

## CM3120: Module 2

### Unsteady State Heat Transfer

- I. Introduction
- II. **Unsteady Microscopic Energy Balance—(slash and burn)**
- III. Unsteady Macroscopic Energy Balance
- IV. Dimensional Analysis (unsteady)—Biot number, Fourier number
- V. Low Biot number solutions—Lumped parameter analysis
- VI. Short Cut Solutions—(initial temperature  $T_0$ ; finite  $h$ ), Gurney and Lurie charts (as a function of position,  $m = \frac{1}{Bi}$ , and  $Fo$ ); Heissler charts (center point only, as a function of  $m = 1/Bi$ , and  $Fo$ )
- VII. Full Analytical Solutions (stretch)

© Faith A. Morrison, Michigan<sup>1</sup> Tech U.

## CM3120: Module 2

Module 2 Lecture II

### Unsteady State Heat Transfer (Microscopic Energy Balances)



*Professor Faith A. Morrison*

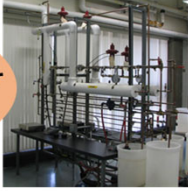
Department of Chemical Engineering  
Michigan Technological University


[www.chem.mtu.edu/~fmorriso/cm3120/cm3120.html](http://www.chem.mtu.edu/~fmorriso/cm3120/cm3120.html)

© Faith A. Morrison, Michigan<sup>2</sup> Tech U.

CM3120: Module 2

**Unsteady State Heat Transfer**  
(Microscopic Energy Balances)






**Professor Faith A. Morrison**  
 Department of Chemical Engineering  
 Michigan Technological University


We model the dynamics of unsteady state heat transfer because there are very practical problems that we can solve with such models.

© Faith A. Morrison, Michigan<sup>3</sup> Tech U.

**Example:**  
When will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?

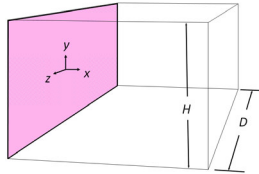




© Faith A. Morrison, Michigan<sup>4</sup> Tech U.

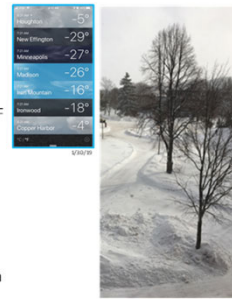
Unsteady State Heat Transfer: Dimensional Analysis

Develop a model:



**Example:**  
When will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?



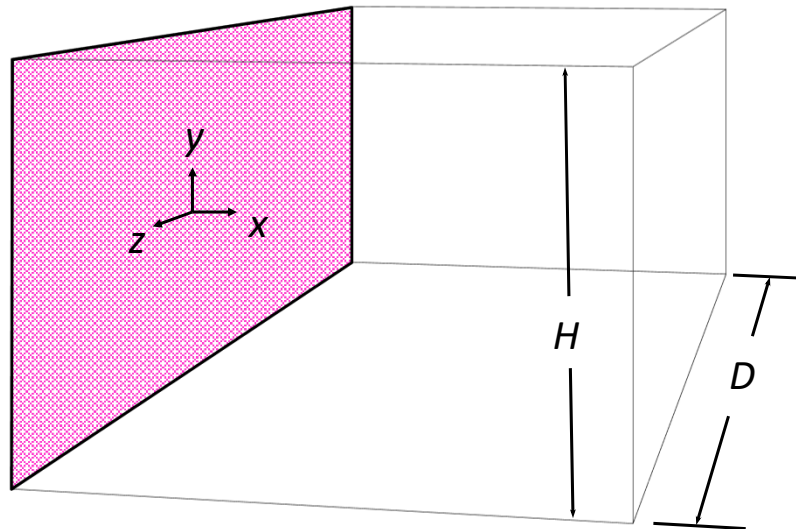
**Example 1: Unsteady Heat Conduction in a Semi-infinite solid**

A very long, very wide, very tall slab is initially at a temperature  $T_0$ . At time  $t = 0$ , the left face of the slab is exposed to a vigorously mixed gas at temperature  $T_1$ . What is the time-dependent temperature profile in the slab?

© Faith A. Morrison, Michigan Tech U.

Unsteady State Heat Transfer

Example: Unsteady Heat Conduction in a Semi-infinite solid



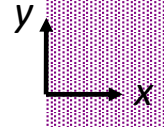
$H, D$ , very large

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

Initial Condition:

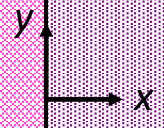
$t < 0$   
 $T = T_o$



$t < 0$   
 $T = T_o$

Then,

$t \geq 0$   
 $T = T_1$



$t > 0$   
 $T = T(x, t)$

© Faith A. Morrison, Michigan Tech U. <sup>7</sup>

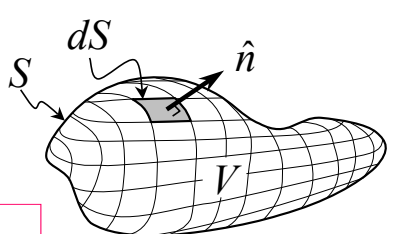
1D Heat Transfer: Unsteady State

**General Energy Transport Equation**  
 (microscopic energy balance)

As for the derivation of the microscopic momentum balance, the microscopic energy balance is derived on an arbitrary volume,  $V$ , enclosed by a surface,  $S$ .

