

## Done with Material Functions.

## What now?

**Chapter 5: Material Functions**

CM4650  
Polymer Rheology  
Michigan Tech

Steady Shear Flow Material Functions

**Imposed Kinematics:**

$$\underline{\underline{\dot{\gamma}}} = \begin{pmatrix} \dot{\gamma} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$\dot{\gamma}(t) = \dot{\gamma}_0 = \text{constant}$

**Material Stress Response:**

$\tau_{xy}(t)$  vs  $t$  and  $\tau_{xy}(t)$  vs  $\dot{\gamma}(t)$  plots.

**Material Functions:**

**Viscosity:**  $\eta(\dot{\gamma}) = \frac{\tau_{xy}}{\dot{\gamma}}$

**Flow normal stress coefficient:**  $\Psi_1(\dot{\gamma}) = \frac{\tau_{xx}}{\dot{\gamma}^2}$

**First normal stress difference:**  $N_1(\dot{\gamma}) = \frac{\tau_{xx} - \tau_{yy}}{\dot{\gamma}^2}$

**Second normal stress difference:**  $N_2(\dot{\gamma}) = \frac{\tau_{yy} - \tau_{zz}}{\dot{\gamma}^2}$

1. Intro
2. Vectors/tensors
3. Newtonian
4. Standard Flows
5. Material Functions
6. **Experimental Behavior**
7. Inelastic effects
8. Memory effects
9. Advanced
10. Rheometry



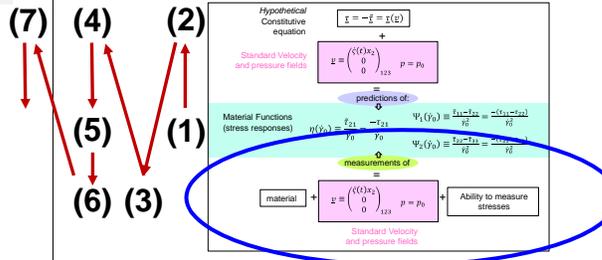
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## Investigating Stress/Deformation Relationships (Rheology)

### What are material functions and why do we need them?

For non-Newtonian fluids:

- We do not know the stress/deformation relationship ( $\underline{\underline{\tau}}(\underline{\underline{\dot{\gamma}}})$ )
- We approach stress/deformation investigations from two directions (**modeling**, **measuring**) to reveal the physics;
- Material functions organize comparisons



1. Choose a material function
2. Predict what Newtonian fluids would do
3. See what non-Newtonian fluids **do**
4. Hypothesize a  $\underline{\underline{\tau}}(\underline{\underline{\dot{\gamma}}})$
5. Predict the material function
6. Compare with what non-Newtonian fluids **do**
7. Reflect, **learn**, revise model, repeat.

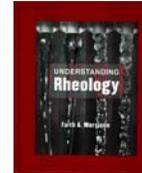
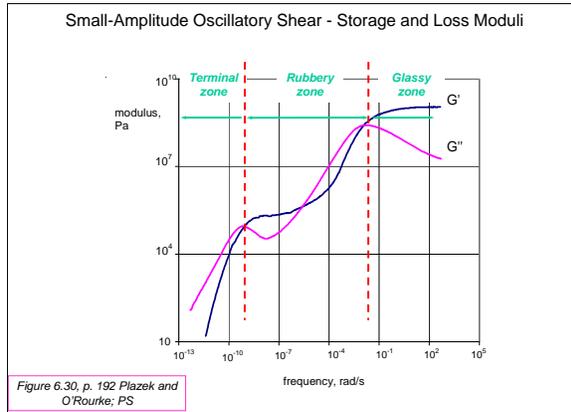
Let's focus more on material observations

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## Chapter 6: Experimental Data

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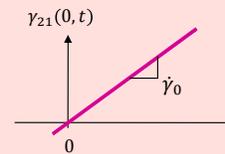
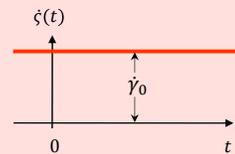
### Steady Shear Flow Material Functions



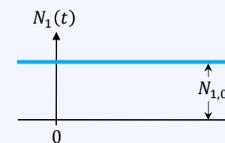
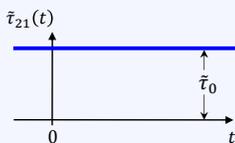
#### Imposed Kinematics:

$$\underline{v} \equiv \begin{pmatrix} \dot{\zeta}(t)x_2 \\ 0 \\ 0 \end{pmatrix}_{123}$$

$$\dot{\zeta}(t) = \dot{\gamma}_0 = \text{constant}$$



#### Material Stress Response:



#### Material Functions:

Viscosity  $\eta(\dot{\gamma}_0) \equiv \frac{\tilde{\tau}_{21}}{\dot{\gamma}_0} = \frac{-\tau_{21}}{\dot{\gamma}_0}$

First normal-stress coefficient

$$\Psi_1(\dot{\gamma}_0) \equiv \frac{\tilde{\tau}_{11} - \tilde{\tau}_{22}}{\dot{\gamma}_0^2} = \frac{-(\tau_{11} - \tau_{22})}{\dot{\gamma}_0^2}$$

Second normal-stress coefficient

$$\Psi_2(\dot{\gamma}_0) \equiv \frac{\tilde{\tau}_{22} - \tilde{\tau}_{33}}{\dot{\gamma}_0^2} = \frac{-(\tau_{22} - \tau_{33})}{\dot{\gamma}_0^2}$$

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Material Behavior Catalog (in terms of material functions)

## Experimental Data (Chapter 6)

First recipe card: **Steady shear flow** ➔

What do we observe for

- Linear Polymers
- Limits on measurability
- Material effects - MW, MWD, branching, mixtures, copolymers
- Temperature and pressure

**later ...** (the rest of the recipe cards)

*Unsteady shear flow (SAOS, step strain, start up, cessation)*

*Steady elongation*

*Unsteady elongation*

**Steady Shear Flow Material Functions**

**Imposed Kinematics:**  $\dot{\epsilon} = \begin{pmatrix} \dot{\gamma} & 0 \\ 0 & 0 \end{pmatrix}$ ,  $\dot{\gamma} = \dot{\gamma}_0 \sin(\omega t)$ ,  $\dot{\gamma}(t) = \dot{\gamma}_0 = \text{constant}$

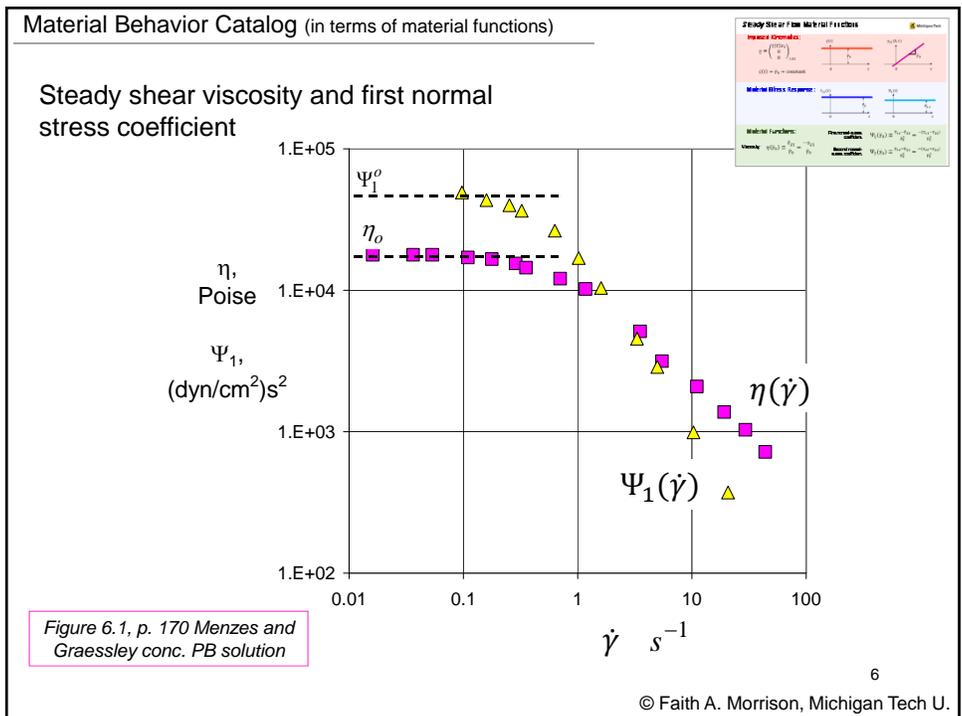
**Material Stress Response:**  $\tau_{xy}(t)$ ,  $\tau_{xx}(t)$ ,  $\tau_{yy}(t)$

