

Table J.1 Binary mass diffusivities in gases[†]

| System | <i>T</i> (K) | <i>D</i> _{AB} <i>P</i> (cm ² atm/s) | <i>D</i> _{AB} <i>P</i> (m ² Pa/s) |
|------------------|--------------|---|---|
| Air | | | |
| Ammonia | 273 | 0.198 | 2.006 |
| Aniline | 298 | 0.0726 | 0.735 |
| Benzene | 298 | 0.0962 | 0.974 |
| Bromine | 293 | 0.091 | 0.923 |
| Carbon dioxide | 273 | 0.136 | 1.378 |
| Carbon disulfide | 273 | 0.0883 | 0.894 |
| Chlorine | 273 | 0.124 | 1.256 |
| Diphenyl | 491 | 0.160 | 1.621 |
| Ethyl acetate | 273 | 0.0709 | 0.718 |
| Ethanol | 298 | 0.132 | 1.337 |
| Ethyl ether | 293 | 0.0896 | 0.908 |
| Iodine | 298 | 0.0834 | 0.845 |
| Methanol | 298 | 0.162 | 1.641 |
| Mercury | 614 | 0.473 | 4.791 |
| Naphthalene | 298 | 0.0611 | 0.619 |
| Nitrobenzene | 298 | 0.0868 | 0.879 |
| <i>n</i> -Octane | 298 | 0.0602 | 0.610 |
| Oxygen | 273 | 0.175 | 1.773 |
| Propyl acetate | 315 | 0.092 | 0.932 |
| Sulfur dioxide | 273 | 0.122 | 1.236 |
| Toluene | 298 | 0.0844 | 0.855 |
| Water | 298 | 0.260 | 2.634 |
| Ammonia | | | |
| Ethylene | 293 | 0.177 | 1.793 |
| Argon | | | |
| Neon | 293 | 0.329 | 3.333 |
| Carbon dioxide | | | |
| Benzene | 318 | 0.0715 | 0.724 |
| Carbon disulfide | 318 | 0.0715 | 0.724 |
| Ethyl acetate | 319 | 0.0666 | 0.675 |

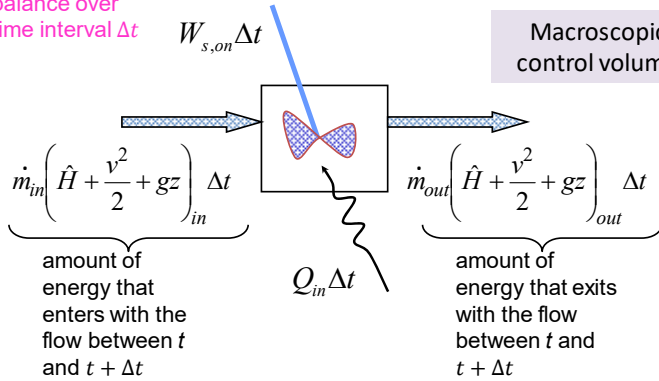
Source: Welty, Rorrer, Foster, 6th ed, 2015, Appendix J, first page only.

Unsteady Macroscopic Energy Balance

balance over time interval Δt

see Felder and Rousseau or Himmelblau

Macroscopic control volume



Unsteady Macroscopic Energy Balance

accumulation = input - output

Q_{in} = Heat **into** the chosen macroscopic control volume

$$\frac{d}{dt}(U_{sys} + E_{k,sys} + E_{p,sys}) = -\Delta H - \Delta E_k - \Delta E_p + Q_{in} + W_{s,on}$$

$Q_{in} = \sum_i q_{in,i}$ comes from a variety of sources:

Signs must match transfer from outside (bulk fluid) to inside (metal)

- Thermal conduction: $q_{in} = -kA \frac{dT}{dx}$
- Convection: $q_{in} = hA(T_b - T)$
- Radiation: $q_{in} = \epsilon \sigma A (T_{surroundings}^4 - T_{surface}^4)$
- Electric current: $q_{in} = I^2 R_{elec} L$
- Chemical Reaction: $q_{in} = S_{rxn} V_{sys}$

$S[=]$ $\frac{\text{energy}}{\text{time volume}}$

Unsteady Macroscopic Energy Balance

$$\frac{d}{dt}(U_{sys} + E_{k,sys} + E_{p,sys}) = -\Delta H - \Delta E_k - \Delta E_p + Q_{in} + W_{s,on}$$

$Q_{in} = \sum_i q_{in,i}$ comes from a variety of sources:

- **Thermal conduction:** $q_{in} = -kA \frac{dT}{dx}$
e.g. device held by bracket; a solid phase that extends through boundaries of control volume
- **Convection:** $q_{in} = hA(T_b - T)$
e.g. device dropped in stirred liquid; forced air stream flows past, natural convection occurs outside system; phase change at boundary
- **Radiation:** $q_{in} = \epsilon \sigma A (T_{surroundings}^4 - T_{surface}^4)$
e.g. device at high temp. exposed to a gas/vacuum; hot enough to produce nat. conv.=possibly hot enough for radiation
- **Electric current:** $q_{in} = I^2 R_{elec} L$
e.g. if electric current is flowing within the device/control volume/system
- **Chemical Reaction:** $q_{in} = S_{rxn} V_{sys}$
e.g. if a homogeneous reaction is taking place throughout the device/control volume/system