Gibbs notation:

$$\rho \hat{C}_p \left( \frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S$$



see handout for component notation

© Faith A. Morrison, Michigan Tech U. <sup>8</sup>

1D Heat Transfer: Unsteady State

### General Energy Transport Equation

(microscopic energy balance)

$$\rho \hat{C}_p \left( \underbrace{\frac{\partial T}{\partial t}}_{\text{rate of change}} + \underbrace{\mathbf{v} \cdot \nabla T}_{\text{convection}} \right) = \underbrace{k \nabla^2 T}_{\text{conduction (all directions)}} + \underbrace{S}_{\text{source (energy generated per unit volume per time)}}$$

velocity must satisfy equation of motion, equation of continuity

see handout for component notation

© Faith A. Morrison, Michigan Tech U.

### Equation of energy

for Newtonian fluids of constant density,  $\rho$ , and thermal conductivity,  $k$ , with source term (source could be viscous dissipation, electrical energy, chemical energy, etc., with units of energy/(volume time)).

Source: R. B. Bird, W. E. Stewart, and E. N. Lightfoot, *Transport Processes*, Wiley, NY, 1960, page 319.

Gibbs notation (vector notation) [www.chem.mtu.edu/~fmorriso/cm310/energy2013.pdf](http://www.chem.mtu.edu/~fmorriso/cm310/energy2013.pdf)

$$\left( \frac{\partial T}{\partial t} + \mathbf{v} \cdot \nabla T \right) = \frac{k}{\rho \hat{C}_p} \nabla^2 T + \frac{S}{\rho \hat{C}_p}$$

thermal diffusivity  $\alpha \equiv \frac{k}{\rho \hat{C}_p}$

Cartesian (xyz) coordinates:

$$\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

Cylindrical (r $\theta$ z) coordinates:

$$\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left( \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

Spherical (r $\theta$  $\phi$ ) coordinates:

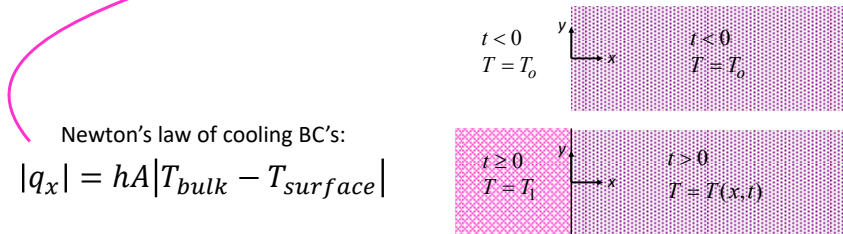
$$\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} = \frac{k}{\rho \hat{C}_p} \left( \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + \frac{S}{\rho \hat{C}_p}$$

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

**Example 1: Unsteady Heat Conduction in a Semi-infinite solid**

A very long, very wide, very tall slab is initially at a temperature  $T_0$ . At time  $t = 0$ , the left face of the slab is exposed to a vigorously mixed gas at temperature  $T_1$ . What is the time-dependent temperature profile in the slab?



Newton's law of cooling BC's:

$$|q_x| = hA|T_{bulk} - T_{surface}|$$

© Faith A. Morrison, Michigan Tech U. <sup>11</sup>

1D Heat Transfer: Unsteady State

Microscopic Energy Equation in Cartesian Coordinates

$$\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

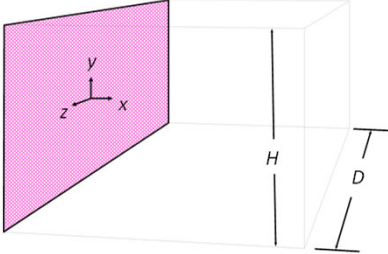
$$\alpha \equiv \frac{k}{\rho \hat{C}_p} = \text{thermal diffusivity}$$

what are the boundary conditions? initial conditions?

© Faith A. Morrison, Michigan Tech U. <sup>12</sup>

1D Heat Transfer: Unsteady State

**Example: Unsteady Heat Conduction in a Semi-infinite solid**



Initial Condition:

$t < 0$   
 $T = T_o$

$t < 0$   
 $T = T_o$

$t \geq 0$   
 $T = T_1$

$t > 0$   
 $T = T(x, t)$

You try.