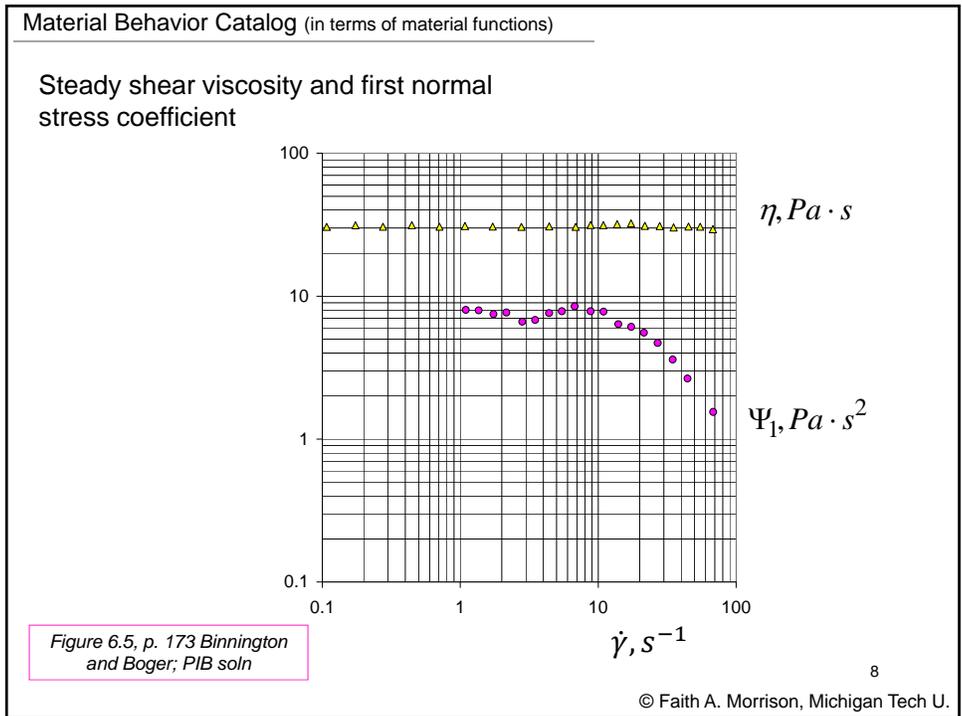
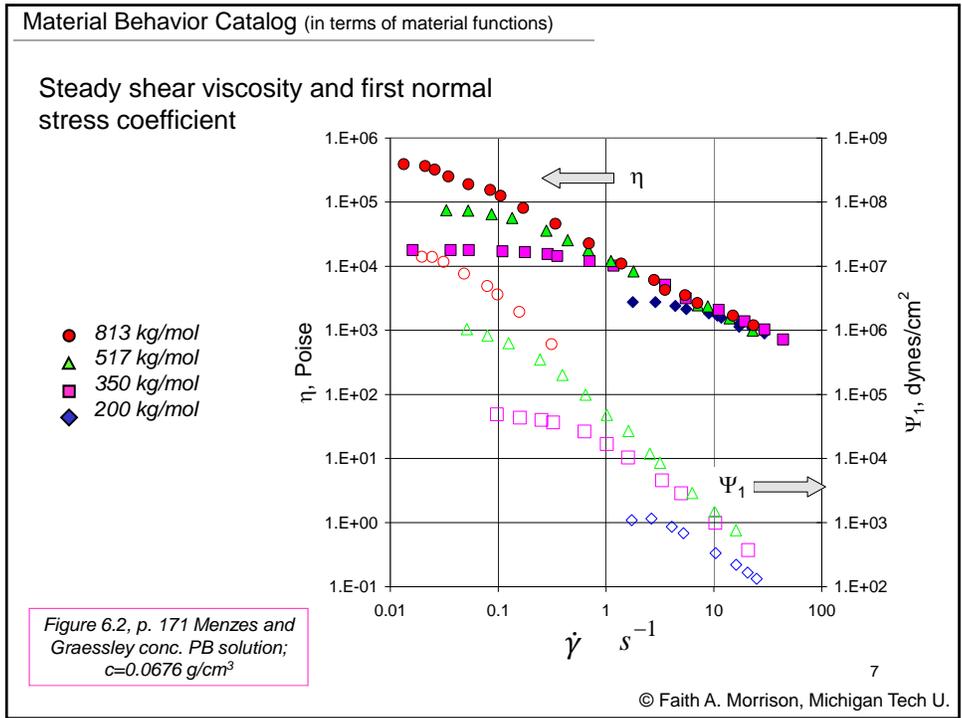
**Material Functions:**  $\eta(\dot{\gamma}) = \frac{\tau_{xy}}{\dot{\gamma}}$ ,  $\Psi_1(\dot{\gamma}) = \frac{\tau_{xx} - \tau_{yy}}{2\dot{\gamma}^2}$

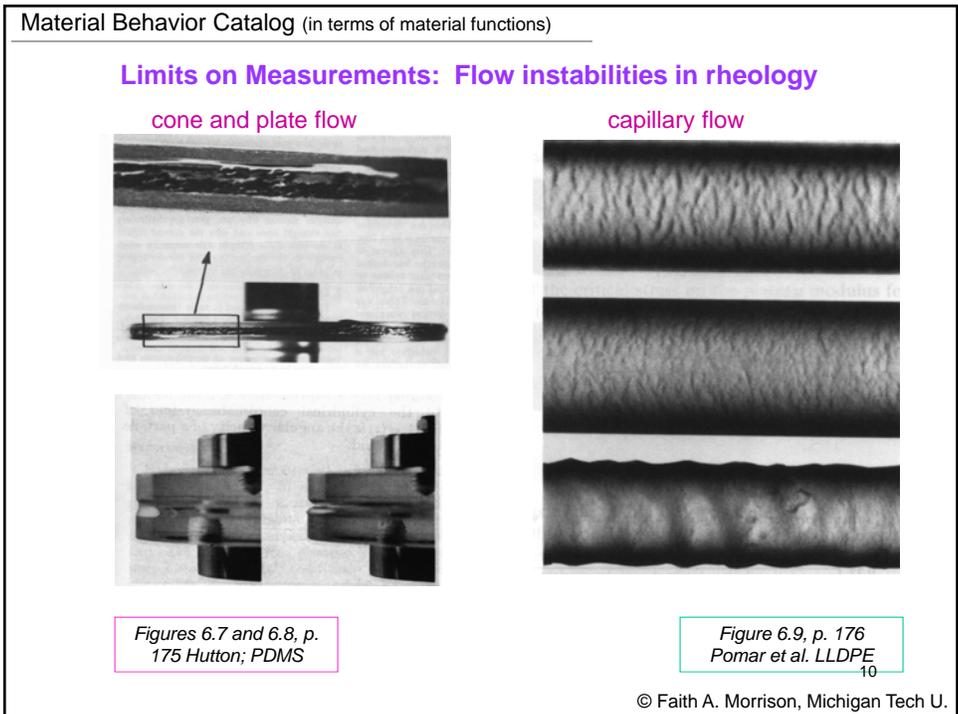
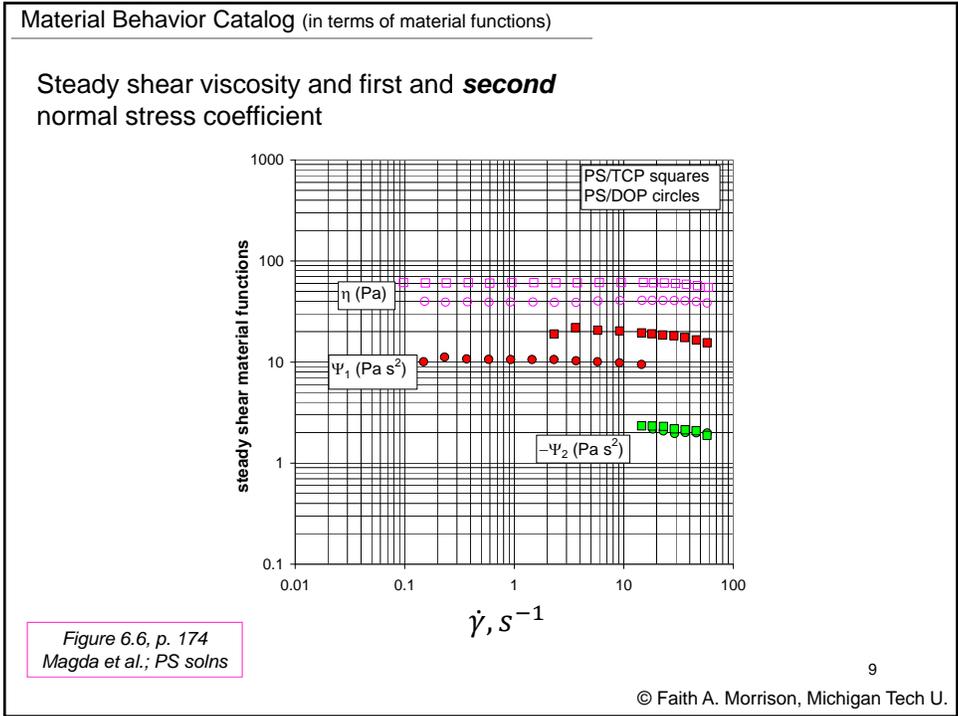
**Phenomenological constitutive equation:**  $\Psi_1(\dot{\gamma}) = \frac{1}{2} \frac{d\eta(\dot{\gamma})}{d\dot{\gamma}}$