S-B constant:
 $\sigma = 5.676 \times 10^{-8} \frac{W}{m^2 K^4}$

Table: Emissivity ϵ of solids (300K)

| Material | ϵ |
|------------------------------|------------|
| Aluminum foil | 0.04 |
| Asbestos board | 0.96 |
| Brass, polished | 0.03 |
| Brass, dull plate | 0.22 |
| Cast iron, turned and heated | 0.60-0.70 |
| Concrete | 0.85 |
| Ice, smooth | 0.966 |
| Ice, rough | 0.985 |
| Plaster | 0.98 |
| Roofing paper | 0.91 |
| Sand | 0.76 |
| Steel, Oxidized | 0.79 |
| Wrought Iron | 0.94 |

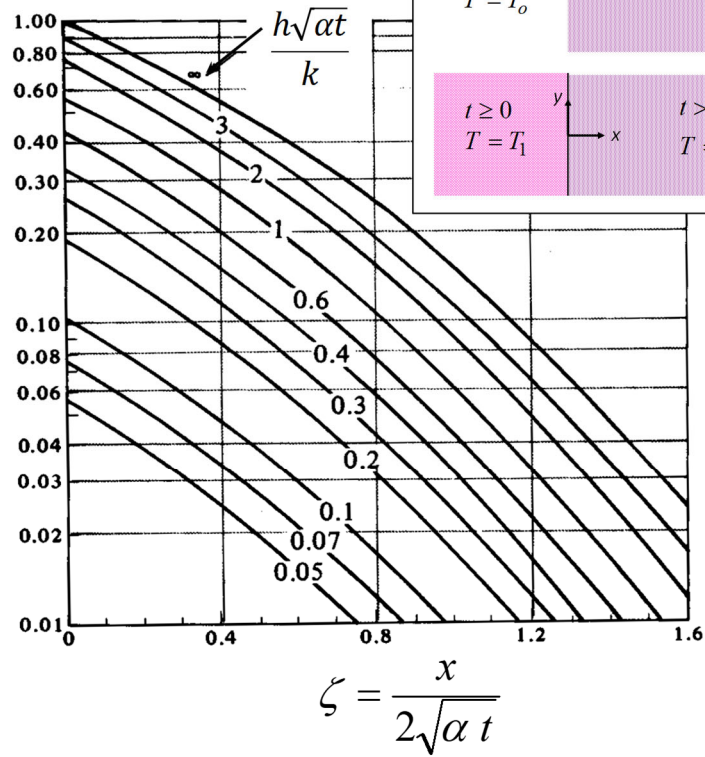
Reference: Engineering Toolbox,
www.engineeringtoolbox.com/emissivity-coefficients-d_447.html

Mechanical Energy Balance:

$$\frac{P_2 - P_1}{\rho} + \frac{\langle v \rangle_2^2 - \langle v \rangle_1^2}{2\alpha} + g(z_2 - z_1) + F_{21} = \frac{W_{s,on,21}}{\dot{m}}$$

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$1 - Y = \left(\frac{T - T_0}{T_1 - T_0} \right)$$



Geankoplis 4th ed.,
Figure 5.3-3, page 364

Heisler chart (sphere)

label = $\frac{k}{hR} = \frac{1}{Bi}$

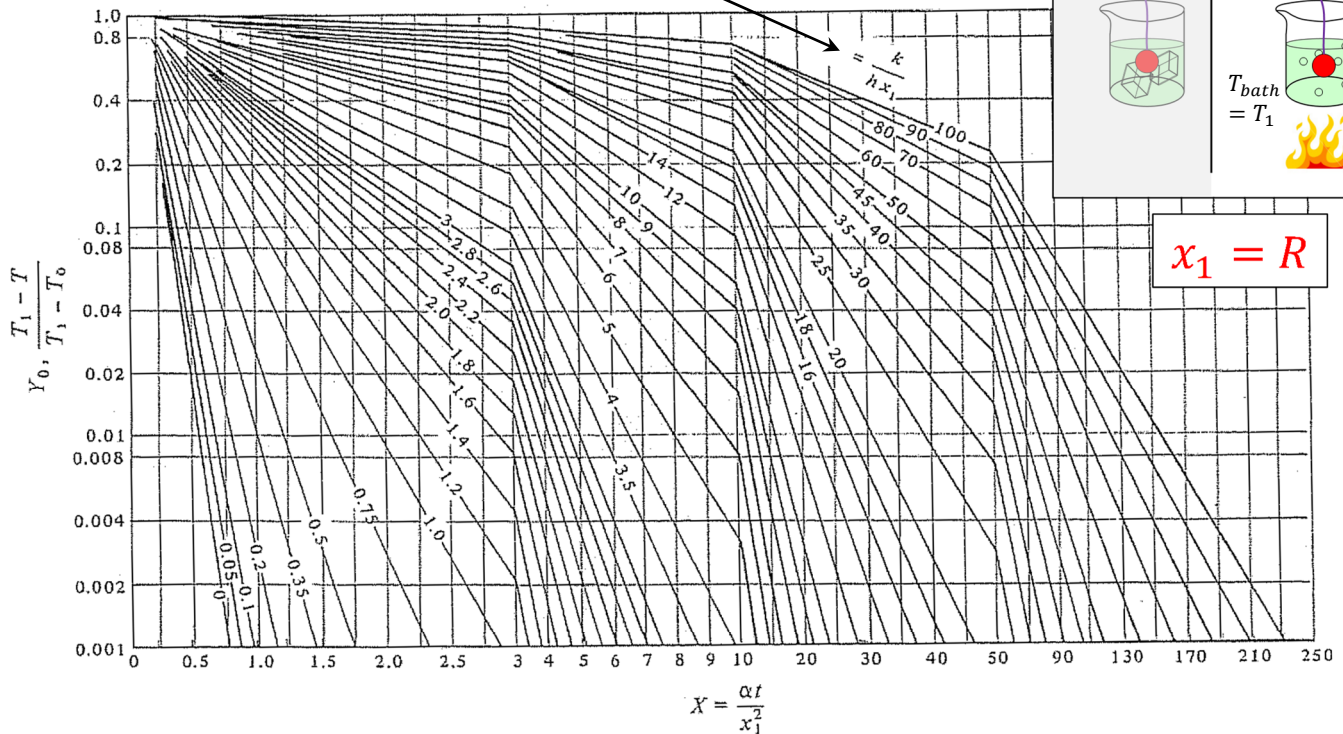
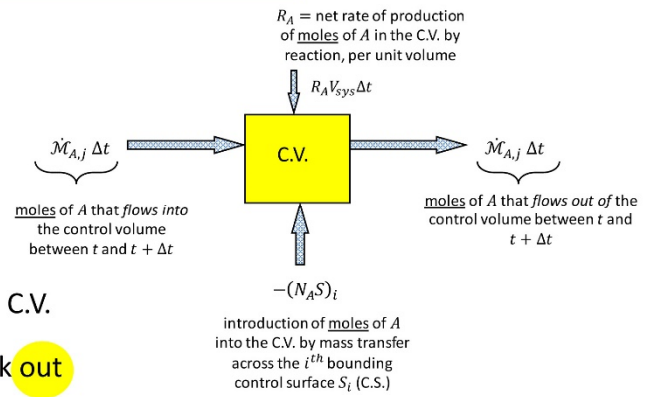