© Faith A. Morrison, Michigan Tech U. <sup>13</sup>

1D Heat Transfer: Unsteady State

**Unsteady State Heat Conduction in a Semi-Infinite Slab**

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left( \frac{\partial^2 T}{\partial x^2} \right) = \alpha \left( \frac{\partial^2 T}{\partial x^2} \right)$$

thermal diffusivity

$$\alpha \equiv \frac{k}{\rho \hat{C}_p}$$

**Initial condition:**  $t = 0 \quad T = T_0 \quad \forall x$

**Boundary conditions:**

$x = 0 \quad \frac{q_x}{A} = -k \frac{dT}{dx} = h(T_1 - T) \quad t > 0$

$x = \infty \quad T = T_0 \quad \forall t$

$t < 0$   
 $T = T_o$

$t \geq 0$   
 $T = T_1$

$t < 0$   
 $T = T_o$

$t > 0$   
 $T = T(x, t)$

© Faith A. Morrison, Michigan Tech U. <sup>14</sup>

1D Heat Transfer: Unsteady State

### Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \alpha \left( \frac{\partial^2 T}{\partial x^2} \right)$$

thermal diffusivity

$$\alpha \equiv \frac{k}{\rho \hat{C}_p}$$

**Initial condition:**  $t = 0 \quad T = T_0 \quad \forall x$  "for all x"

**Boundary conditions:**

$x = 0 \quad \frac{q_x}{A} = -k \frac{dT}{dx} = h(T_1 - T) \quad t > 0$

$x = \infty \quad T = T_0 \quad \forall t$  "for all t"

15  
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

### Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \alpha \left( \frac{\partial^2 T}{\partial x^2} \right)$$

**The solution of the PDE is obtained by combination of variables.**

**Initial condition:**  $t = 0 \quad T = T_0 \quad \forall x$

**Boundary conditions:**

$x = 0 \quad \frac{q_x}{A} = -k \frac{dT}{dx} = h(T_1 - T) \quad t > 0$

$x = \infty \quad T = T_0 \quad \forall t$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

See text WRF 6<sup>th</sup> ed p284 or BSL1 p353 for the solution with temp BCs

16  
© Faith A. Morrison, Michigan Tech U.



1D Heat Transfer: Unsteady State

### Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \alpha \left( \frac{\partial^2 T}{\partial x^2} \right)$$

The solution of the PDE is obtained by combination of variables.

**Initial condition:**  $t = 0 \quad T = T_0 \quad \forall x$

**Boundary conditions:**

$$x = 0 \quad \frac{q_x}{A} = -k \frac{dT}{dx} = h(T_1 - T) \quad t > 0$$

$$x = \infty \quad T = T_0 \quad \forall t$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k} \quad \zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

See text WRF 6<sup>th</sup> ed p284 or BSL1 p353 for the solution with temp BCs

© Faith A. Morrison, Michigan Tech U. <sup>17</sup>

### Unsteady State Heat Conduction in a Semi-Infinite Slab

**Solution:**

$$\frac{T - T_0}{T_1 - T_0} = \text{erfc} \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k} \quad \zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

$$Y \equiv \frac{(T_1 - T)}{(T_1 - T_0)} \quad 1 - Y = \frac{(T - T_0)}{(T_1 - T_0)}$$

**complementary error function of y**  
(a standard function in Excel)

$$\text{erfc}(y) \equiv 1 - \text{erf}(y)$$

**error function of y**

$$\text{erf}(y) \equiv \frac{2}{\sqrt{\pi}} \int_0^y e^{-(y')^2} dy'$$

- Geankoplis 4<sup>th</sup> ed., eqn 5.3-7, page 363
- WRF, eqn 18-21, page 286

thermal diffusivity  $\alpha \equiv \frac{k}{\rho c_p}$

© Faith A. Morrison, Michigan Tech U. <sup>18</sup>

### Unsteady State Heat Conduction in a Semi-Infinite Slab

**Solution:**

$$\frac{T - T_0}{T_1 - T_0} = \text{erfc } \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

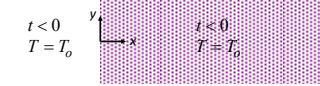
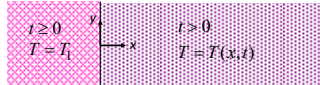
$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

complementary error function of y

$$\text{erfc}(y) \equiv 1 - \text{erf}(y)$$

error function of y

$$\text{erf}(y) \equiv \frac{2}{\sqrt{\pi}} \int_0^y e^{-(y')^2} dy'$$

To make this solution easier to use, we can plot it.

$$Y \equiv \frac{(T_1 - T)}{(T_1 - T_0)}$$

$$1 - Y = \frac{(T - T_0)}{(T_1 - T_0)}$$

thermal diffusivity  $\alpha \equiv \frac{k}{\rho c_p}$  © Faith A. Morrison, Michigan Tech U. <sup>19</sup>