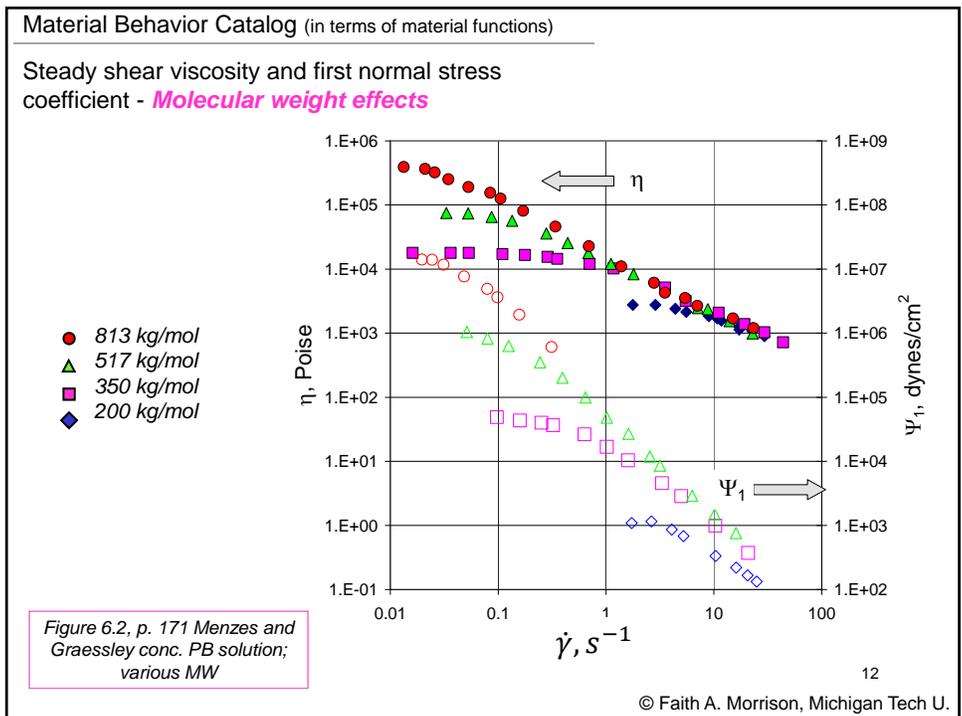
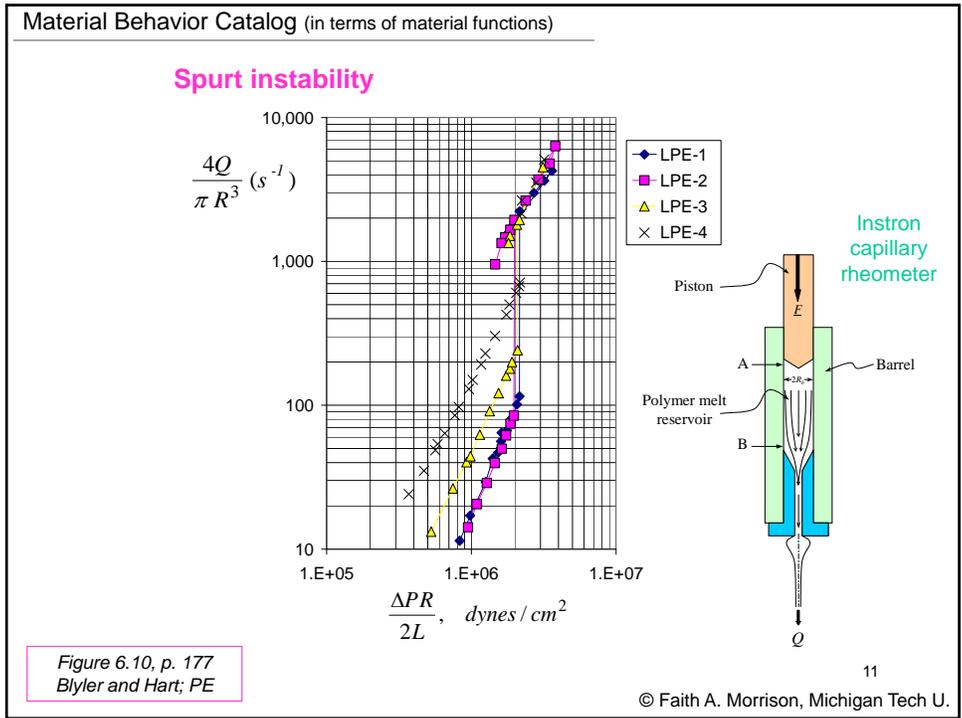
**General constitutive equation:**  $\Psi_2(\dot{\gamma}) = \frac{1}{2} \frac{d^2\eta(\dot{\gamma})}{d\dot{\gamma}^2}$

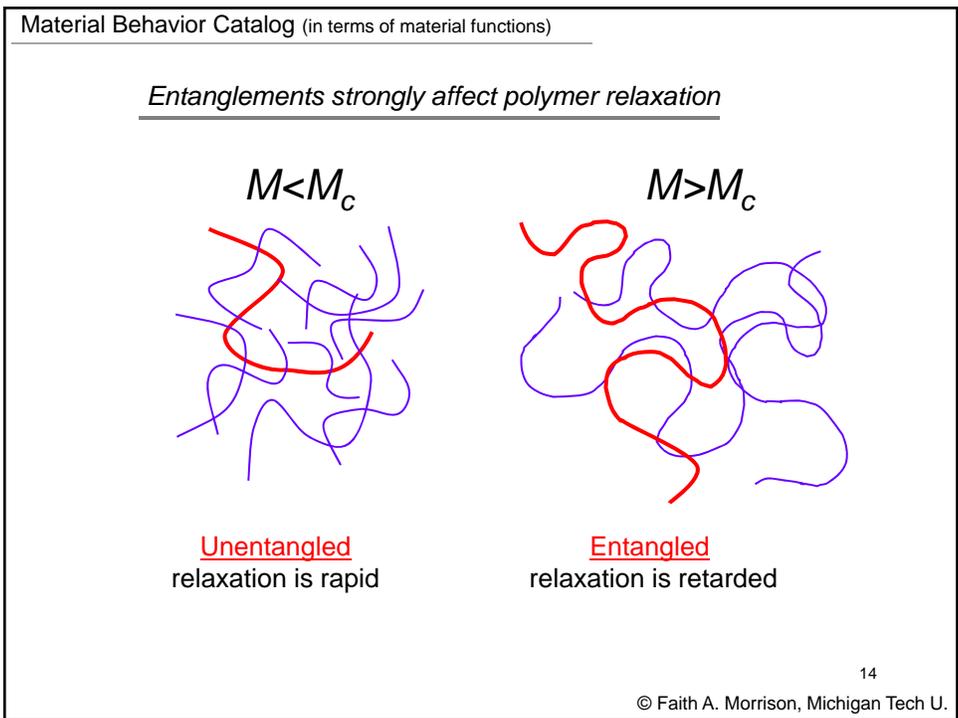
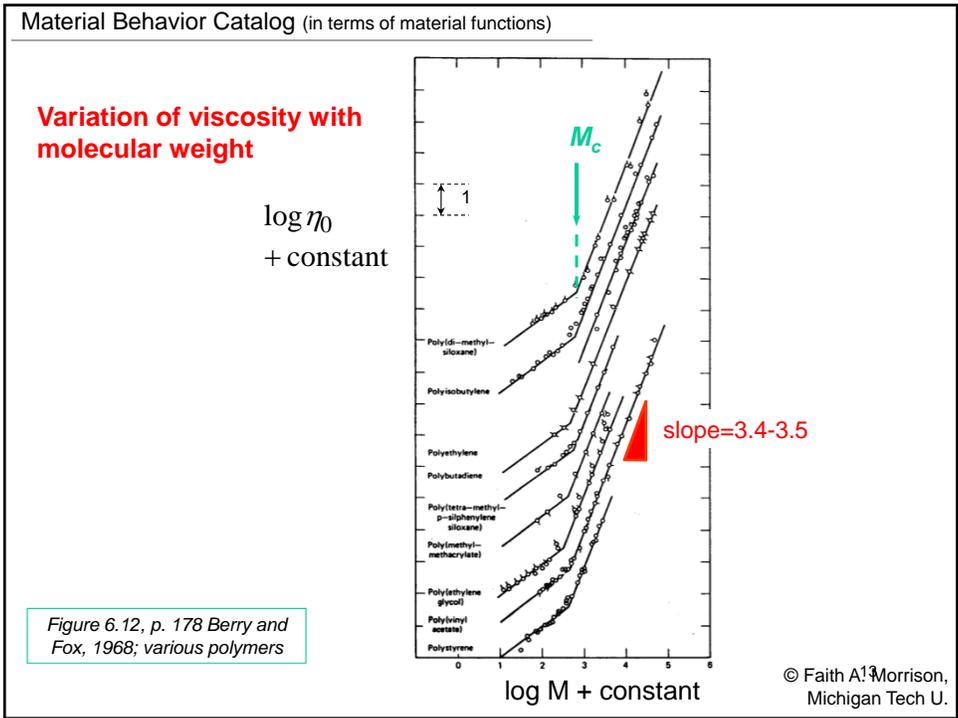
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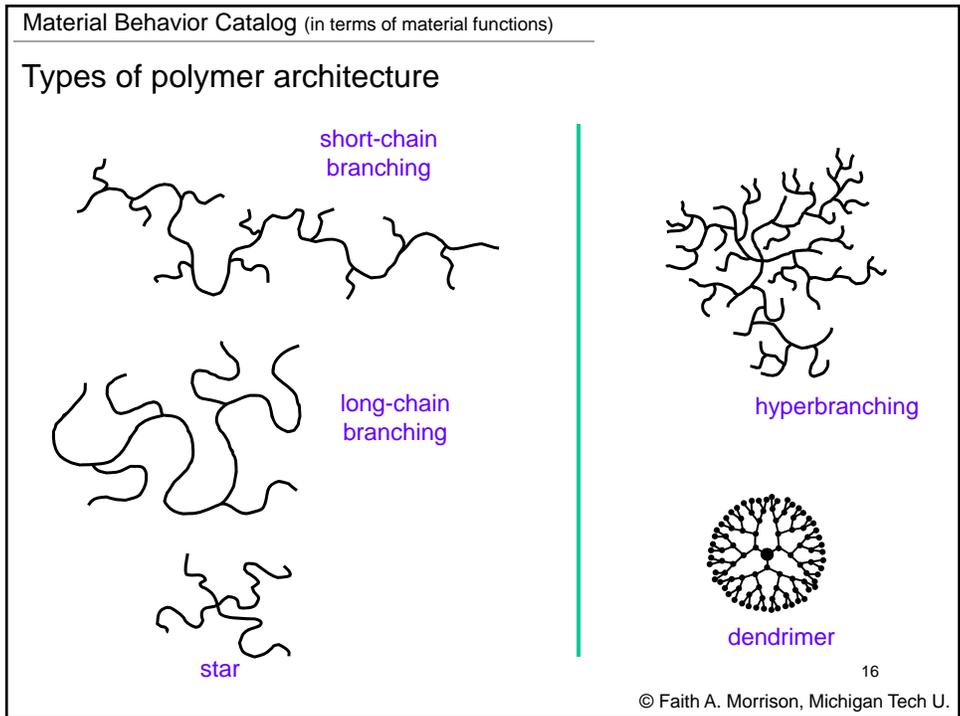
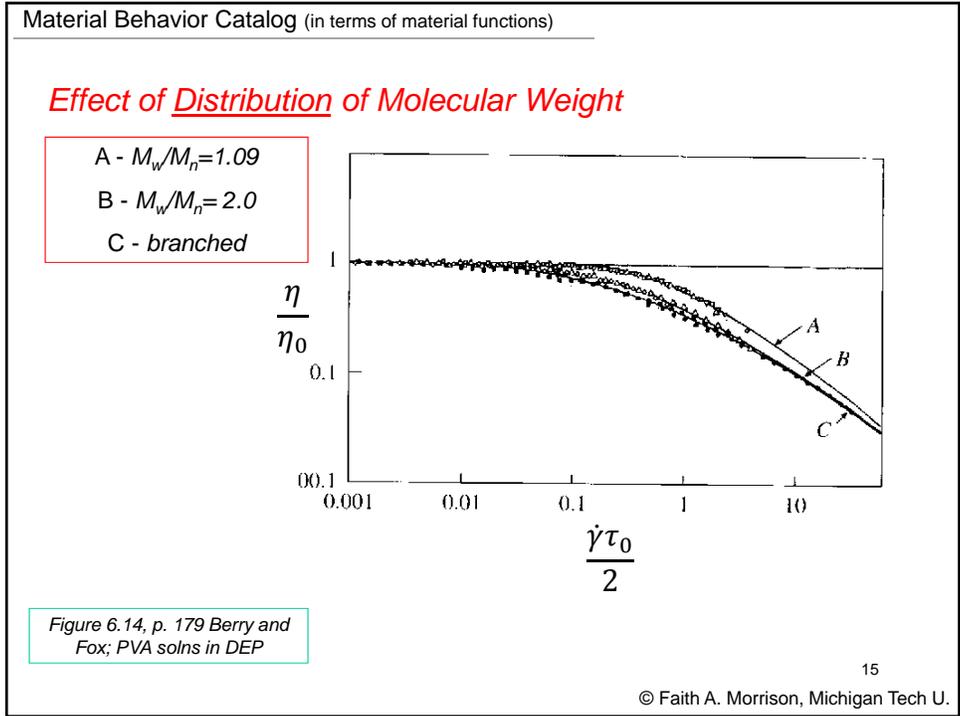