FIGURE 5.3-10. Chart for determining the temperature at the center of a sphere for unsteady-state heat conduction. [From H. P. Heisler, *Trans. A.S.M.E.*, 69, 227 (1947). With permission.] From Geankoplis, 4th edition, page 374

accumulation = net flow in + production + introduction

$$\frac{d}{dt}(\mathcal{M}_{A,sys}) = -\Delta\dot{\mathcal{M}}_A + R_A V_{sys} - \sum_i (N_A S)_i$$



$\mathcal{M}_{A,sys} = c_A V_{sys}$ = total moles of A in the C.V.

$\Delta\dot{\mathcal{M}}_A = \sum_{j,outs} \dot{\mathcal{M}}_{A,j} - \sum_{j,ins} \dot{\mathcal{M}}_{A,j}$ = bulk out

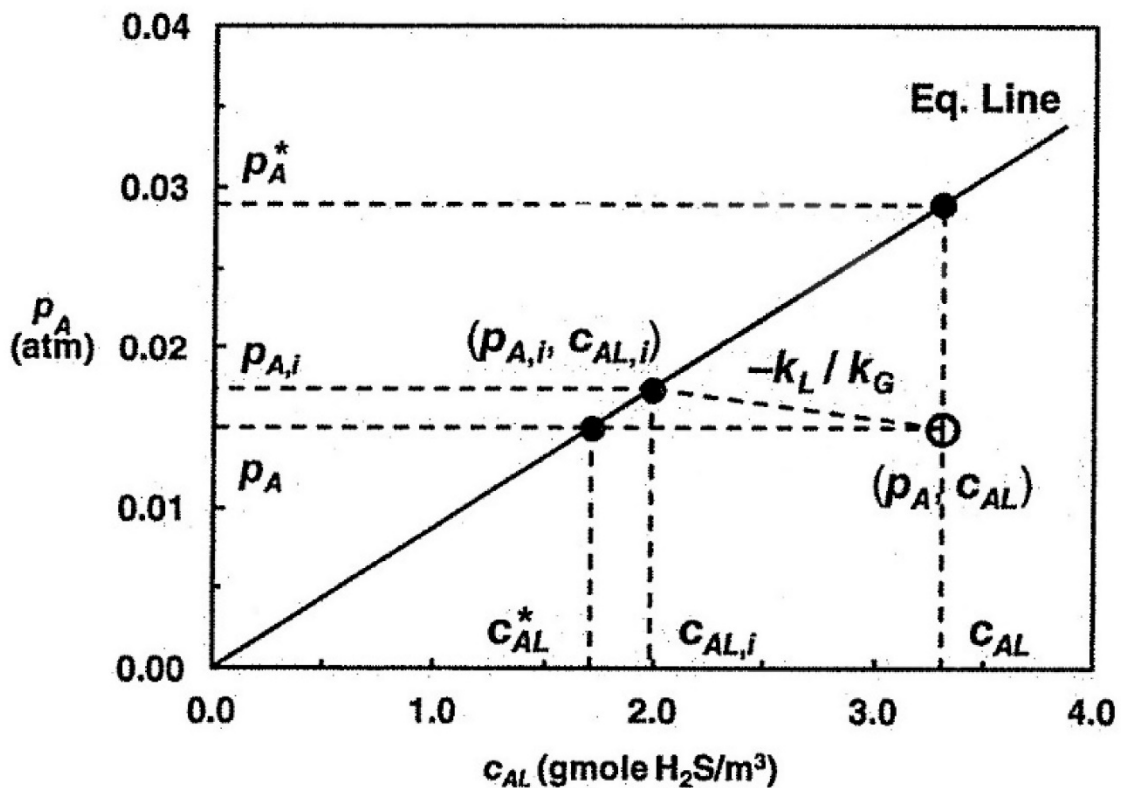
R_A = net rate of production of moles of A in the C.V. by reaction, per unit volume

V_{sys} = system volume

$N_{A,i} = k_c (c_A - c_{A,i}^*)$ = molar flux of A out through the ith C.S.