### Unsteady State Heat Conduction in a Semi-Infinite Slab

**This:**

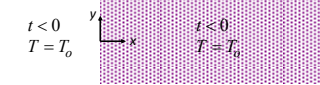
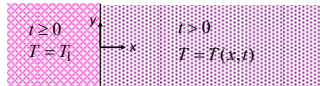
$$\frac{T - T_0}{T_1 - T_0} = \text{erfc } \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

**Versus this:**

$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

**At various values of this:**

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

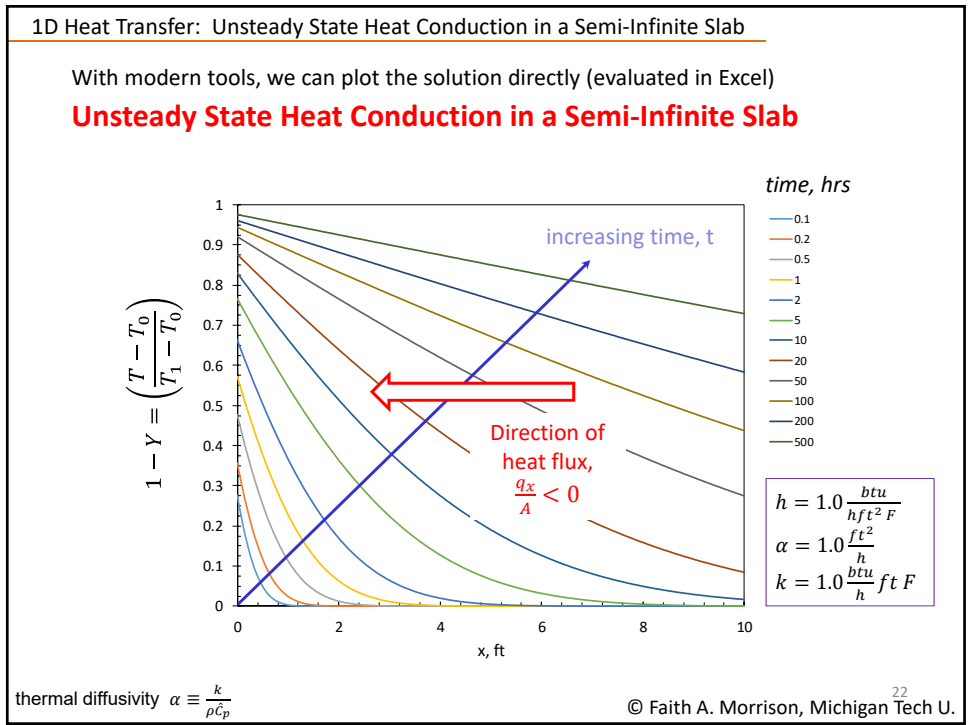
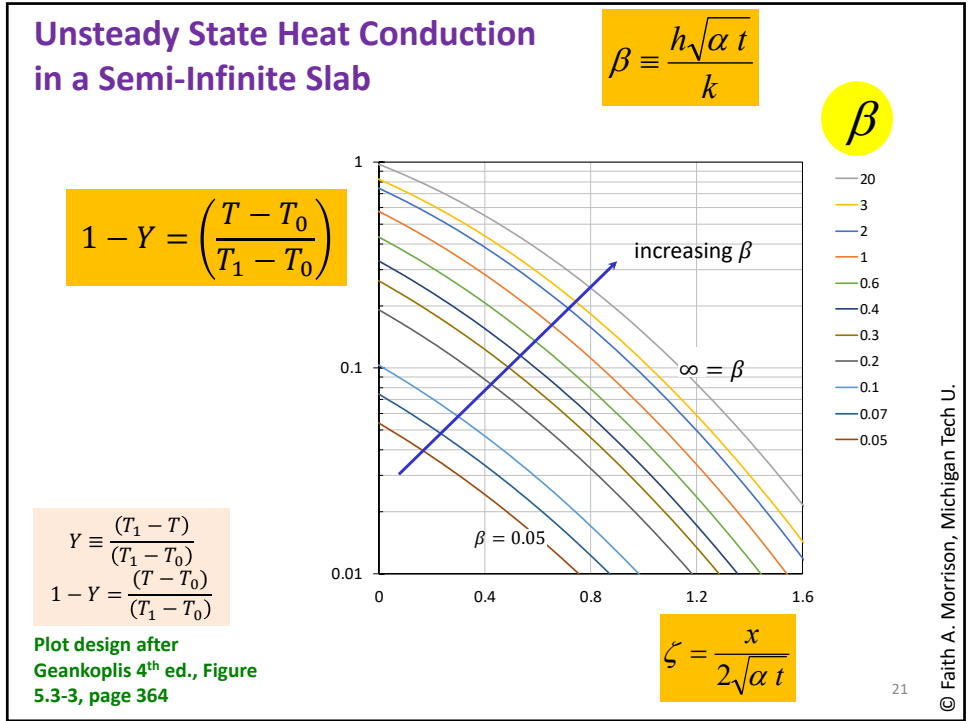