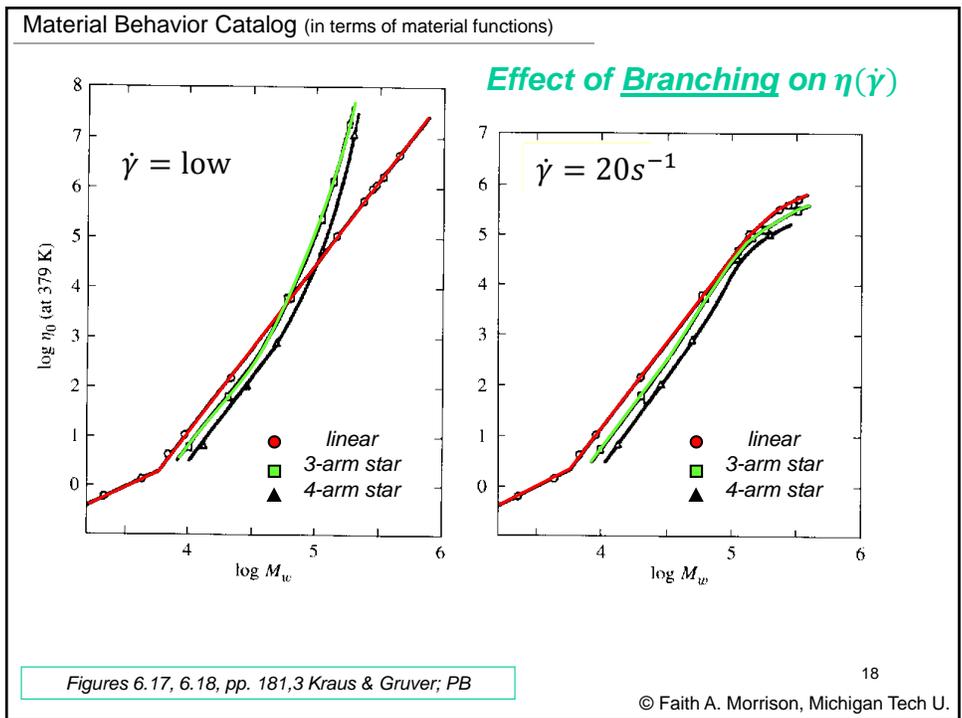
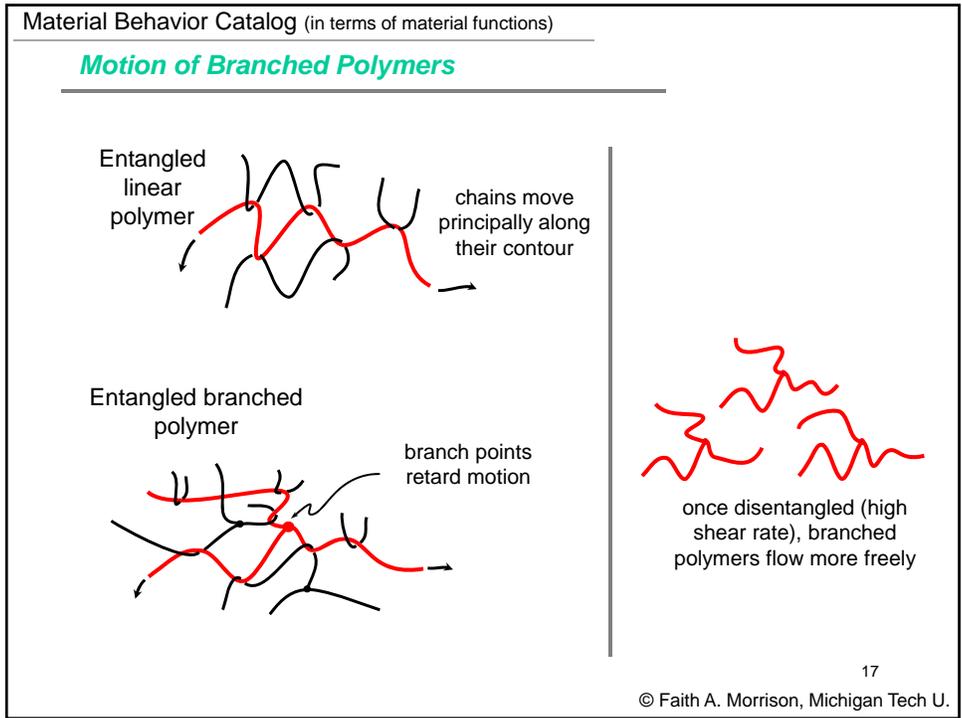




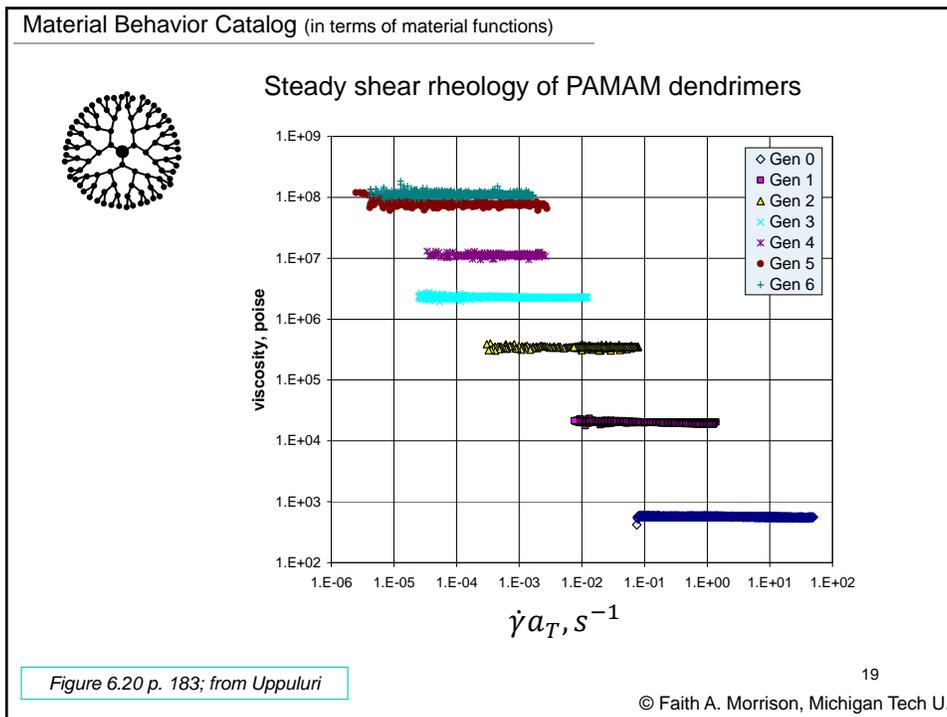








Figures 6.17, 6.18, pp. 181,3 Kraus & Gruver; PB



- Material Behavior Catalog (in terms of material functions)
- ### Steady Shear Summary:
1. General traits
  2. Effect of MW on linear polymers
  3. Effect of architecture
  4. Measurement issues
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Material Behavior Catalog (in terms of material functions)

Mixtures of Polymers with other materials - Filler Effect

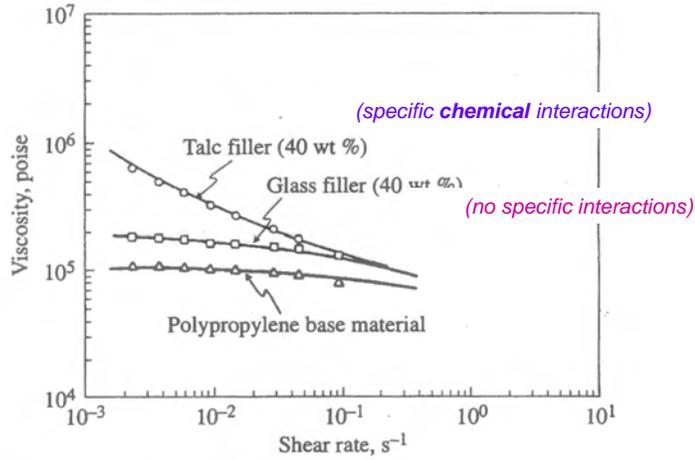


Figure 6.22, p. 184 Chapman and Lee; PP and filled PP

For more on filled systems, see Larson, *The Structure and Rheology of Complex Fluids*, Oxford, 1999.