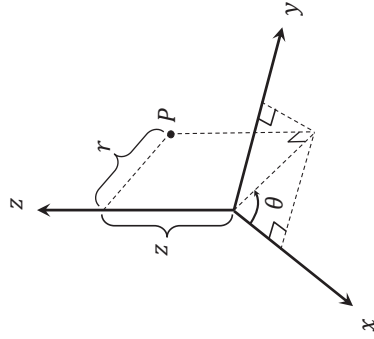
$S_{sys} = \sum_i S_i$
 Δ is "out" - "in"
 C.S. = control surface
 C.V. = control volume

Example:
 WRF Example 1 page 604 (solution in text)

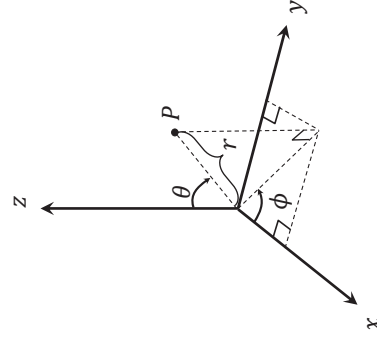


The equations in F. A. Morrison, *An Introduction to Fluid Mechanics* (Cambridge, 2013) assume the following definitions of the cylindrical and spherical coordinate systems.

Cylindrical Coordinate System: Note that the θ -coordinate swings around the z -axis



Spherical Coordinate System: Note that the θ -coordinate swings down from the z -axis; this is different from its definition in the cylindrical system above.



Typical values of the convection heat transfer coefficient. From Incropera et al., *Fundamentals of Heat and Mass Transfer*, 6th edition, Wiley, 2007.

| Process | | $h \left(\frac{W}{m^2 K} \right)$ |
|------------------------------|-------------------------|------------------------------------|
| Free convection | Gases | 2-25 |
| | Liquids | 50-1000 |
| Forced convection | Gases | 25-250 |
| | Liquids | 100-20,000 |
| Convection with phase change | Boiling or condensation | $2500-10^5$ |

The **Equation of Energy** in Cartesian, cylindrical, and spherical coordinates for Newtonian fluids of constant density, with source term S . Source could be electrical energy due to current flow, chemical energy, etc. Two cases are presented: the general case where thermal conductivity may be a function of temperature (vector flux $\underline{\tilde{q}} = \underline{q}/A$ appears in the equations); and the more usual case, where thermal conductivity is constant.

Fall 2013 Faith A. Morrison, Michigan Technological University

Microscopic energy balance, in terms of flux; Gibbs notation

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = -\nabla \cdot \underline{\tilde{q}} + S$$

Microscopic energy balance, in terms of flux; Cartesian coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) = - \left(\frac{\partial \tilde{q}_x}{\partial x} + \frac{\partial \tilde{q}_y}{\partial y} + \frac{\partial \tilde{q}_z}{\partial z} \right) + S$$

Microscopic energy balance, in terms of flux; cylindrical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} \right) = - \left(\frac{1}{r} \frac{\partial (r \tilde{q}_r)}{\partial r} + \frac{1}{r} \frac{\partial \tilde{q}_\theta}{\partial \theta} + \frac{\partial \tilde{q}_z}{\partial z} \right) + S$$

Microscopic energy balance, in terms of flux; spherical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} \right) = - \left(\frac{1}{r^2} \frac{\partial (r^2 \tilde{q}_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (\tilde{q}_\theta \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial \tilde{q}_\phi}{\partial \phi} \right) + S$$

Fourier's law of heat conduction, Gibbs notation: $\underline{\tilde{q}} = -k \nabla T$

Fourier's law of heat conduction, Cartesian coordinates:

$$\begin{pmatrix} \tilde{q}_x \\ \tilde{q}_y \\ \tilde{q}_z \end{pmatrix}_{xyz} = \begin{pmatrix} -k \frac{\partial T}{\partial x} \\ -k \frac{\partial T}{\partial y} \\ -k \frac{\partial T}{\partial z} \end{pmatrix}_{xyz}$$

Fourier's law of heat conduction, cylindrical coordinates:

$$\begin{pmatrix} \tilde{q}_r \\ \tilde{q}_\theta \\ \tilde{q}_z \end{pmatrix}_{xyz} = \begin{pmatrix} -k \frac{\partial T}{\partial r} \\ -\frac{k}{r} \frac{\partial T}{\partial \theta} \\ -k \frac{\partial T}{\partial z} \end{pmatrix}_{r\theta z}$$

Fourier's law of heat conduction, spherical coordinates:

$$\begin{pmatrix} \tilde{q}_r \\ \tilde{q}_\theta \\ \tilde{q}_\phi \end{pmatrix}_{xyz} = \begin{pmatrix} -k \frac{\partial T}{\partial r} \\ -\frac{k}{r} \frac{\partial T}{\partial \theta} \\ -\frac{k}{r \sin \theta} \frac{\partial T}{\partial \phi} \end{pmatrix}_{r\theta\phi}$$