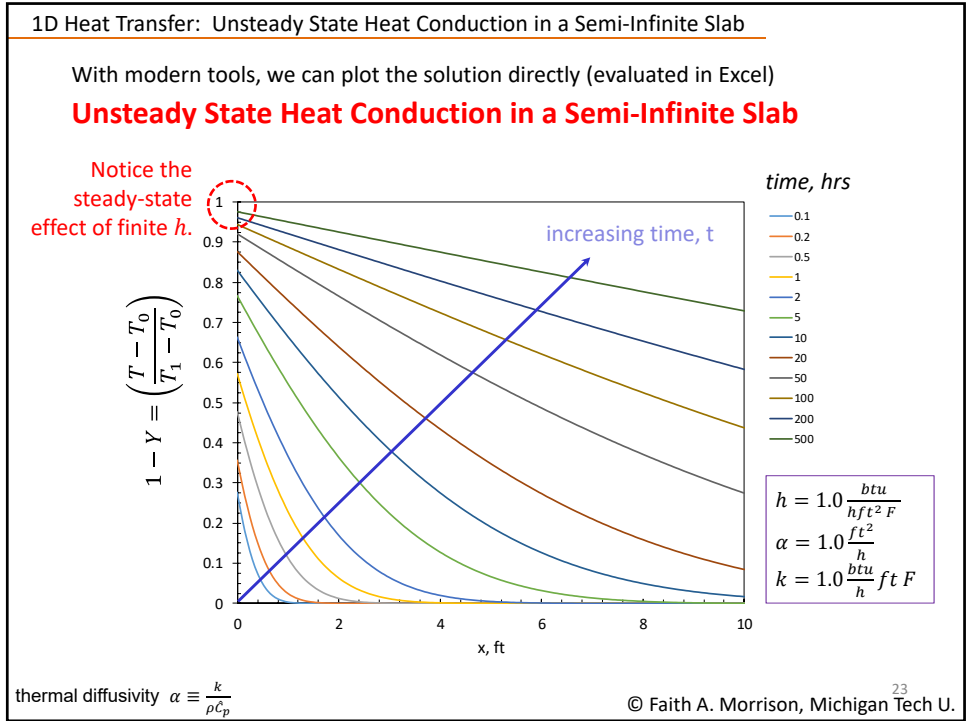
To make this solution easier to use, we can plot it.

$$Y \equiv \frac{(T_1 - T)}{(T_1 - T_0)}$$

$$1 - Y = \frac{(T - T_0)}{(T_1 - T_0)}$$

thermal diffusivity  $\alpha \equiv \frac{k}{\rho c_p}$  © Faith A. Morrison, Michigan Tech U. <sup>20</sup>





**Example:**  
When will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?

© Faith A. Morrison, Michigan Tech U. <sup>24</sup>

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

We need the appropriate physical property data for the soil.

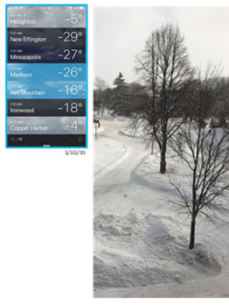
$$h = 2.0 \frac{BTU}{h \text{ ft}^2 \text{ } ^\circ F}$$

$$\alpha_{soil} = 0.018 \frac{\text{ft}^2}{h}$$

$$k_{soil} = 0.5 \frac{BTU}{h \text{ ft } ^\circ F}$$

**Example:** When will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?



thermal diffusivity  $\alpha \equiv \frac{k}{\rho c_p}$

**Example:** When will my pipes freeze?

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

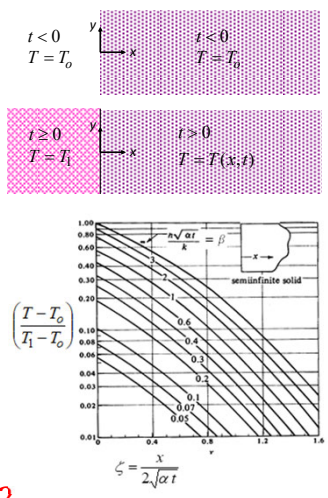
$$\frac{T - T_0}{T_1 - T_0} = \text{erfc } \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