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Material Behavior Catalog (in terms of material functions)

Mixtures of Polymers with other materials - Filler Effect

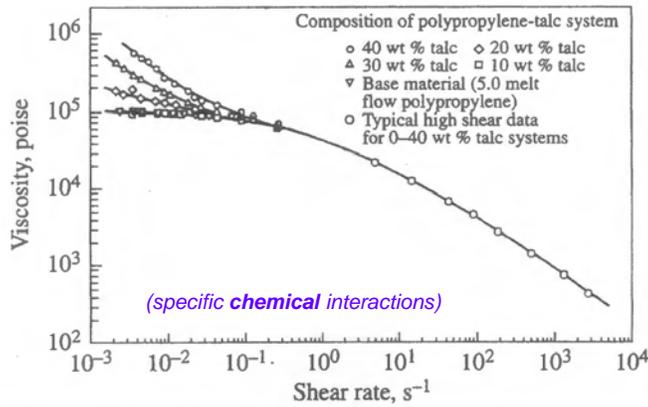
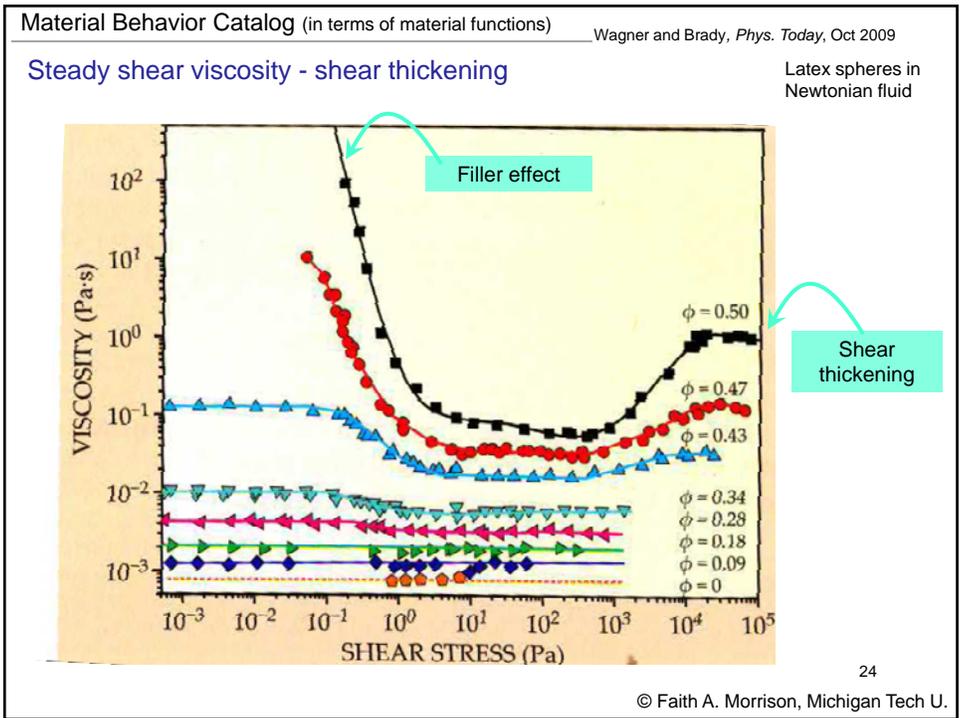
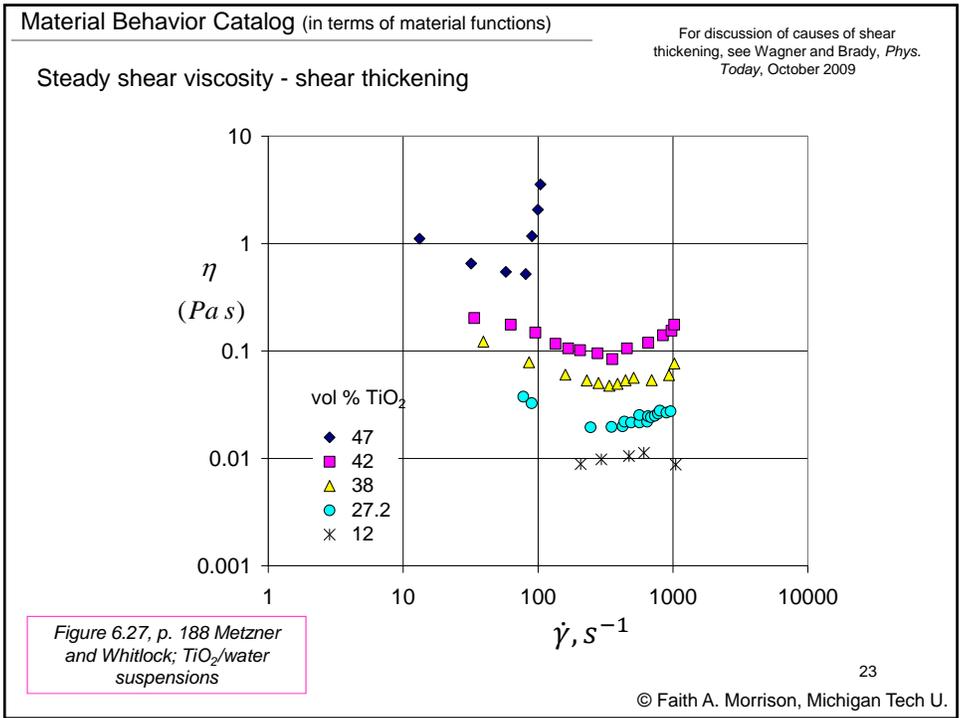


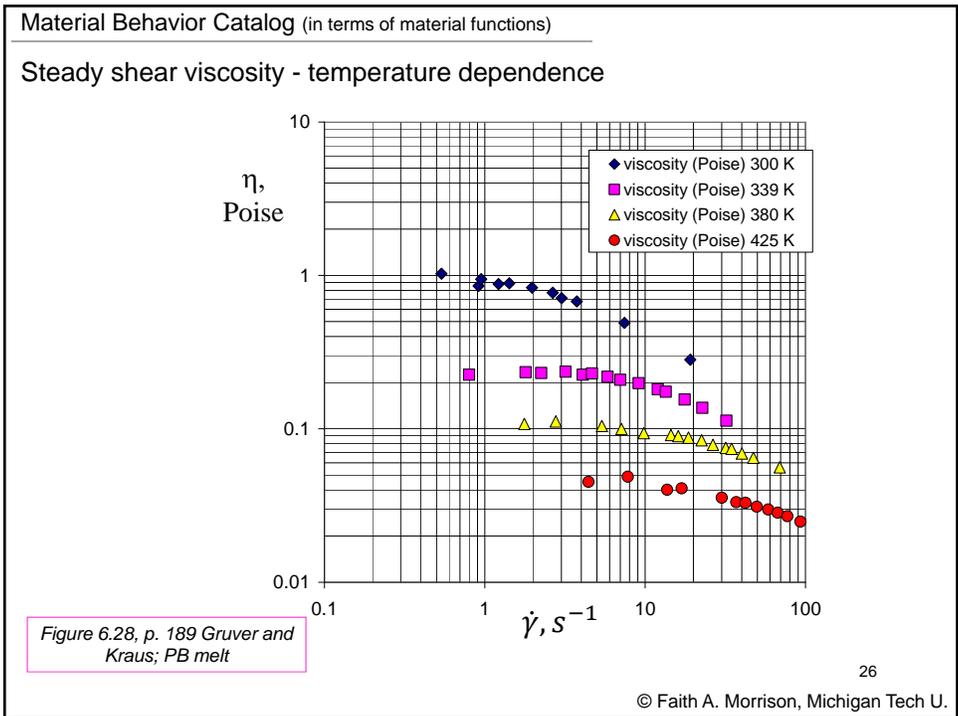
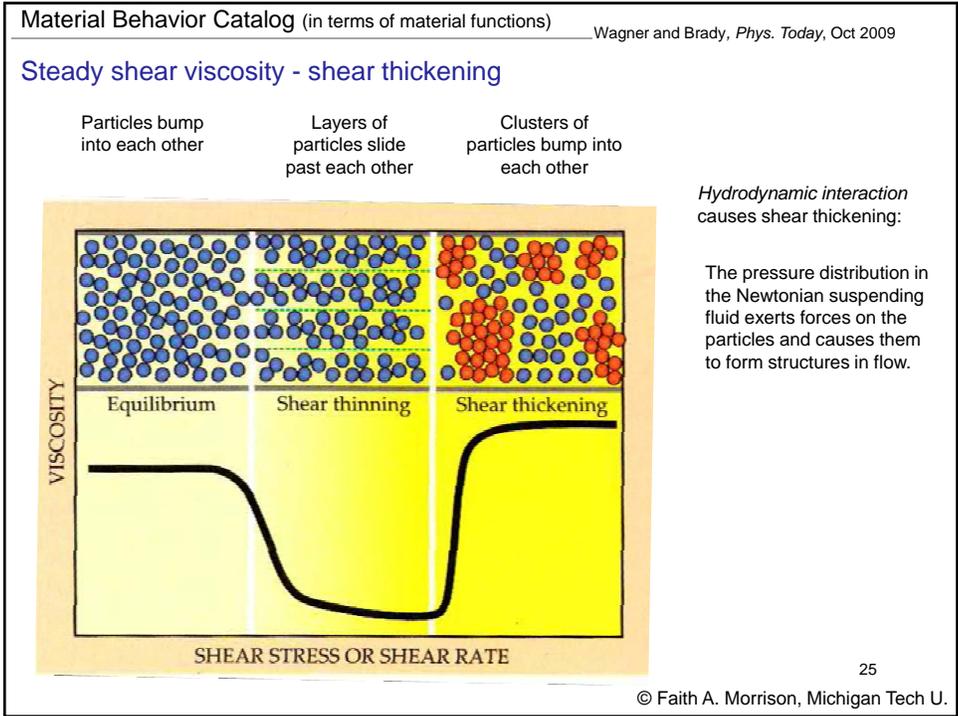
Figure 6.21, p. 184 Chapman and Lee; filled PP