The **Equation of Energy** for systems with **constant k**

Microscopic energy balance, constant thermal conductivity; Gibbs notation

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S$$

Microscopic energy balance, constant thermal conductivity; Cartesian coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + S$$

Microscopic energy balance, constant thermal conductivity; cylindrical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + S$$

Microscopic energy balance, constant thermal conductivity; spherical coordinates

$$\begin{aligned} \rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} \right) \\ = k \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + S \end{aligned}$$

Reference: F. A. Morrison, "Web Appendix to *An Introduction to Fluid Mechanics*," Cambridge University Press, New York, 2013. On the web at www.chem.mtu.edu/~fmorriso/IFM_WebAppendixCD2013.pdf

The **Equation of Species Mass Balance** in Cartesian, cylindrical, and spherical coordinates for binary mixtures of A and B. Two cases are presented: the general case, where the mass flux with respect to mass-average velocity (\underline{J}_A) appears (p. 1), and the more usual case (p. 2), where the diffusion coefficient is constant and Fick's law has been incorporated.

Spring 2019 Faith A. Morrison, Michigan Technological University

In terms of mass flux, \underline{J}_A

Microscopic species mass balance, in terms of mass flux; Gibbs notation

$$\rho \left(\frac{\partial \omega_A}{\partial t} + \underline{v} \cdot \nabla \omega_A \right) = -\nabla \cdot \underline{J}_A + r_A$$

WRF 25-10

Microscopic species mass balance, in terms of mass flux; Cartesian coordinates

$$\rho \left(\frac{\partial \omega_A}{\partial t} + v_x \frac{\partial \omega_A}{\partial x} + v_y \frac{\partial \omega_A}{\partial y} + v_z \frac{\partial \omega_A}{\partial z} \right) = - \left(\frac{\partial j_{A,x}}{\partial x} + \frac{\partial j_{A,y}}{\partial y} + \frac{\partial j_{A,z}}{\partial z} \right) + r_A$$

Microscopic species mass balance, in terms of mass flux; cylindrical coordinates

$$\rho \left(\frac{\partial \omega_A}{\partial t} + v_r \frac{\partial \omega_A}{\partial r} + \frac{v_\theta}{r} \frac{\partial \omega_A}{\partial \theta} + v_z \frac{\partial \omega_A}{\partial z} \right) = - \left(\frac{1}{r} \frac{\partial (r j_{A,r})}{\partial r} + \frac{1}{r} \frac{\partial j_{A,\theta}}{\partial \theta} + \frac{\partial j_{A,z}}{\partial z} \right) + r_A$$

Microscopic species mass balance, in terms of mass flux; spherical coordinates

$$\rho \left(\frac{\partial \omega_A}{\partial t} + v_r \frac{\partial \omega_A}{\partial r} + \frac{v_\theta}{r} \frac{\partial \omega_A}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial \omega_A}{\partial \phi} \right) = - \left(\frac{1}{r^2} \frac{\partial (r^2 j_{A,r})}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (j_{A,\theta} \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial j_{A,\phi}}{\partial \phi} \right) + r_A$$

Fick's law of diffusion, Gibbs notation: $\underline{J}_A = -\rho D_{AB} \nabla \omega_A$

WRF 24-17

$$= \rho \omega_A (\underline{v}_A - \underline{v})$$

Fick's law of diffusion, Cartesian coordinates: $\begin{pmatrix} j_{A,x} \\ j_{A,y} \\ j_{A,z} \end{pmatrix}_{xyz} = \begin{pmatrix} -\rho D_{AB} \frac{\partial \omega_A}{\partial x} \\ -\rho D_{AB} \frac{\partial \omega_A}{\partial y} \\ -\rho D_{AB} \frac{\partial \omega_A}{\partial z} \end{pmatrix}_{xyz}$

Fick's law of diffusion, cylindrical coordinates: $\begin{pmatrix} j_{A,r} \\ j_{A,\theta} \\ j_{A,z} \end{pmatrix}_{r\theta z} = \begin{pmatrix} -\rho D_{AB} \frac{\partial \omega_A}{\partial r} \\ -\frac{\rho D_{AB}}{r} \frac{\partial \omega_A}{\partial \theta} \\ -\rho D_{AB} \frac{\partial \omega_A}{\partial z} \end{pmatrix}_{r\theta z}$

Fick's law of diffusion, spherical coordinates: $\begin{pmatrix} j_{A,r} \\ j_{A,\theta} \\ j_{A,\phi} \end{pmatrix}_{r\theta\phi} = \begin{pmatrix} -\rho D_{AB} \frac{\partial \omega_A}{\partial r} \\ -\frac{\rho D_{AB}}{r} \frac{\partial \omega_A}{\partial \theta} \\ -\frac{\rho D_{AB}}{r \sin \theta} \frac{\partial \omega_A}{\partial \phi} \end{pmatrix}_{r\theta\phi}$

The **Equation of Species Mass Balance, constant ρD_{AB}** . For binary systems, and Fick's law has been incorporated. Good for dilute liquid solutions at constant temperature and pressure.