Both  $\zeta$  and  $\beta$  depend on time

$T_0 = ?$   
 $T_1 = ?$   
 $T = ?$   
 $\frac{T - T_0}{T_1 - T_0} = ?$



$$Y \equiv \frac{(T_1 - T)}{(T_1 - T_0)}$$

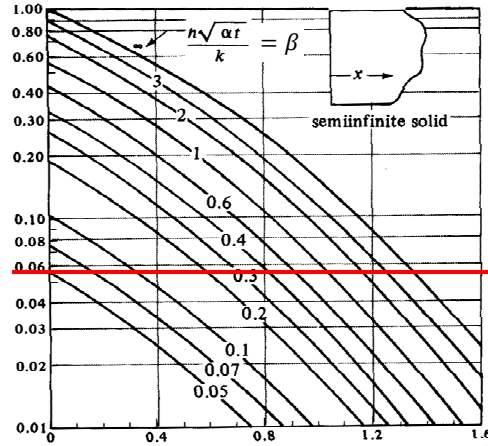
$$1 - Y = \frac{(T - T_0)}{(T_1 - T_0)}$$

**Example:** When will my pipes freeze?

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$1 - Y = \left( \frac{T - T_0}{T_1 - T_0} \right)$$

You try.



Geankoplis 4<sup>th</sup> ed., Figure 5.3-3, page 364

$$\zeta = \frac{x}{2\sqrt{\alpha t}}$$

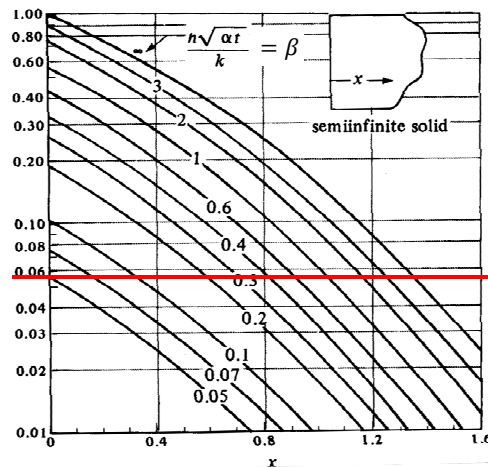
© Faith A. Morrison, Michigan Tech U. <sup>27</sup>

**Example:** When will my pipes freeze?

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$1 - Y = \left( \frac{T - T_0}{T_1 - T_0} \right)$$

**Solution:**  
 Guess large  $\beta$   
 (Iterative solution)



Geankoplis 4<sup>th</sup> ed., Figure 5.3-3, page 364

$$\zeta = \frac{x}{2\sqrt{\alpha t}}$$

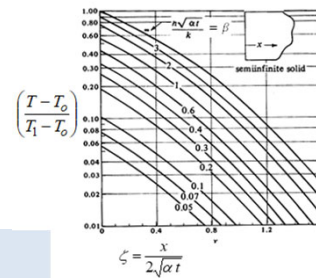
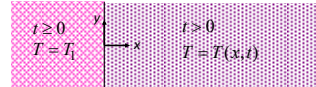
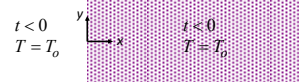
© Faith A. Morrison, Michigan Tech U. <sup>28</sup>

**Example: When will my pipes freeze?**

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{T - T_0}{T_1 - T_0} = \operatorname{erfc} \zeta - e^{\beta(2\zeta + \beta)} \operatorname{erfc}(\zeta + \beta)$$

**Answer:**  
 $t \approx 480 \text{ hours} \approx 20 \text{ days}$



$$Y \equiv \frac{(T_1 - T)}{(T_1 - T_0)}$$

$$1 - Y = \frac{(T - T_0)}{(T_1 - T_0)}$$

© Faith A. Morrison, Michigan Tech U.

**Example: When will my pipes freeze?**

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

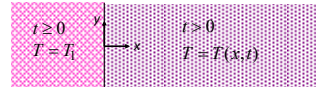
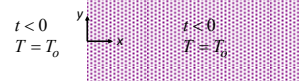
Or, use Excel. (How exactly?)

$$\frac{T - T_0}{T_1 - T_0} = \operatorname{erfc} \zeta - e^{\beta(2\zeta + \beta)} \operatorname{erfc}(\zeta + \beta)$$