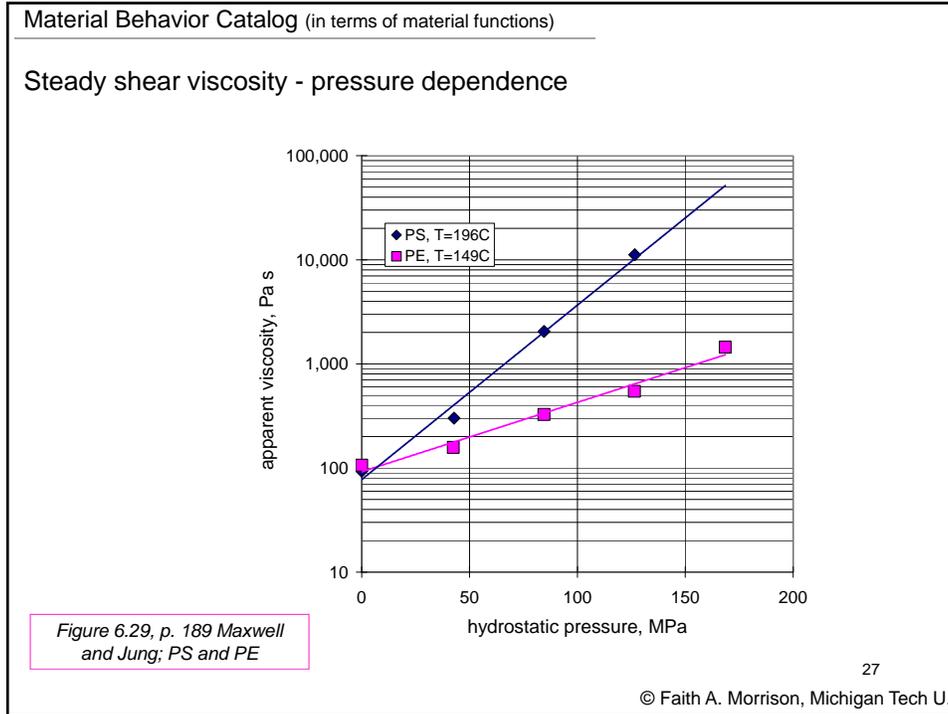
For more on filled systems, see Larson, *The Structure and Rheology of Complex Fluids*, Oxford, 1999.

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- Material Behavior Catalog (in terms of material functions)
- Steady Shear Summary:
1. General traits
  2. Effect of MW (linear polymers)
  3. Effect of architecture
  4. Measurement issues
  5. Effect of chemical composition
  6. Effect of temperature
  7. Effect of pressure
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Material Behavior Catalog (in terms of material functions)

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## Experimental Data (continues)

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**Next:**

- Unsteady shear flows (small and large strain)*
- Steady elongation*
- Unsteady elongation*

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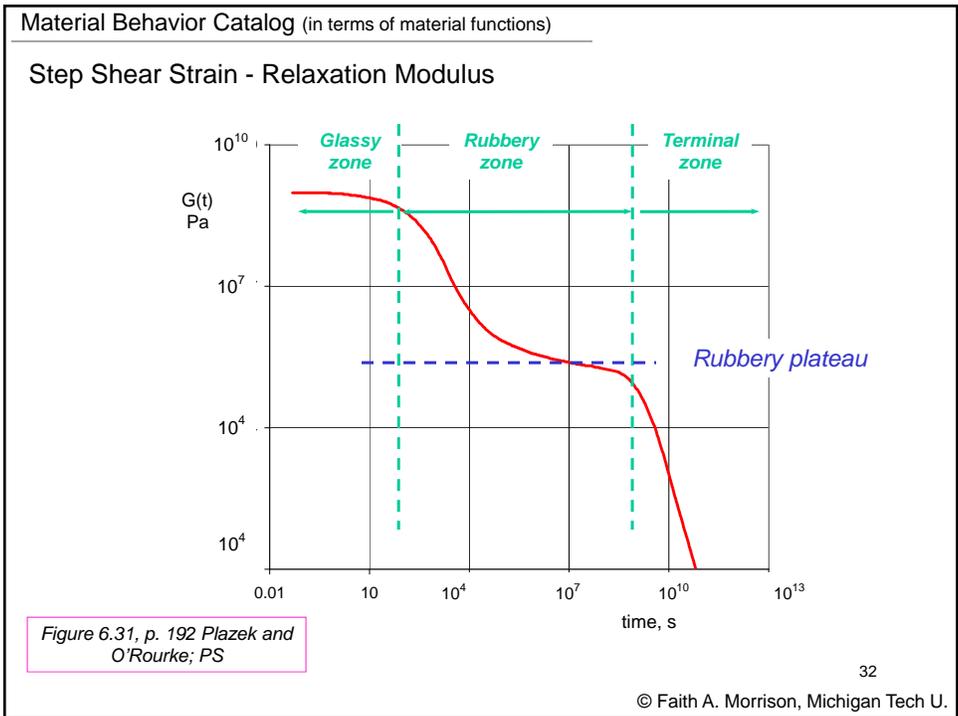
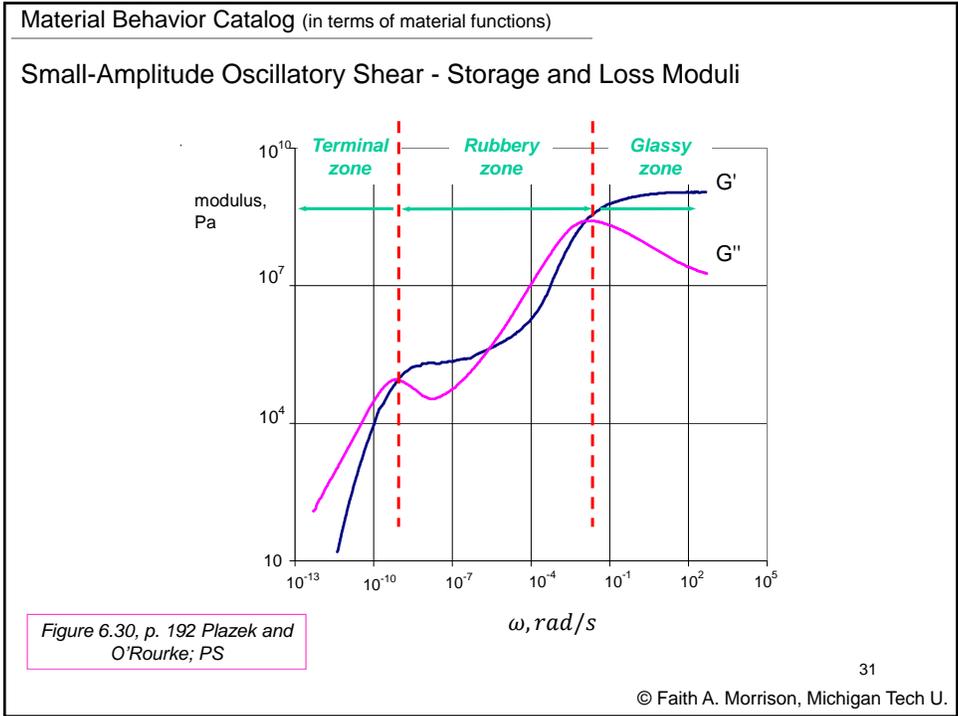
Material Behavior Catalog (in terms of material functions)

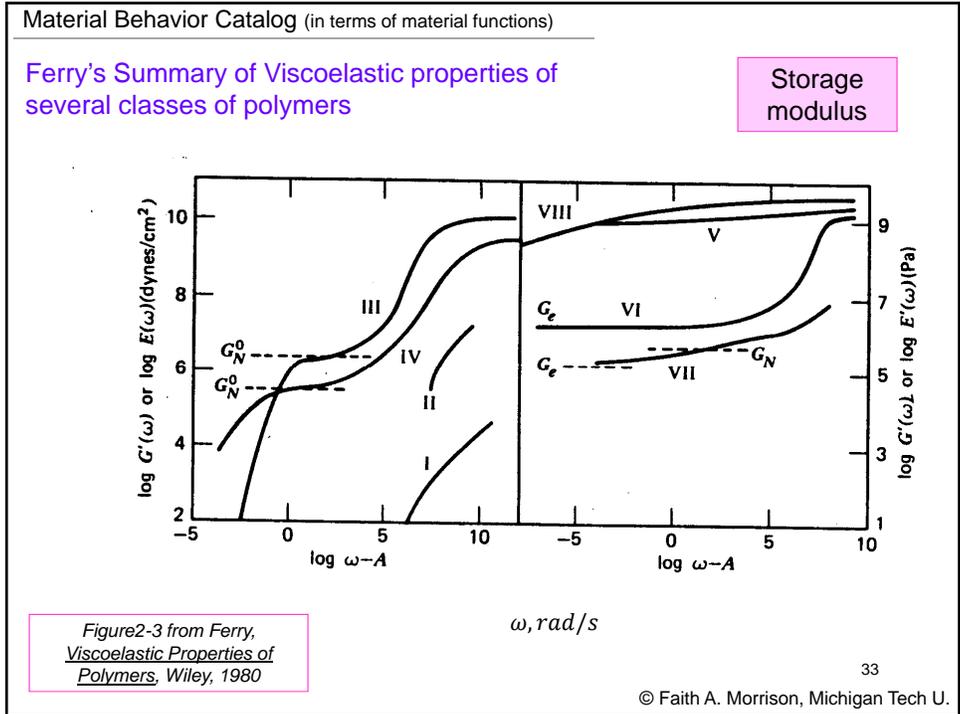
### Small-Amplitude Oscillatory Shear - Storage and Loss Moduli