Microscopic species mass balance, constant thermal conductivity; Gibbs notation

$$\rho \left(\frac{\partial \omega_A}{\partial t} + \underline{v} \cdot \nabla \omega_A \right) = \rho D_{AB} \nabla^2 \omega_A + r_A$$

Microscopic species mass balance, constant thermal conductivity; Cartesian coordinates

$$\rho \left(\frac{\partial \omega_A}{\partial t} + v_x \frac{\partial \omega_A}{\partial x} + v_y \frac{\partial \omega_A}{\partial y} + v_z \frac{\partial \omega_A}{\partial z} \right) = \rho D_{AB} \left(\frac{\partial^2 \omega_A}{\partial x^2} + \frac{\partial^2 \omega_A}{\partial y^2} + \frac{\partial^2 \omega_A}{\partial z^2} \right) + r_A$$

Microscopic species mass balance, constant thermal conductivity; cylindrical coordinates

$$\rho \left(\frac{\partial \omega_A}{\partial t} + v_r \frac{\partial \omega_A}{\partial r} + \frac{v_\theta}{r} \frac{\partial \omega_A}{\partial \theta} + v_z \frac{\partial \omega_A}{\partial z} \right) = \rho D_{AB} \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \omega_A}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \omega_A}{\partial \theta^2} + \frac{\partial^2 \omega_A}{\partial z^2} \right) + r_A$$

Microscopic species mass balance, constant thermal conductivity; spherical coordinates

$$\begin{aligned} \rho \left(\frac{\partial \omega_A}{\partial t} + v_r \frac{\partial \omega_A}{\partial r} + \frac{v_\theta}{r} \frac{\partial \omega_A}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial \omega_A}{\partial \phi} \right) \\ = \rho D_{AB} \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \omega_A}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \omega_A}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \omega_A}{\partial \phi^2} \right) + r_A \end{aligned}$$

$$c x_A = c_A = \frac{1}{M_A} (\rho_A) = \frac{1}{M_A} (\rho \omega_A) \quad \left(\text{units: } c [=] \frac{\text{mol mix}}{\text{vol soln}}; \rho [=] \frac{\text{mass mix}}{\text{vol soln}}; c_A [=] \frac{\text{mol } A}{\text{vol soln}}; \rho_A [=] \frac{\text{mass } A}{\text{vol soln}} \right)$$

$$\underline{J}_A \equiv \text{mass flux of species } A \text{ relative to a mixture's mass average velocity, } \underline{v} \quad \left(\text{units: } \underline{J}_A [=] \frac{\text{mass } A}{\text{area} \cdot \text{time}} \right)$$

$$= \rho_A (\underline{v}_A - \underline{v})$$

$\underline{J}_A + \underline{J}_B = 0$, i.e. these fluxes are measured relative to the mixture's center of mass

$\underline{n}_A \equiv \rho_A \underline{v}_A = \underline{J}_A + \rho_A \underline{v} =$ combined mass flux relative to stationary coordinates

$$\underline{n}_A + \underline{n}_B = \rho \underline{v}$$

$\underline{v}_A \equiv$ velocity of species A in a mixture, i.e. average velocity of all molecules of species A within a small volume

$\underline{v} = \omega_A \underline{v}_A + \omega_B \underline{v}_B \equiv$ mass average velocity; same velocity as in the microscopic momentum and energy balances

The Equation of Species Mass Balance in Terms of Combined

Molar quantities in Cartesian, cylindrical, and spherical coordinates for binary mixtures of A and B.

The general case, where the combined molar flux with respect to molar velocity (\underline{N}_A), is given on page 1.

Spring 2019 Faith A. Morrison, Michigan Technological University

In terms of total molar flux, \underline{N}_A

Microscopic species mass balance, in terms of molar flux; Gibbs notation

$$\frac{\partial c_A}{\partial t} = -\nabla \cdot \underline{N}_A + R_A$$

WRF 25-11

Microscopic species mass balance, in terms of combined molar flux; Cartesian coordinates

$$\frac{\partial c_A}{\partial t} = -\left(\frac{\partial N_{A,x}}{\partial x} + \frac{\partial N_{A,y}}{\partial y} + \frac{\partial N_{A,z}}{\partial z}\right) + R_A$$

Microscopic species mass balance, in terms of combined molar flux; cylindrical coordinates

$$\frac{\partial c_A}{\partial t} = -\left(\frac{1}{r} \frac{\partial(rN_{A,r})}{\partial r} + \frac{1}{r} \frac{\partial N_{A,\theta}}{\partial \theta} + \frac{\partial N_{A,z}}{\partial z}\right) + R_A$$

Microscopic species mass balance, in terms of combined molar flux; spherical coordinates

$$\frac{\partial c_A}{\partial t} = -\left(\frac{1}{r^2} \frac{\partial(r^2 N_{A,r})}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial(N_{A,\theta} \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial N_{A,z}}{\partial \phi}\right) + R_A$$

Fick's law of diffusion, Gibbs notation: $\underline{N}_A = x_A(\underline{N}_A + \underline{N}_B) - cD_{AB}\nabla x_A$