$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

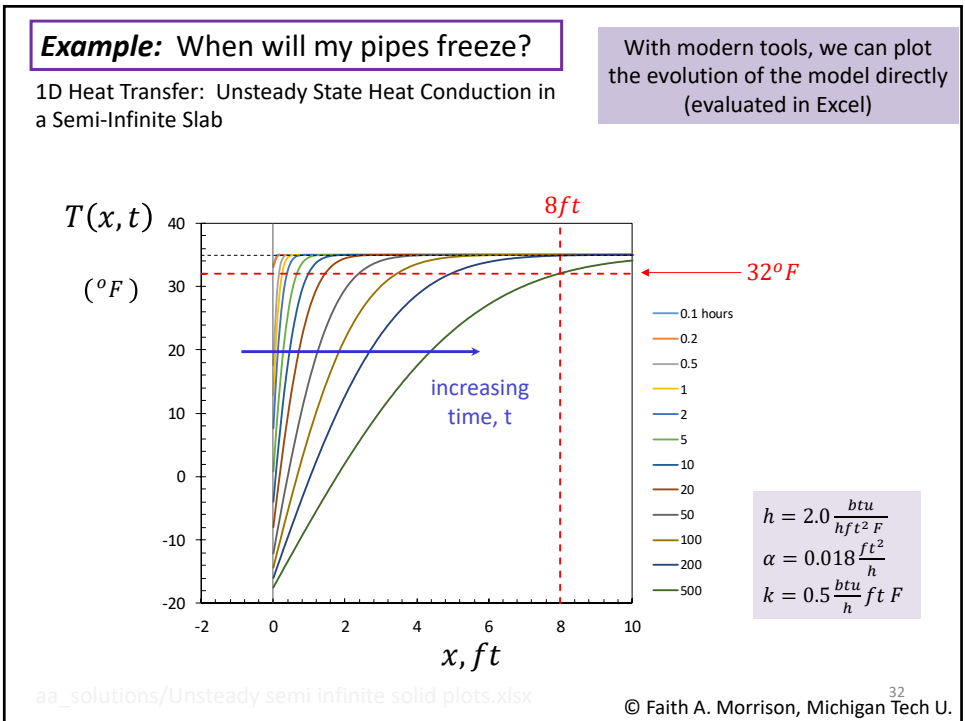
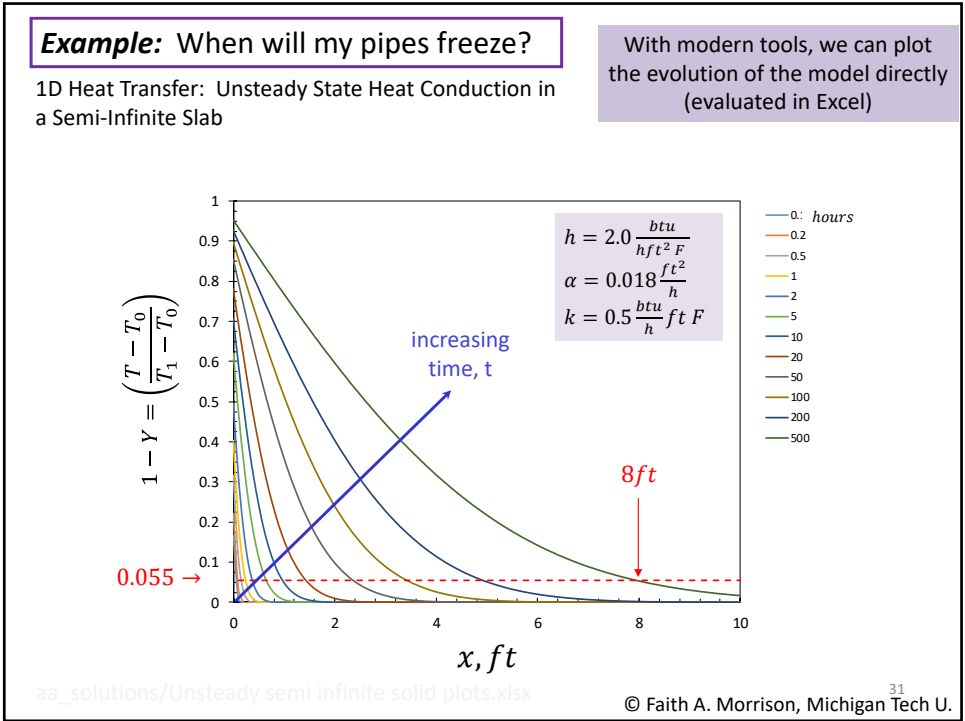
$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

You try.



T0=		
T1=		
T=		
h=		
alpha=		
k=		
x=		

**Answer:**  
 $t = 21.2 \text{ days}$   
 $\beta = 12.1$

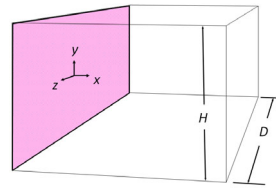
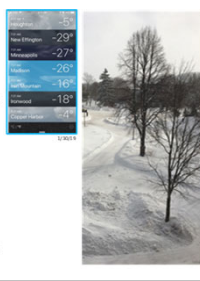