Figure 6.30, p. 192 Plazek and O'Rourke; PS

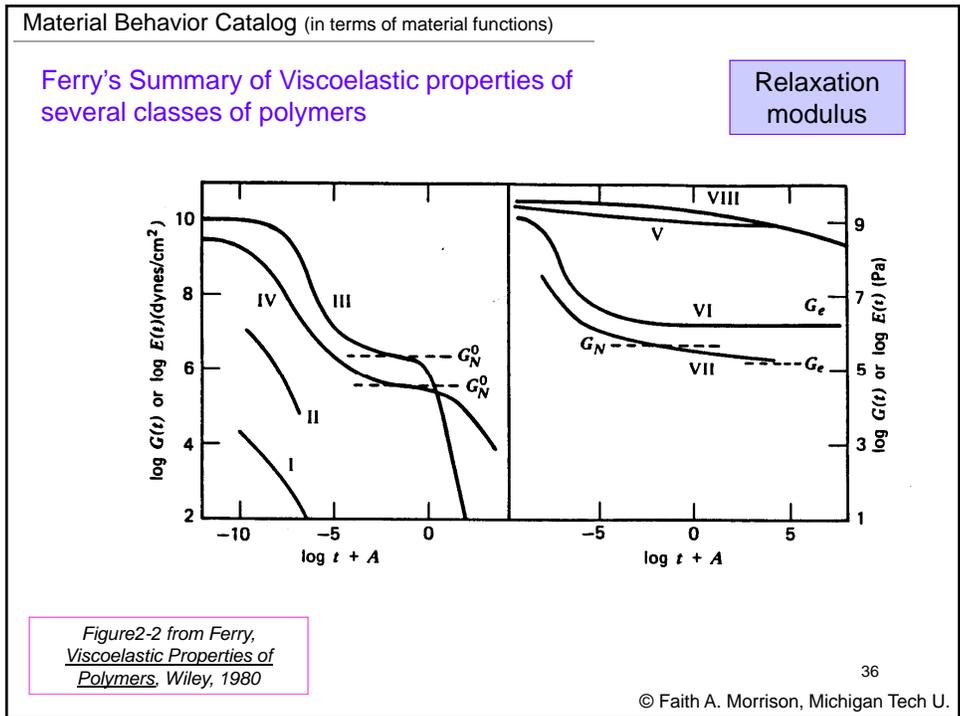
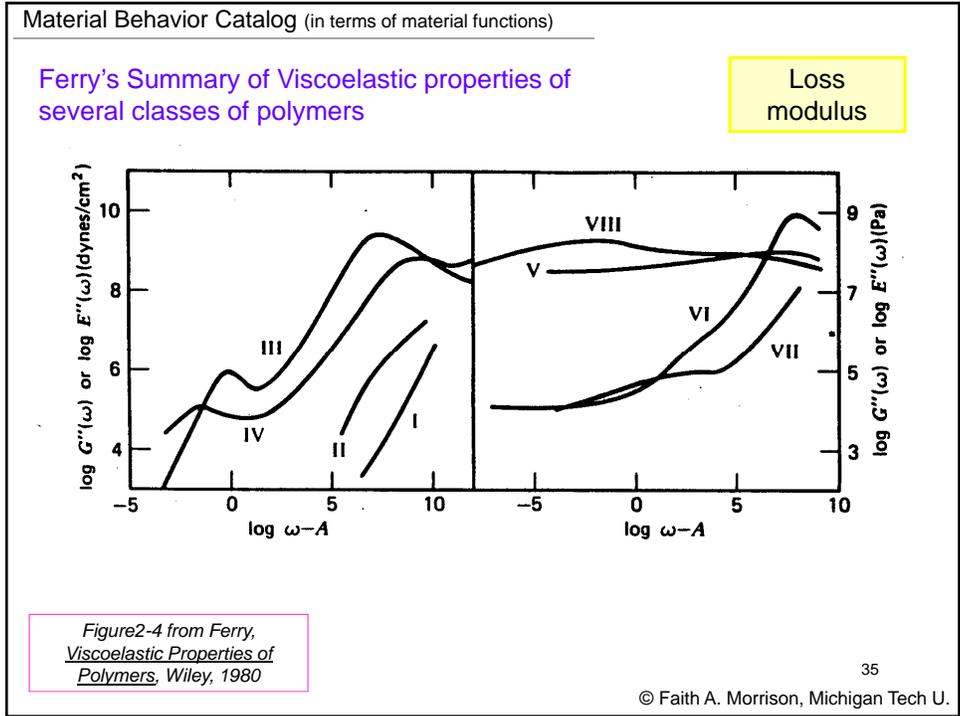
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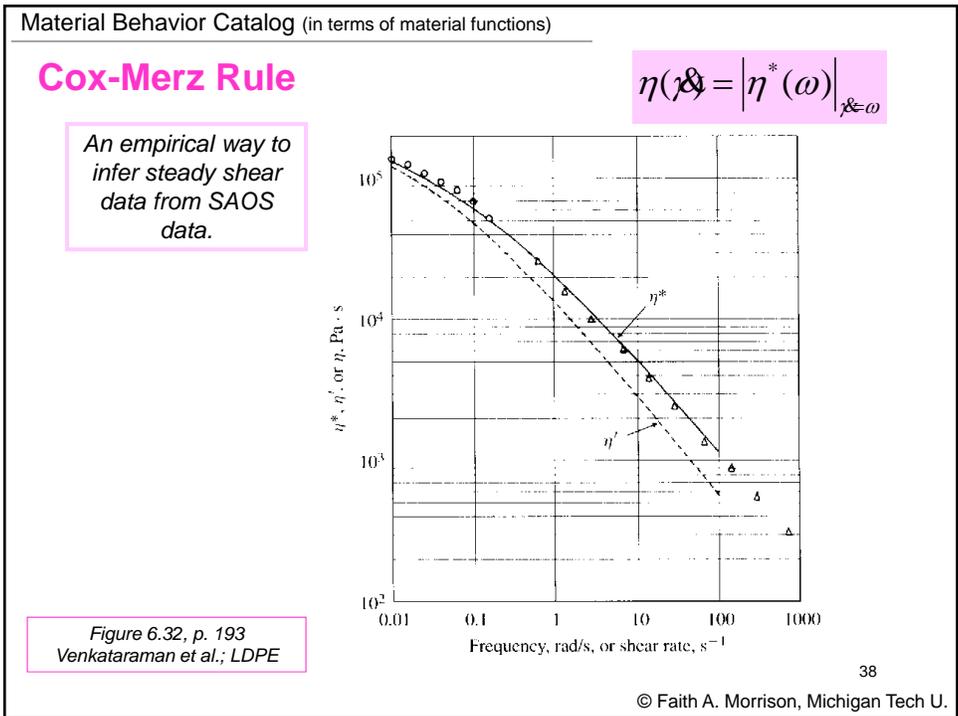
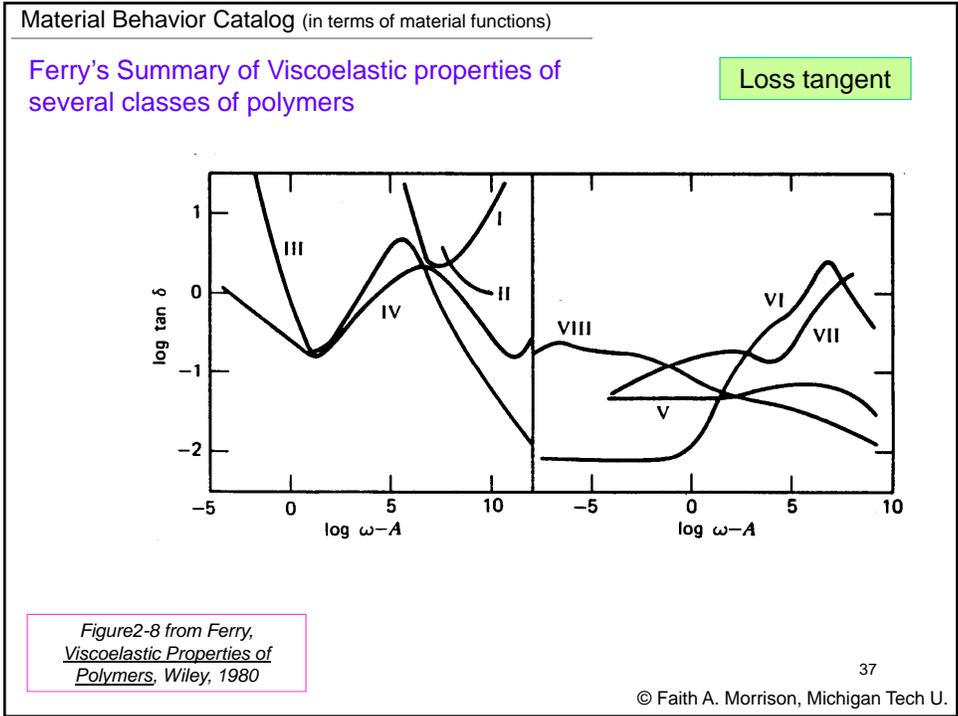
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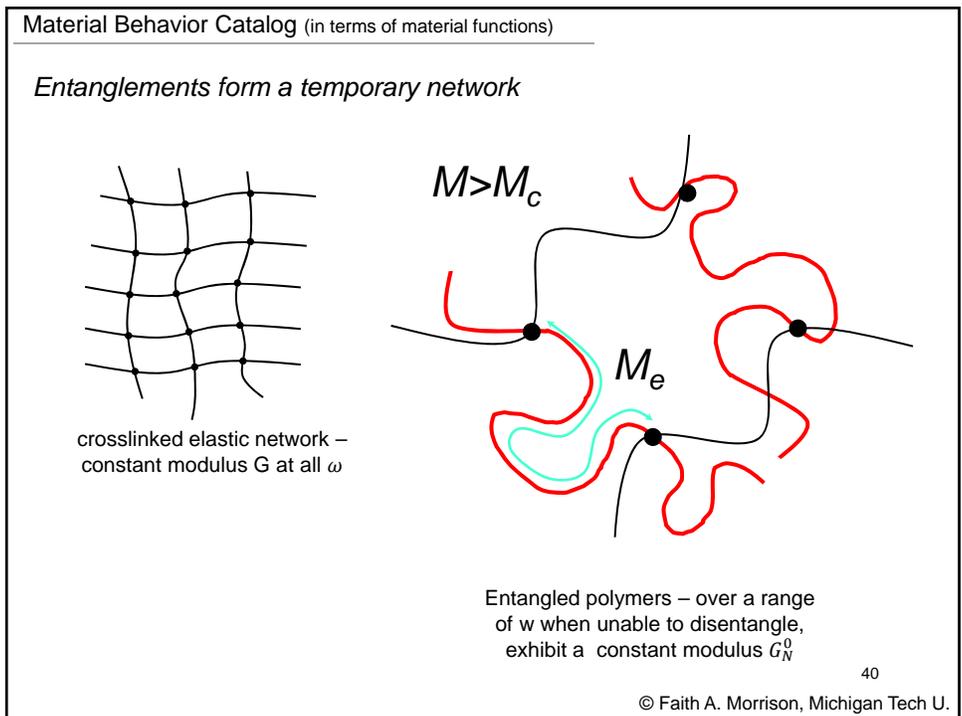
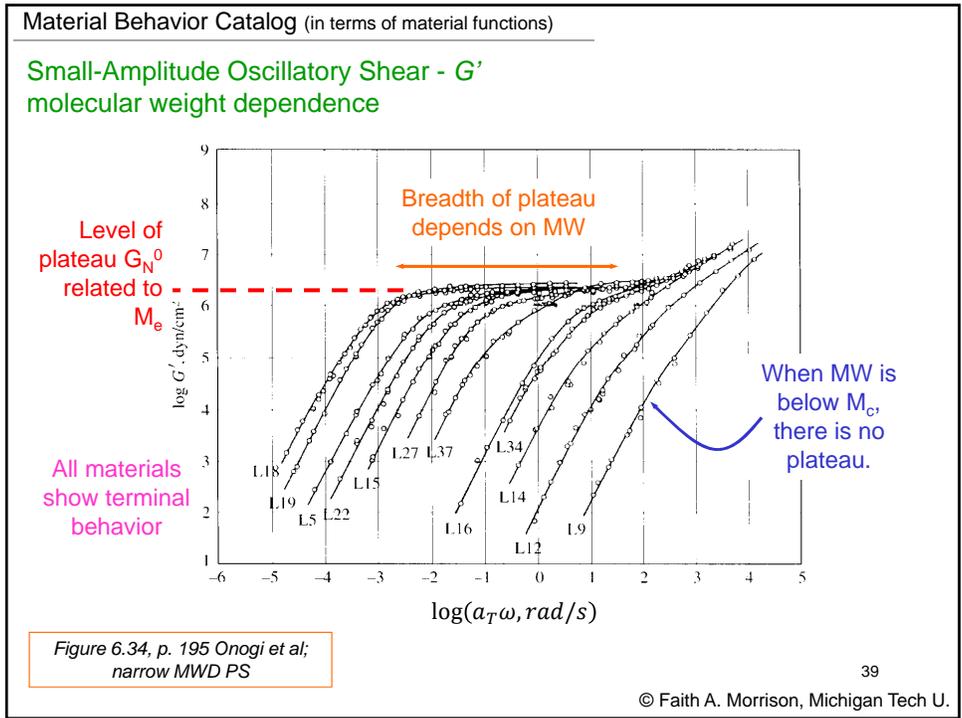