WRF 24-22

$$= c_A \underline{v}^* - cD_{AB}\nabla x_A$$

Fick's law of diffusion, Cartesian coordinates: $\begin{pmatrix} N_{A,x} \\ N_{A,y} \\ N_{A,z} \end{pmatrix}_{xyz} = \begin{pmatrix} x_A(N_{A,x} + N_{B,x}) - cD_{AB} \frac{\partial x_A}{\partial x} \\ x_A(N_{A,y} + N_{B,y}) - cD_{AB} \frac{\partial x_A}{\partial y} \\ x_A(N_{A,z} + N_{B,z}) - cD_{AB} \frac{\partial x_A}{\partial z} \end{pmatrix}_{xyz}$

Fick's law of diffusion, cylindrical coordinates: $\begin{pmatrix} N_{A,r} \\ N_{A,\theta} \\ N_{A,z} \end{pmatrix}_{r\theta z} = \begin{pmatrix} x_A(N_{A,r} + N_{B,r}) - cD_{AB} \frac{\partial x_A}{\partial r} \\ x_A(N_{A,\theta} + N_{B,\theta}) - \frac{cD_{AB}}{r} \frac{\partial x_A}{\partial \theta} \\ x_A(N_{A,z} + N_{B,z}) - cD_{AB} \frac{\partial x_A}{\partial z} \end{pmatrix}_{r\theta z}$

Fick's law of diffusion, spherical coordinates: $\begin{pmatrix} N_{A,r} \\ N_{A,\theta} \\ N_{A,\phi} \end{pmatrix}_{r\theta\phi} = \begin{pmatrix} x_A(N_{A,r} + N_{B,r}) - cD_{AB} \frac{\partial x_A}{\partial r} \\ x_A(N_{A,\theta} + N_{B,\theta}) - \frac{cD_{AB}}{r} \frac{\partial x_A}{\partial \theta} \\ x_A(N_{A,\phi} + N_{B,\phi}) - \frac{cD_{AB}}{r \sin \theta} \frac{\partial x_A}{\partial \phi} \end{pmatrix}_{r\theta\phi}$

NOTES:

- If component A has no sink, $\underline{N}_A = 0$.
- If A diffuses through stagnant B , $\underline{N}_B = 0$.
- If a binary mixture of A and B are undergoing steady equimolar counterdiffusion, $\underline{N}_A = -\underline{N}_B$.
- If, for example, two moles of A diffuse to a surface at which a rapid, irreversible reaction converts it to one mole of B , then at steady state $-0.5\underline{N}_A = \underline{N}_B$.

$$c x_A = c_A = \frac{1}{M_A} (\rho_A) = \frac{1}{M_A} (\rho \omega_A) \quad \left(\text{units: } c [=] \frac{\text{mol mix}}{\text{vol soln}}; \rho [=] \frac{\text{mass mix}}{\text{vol soln}}; c_A [=] \frac{\text{mol } A}{\text{vol soln}}; \rho_A [=] \frac{\text{mass } A}{\text{vol soln}} \right)$$

$$\underline{J}_A^* \equiv \text{molar flux relative to a mixture's molar average velocity, } \underline{v}^* \quad \left(\text{units: } \underline{J}_A^* [=] \frac{\text{mole } A}{\text{area} \cdot \text{time}} \right)$$

$$= c_A (\underline{v}_A - \underline{v}^*)$$

$$\underline{J}_A^* + \underline{J}_B^* = 0$$

$$\underline{N}_A \equiv c_A \underline{v}_A = \underline{J}_A^* + c_A \underline{v}^* = \text{combined molar flux relative to stationary coordinates}$$

$$\underline{N}_A + \underline{N}_B = c \underline{v}^*$$

$\underline{v}_A \equiv$ velocity of species A in a mixture, i.e. average velocity of all molecules of species A within a small volume

$$\underline{v}^* = x_A \underline{v}_A + x_B \underline{v}_B \equiv \text{molar average velocity}$$

The Equation of Species Mass Balance in Terms of Molar

quantities in Cartesian, cylindrical, and spherical coordinates for binary mixtures of A and B. Two cases are presented: the general case, where the molar flux with respect to molar velocity (\underline{J}_A^*) appears (p. 1), and the more usual case (p. 2), where the diffusion coefficient is constant and Fick's law has been incorporated.

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In terms of molar flux, \underline{J}_A^*

Microscopic species mass balance, in terms of molar flux; Gibbs notation

$$c \left(\frac{\partial x_A}{\partial t} + \underline{v}^* \cdot \nabla x_A \right) = -\nabla \cdot \underline{J}_A^* + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, in terms of molar flux; Cartesian coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_x^* \frac{\partial x_A}{\partial x} + v_y^* \frac{\partial x_A}{\partial y} + v_z^* \frac{\partial x_A}{\partial z} \right) = - \left(\frac{\partial J_{A,x}^*}{\partial x} + \frac{\partial J_{A,y}^*}{\partial y} + \frac{\partial J_{A,z}^*}{\partial z} \right) + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, in terms of molar flux; cylindrical coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_r^* \frac{\partial x_A}{\partial r} + \frac{v_\theta^*}{r} \frac{\partial x_A}{\partial \theta} + v_z^* \frac{\partial x_A}{\partial z} \right) = - \left(\frac{1}{r} \frac{\partial (r J_{A,r}^*)}{\partial r} + \frac{1}{r} \frac{\partial J_{A,\theta}^*}{\partial \theta} + \frac{\partial J_{A,z}^*}{\partial z} \right) + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, in terms of molar flux; spherical coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_r^* \frac{\partial x_A}{\partial r} + \frac{v_\theta^*}{r} \frac{\partial x_A}{\partial \theta} + \frac{v_\phi^*}{r \sin \theta} \frac{\partial x_A}{\partial \phi} \right) = - \left(\frac{1}{r^2} \frac{\partial (r^2 J_{A,r}^*)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (J_{A,\theta}^* \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial J_{A,\phi}^*}{\partial \phi} \right) + (x_B R_A - x_A R_B)$$