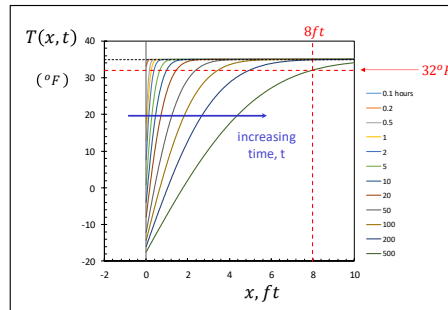
**Solution Summary:**

**Example:**  
When will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?



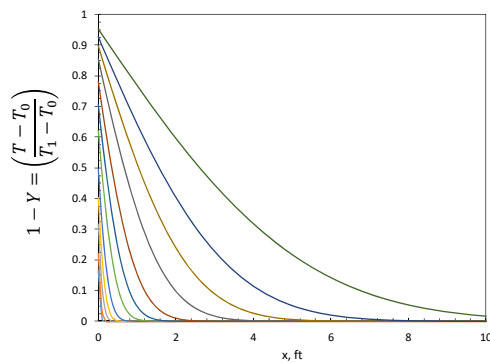
**Answer:**  
 $t = 509 \text{ hours} \approx 21 \text{ days}$



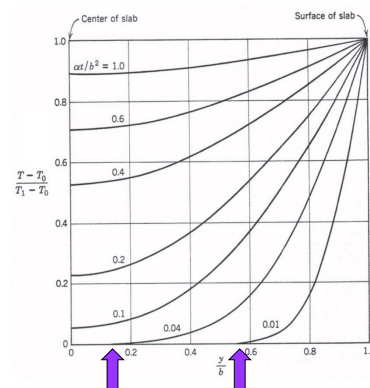
33  
© Faith A. Morrison, Michigan Tech U.

**Note:** We can use the semi-infinite slab solution for finite slabs, within limits

Semi-Infinite Slab



Finite Slab



BSL1, p356, 1960

For some cases, the finite slab looks semi-infinite

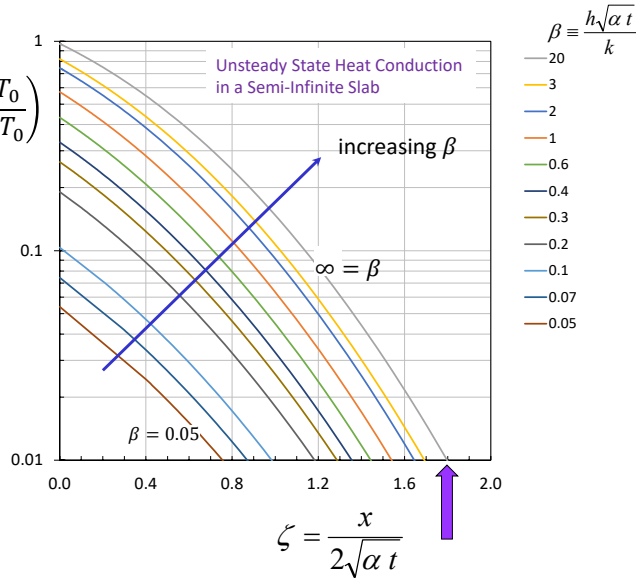
- Short time
- Thicker slab

34  
© Faith A. Morrison, Michigan Tech U.

**Note:** We can use the semi-infinite slab solution for finite slabs, within limits

$$1 - Y = \left( \frac{T - T_0}{T_1 - T_0} \right)$$

For values of  $\zeta(t, x)$  that predict  $T \approx T_0$  or  $(1 - Y) = 0.01$  at a distance equal to the half-slab thickness  $b$ , the semi-infinite slab solution is equivalent to the finite slab; this occurs  $\forall \beta$  when  $\zeta_{half-slab} = \frac{b}{2\sqrt{\alpha t}} > 1.8$



35

© Faith A. Morrison, Michigan Tech U.

**TAKEAWAY:**

We're not making the case that this ONE solution is so important to learn. . .

Rather, knowing that solutions are available, *and* being able to set up and walk yourself through the published graph (chart, plot, equation) to answer a question of interest, *is* an important engineering thinking skill.

**Example:** When will my pipes freeze?  
 The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft under ground?

**Example:** When will my pipes freeze?  
 1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$1 - Y = \left( \frac{T - T_0}{T_1 - T_0} \right)$$

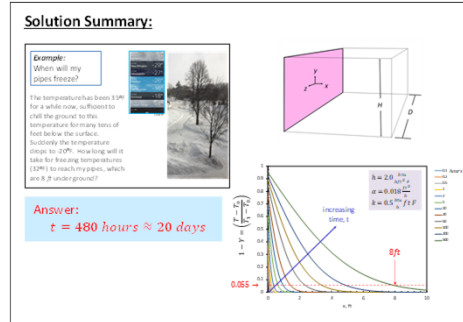
**Solution:**  
 Guess large  $\beta$   
 (Iterative solution)

Geankoplis 4<sup>th</sup> ed., Figure 5.3-3, page 364

36

© Faith A. Morrison, Michigan Tech U.

We used the **unsteady state microscopic energy balance** to solve one practical problem.



Next, we explore the **unsteady macroscopic energy balance**.

This adds another tool to our tool belt.