Fick's law of diffusion, Gibbs notation: $\underline{J}_A^* = -c D_{AB} \nabla x_A$

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$$= c x_A (\underline{v}_A - \underline{v}^*)$$

Fick's law of diffusion, Cartesian coordinates: $\begin{pmatrix} J_{A,x}^* \\ J_{A,y}^* \\ J_{A,z}^* \end{pmatrix}_{xyz} = \begin{pmatrix} -c D_{AB} \frac{\partial x_A}{\partial x} \\ -c D_{AB} \frac{\partial x_A}{\partial y} \\ -c D_{AB} \frac{\partial x_A}{\partial z} \end{pmatrix}_{xyz}$

Fick's law of diffusion, cylindrical coordinates: $\begin{pmatrix} J_{A,r}^* \\ J_{A,\theta}^* \\ J_{A,z}^* \end{pmatrix}_{r\theta z} = \begin{pmatrix} -c D_{AB} \frac{\partial x_A}{\partial r} \\ -\frac{c D_{AB}}{r} \frac{\partial x_A}{\partial \theta} \\ -c D_{AB} \frac{\partial x_A}{\partial z} \end{pmatrix}_{r\theta z}$

Fick's law of diffusion, spherical coordinates: $\begin{pmatrix} J_{A,r}^* \\ J_{A,\theta}^* \\ J_{A,\phi}^* \end{pmatrix}_{r\theta\phi} = \begin{pmatrix} -c D_{AB} \frac{\partial x_A}{\partial r} \\ -\frac{c D_{AB}}{r} \frac{\partial x_A}{\partial \theta} \\ -\frac{c D_{AB}}{r \sin \theta} \frac{\partial x_A}{\partial \phi} \end{pmatrix}_{r\theta\phi}$

The Equation of Species Mass Balance in Terms of Molar

Quantities, constant cD_{AB} . For binary systems, and Fick's law has been incorporated. Good for low density gases at constant temperature and pressure.

Microscopic species mass balance, constant thermal conductivity; Gibbs notation

$$c \left(\frac{\partial x_A}{\partial t} + \underline{v}^* \cdot \nabla x_A \right) = cD_{AB} \nabla^2 x_A + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, constant thermal conductivity; Cartesian coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_x^* \frac{\partial x_A}{\partial x} + v_y^* \frac{\partial x_A}{\partial y} + v_z^* \frac{\partial x_A}{\partial z} \right) = cD_{AB} \left(\frac{\partial^2 x_A}{\partial x^2} + \frac{\partial^2 x_A}{\partial y^2} + \frac{\partial^2 x_A}{\partial z^2} \right) + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, constant thermal conductivity; cylindrical coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_r^* \frac{\partial x_A}{\partial r} + \frac{v_\theta^*}{r} \frac{\partial x_A}{\partial \theta} + v_z^* \frac{\partial x_A}{\partial z} \right) = cD_{AB} \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial x_A}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 x_A}{\partial \theta^2} + \frac{\partial^2 x_A}{\partial z^2} \right) + (x_B R_A - x_A R_B)$$

Microscopic species mass balance, constant thermal conductivity; spherical coordinates

$$c \left(\frac{\partial x_A}{\partial t} + v_r^* \frac{\partial x_A}{\partial r} + \frac{v_\theta^*}{r} \frac{\partial x_A}{\partial \theta} + \frac{v_\phi^*}{r \sin \theta} \frac{\partial x_A}{\partial \phi} \right) = cD_{AB} \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial x_A}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial x_A}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 x_A}{\partial \phi^2} \right) + (x_B R_A - x_A R_B)$$

In terms of Diffusivity, D_{AB}

$$c x_A = c_A = \frac{1}{M_A} (\rho_A) = \frac{1}{M_A} (\rho \omega_A) \quad \left(\text{units: } c [=] \frac{\text{mol mix}}{\text{vol soln}}; \rho [=] \frac{\text{mass mix}}{\text{vol soln}}; c_A [=] \frac{\text{mol A}}{\text{vol soln}}; \rho_A [=] \frac{\text{mass A}}{\text{vol soln}} \right)$$

$$\underline{J}_A^* \equiv \text{molar flux relative to a mixture's molar average velocity, } \underline{v}^* \quad \left(\text{units: } \underline{J}_A^* [=] \frac{\text{mole}}{\text{area} \cdot \text{time}} \right)$$

$$= c_A (\underline{v}_A - \underline{v}^*)$$

$$\underline{J}_A^* + \underline{J}_B^* = 0$$

$$\underline{N}_A \equiv c_A \underline{v}_A = \underline{J}_A^* + c_A \underline{v}^* = \text{combined molar flux relative to stationary coordinates}$$

$$\underline{N}_A + \underline{N}_B = c \underline{v}^*$$

$\underline{v}_A \equiv$ velocity of species A in a mixture, i.e. average velocity of all molecules of species A within a small volume

$\underline{v}^* = x_A \underline{v}_A + x_B \underline{v}_B \equiv$ molar average velocity