- Material Behavior Catalog (in terms of material functions)
- Key to Ferry's plots
- I. **Dilute polymer solutions: atactic polystyrene**, 0.015 g/ml in Aroclor 1248, a chlorinated diphenyl with viscosity 2.47 poise at 25°C.  $M_w=86,000$ ,  $M_w/M_n$  near 1.
  - II. **Amorphous polymer of low molecular weight**: poly(vinyl acetate),  $M=10,500$ , fractionated.
  - III. **Amorphous polymer of high molecular weight**: atactic polystyrene, narrow MW distribution,  $M_w=600,000$ .
  - IV. **Amorphous polymer of high molecular weight with long side groups**: fractionated poly(n-octyl methacrylate),  $M_w=3.62 \times 10^6$ .
  - V. **Amorphous polymer of high molecular weight below its glass transition temperature**: poly(methyl methacrylate).
  - VI. **Lightly cross-linked amorphous polymer**: lightly vulcanized Hevea rubber.
  - VII. **Very lightly cross-linked amorphous polymer**: styrene butadiene random copolymer, 23.5% styrene by weight.
  - VII. **Highly crystalline polymer**: linear polyethylene.
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Material Behavior Catalog (in terms of material functions)

Small-Amplitude Oscillatory Shear -  $G'$   
molecular weight dependence

Level of plateau  $G_N^0$  is related to  $M_e$   
(molecular theory for temporary networks)

$$G_N^0 = \frac{4}{5} \nu k_B T$$

$\nu$  = density of effective cross links  
 $\nu$  = cross links/volume

$$M_e = \frac{\left(\frac{\text{mass}}{\text{volume}}\right) \left(\frac{\text{crosslinks}}{\text{mole}}\right)}{\left(\frac{\text{crosslinks}}{\text{volume}}\right)} = \frac{\rho N_A}{\nu}$$

$$M_c \cong 2M_e$$

$$G_N^0 = \frac{4}{5} \frac{\rho N_A k_B T}{M_e}$$

Larger the MW between entanglements, the softer the network

See Larson, *The Structure and Rheology of Complex Fluids*, Oxford, 1999

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Material Behavior Catalog (in terms of material functions)

Small-Amplitude Oscillatory Shear -  $G''$   
molecular weight dependence

Breadth of minimum depends on MW; structure is more complex

When MW is below  $M_c$ , there is no minimum.

All materials show terminal behavior

Figure 6.36, p. 196 Onogi et al; narrow MWD PS

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Material Behavior Catalog (in terms of material functions)

Small-Strain Unsteady Shear Summary:

1. General traits
2. Effect of MW (linear polymers)
3. Effect of architecture
4. Relationship to steady flow material functions
5. Measurement issues
6. Effect of chemical composition

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Material Behavior Catalog (in terms of material functions)

Small-Amplitude Oscillatory Shear -  $G'$  as a function of temperature for copolymers

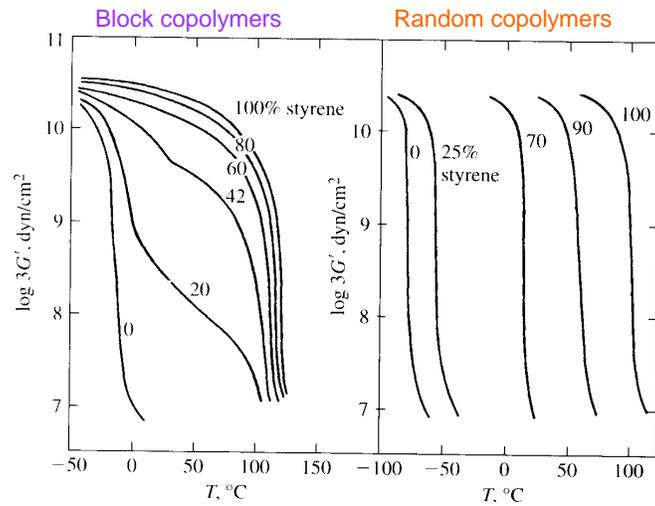
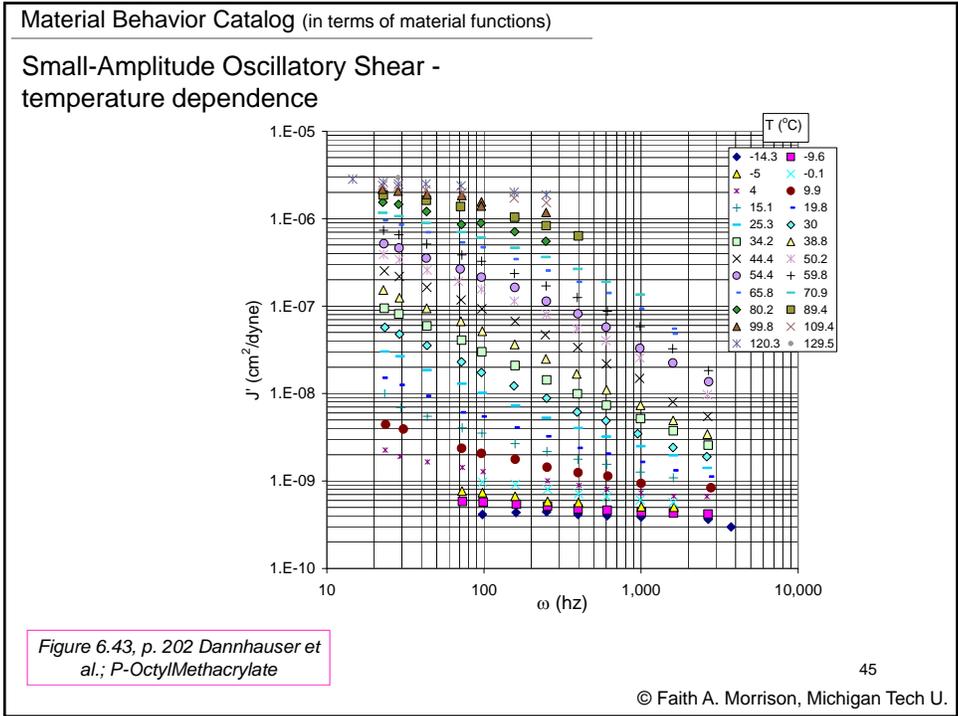


Figure 6.39, p. 198 Cooper and Tobolsky; SIS block and SBS random

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Material Behavior Catalog (in terms of material functions)

*Time-Temperature Superposition*

Material functions depend on  $g_i, l_i$

$$G' = G'(\omega, \lambda_i, g_i)$$

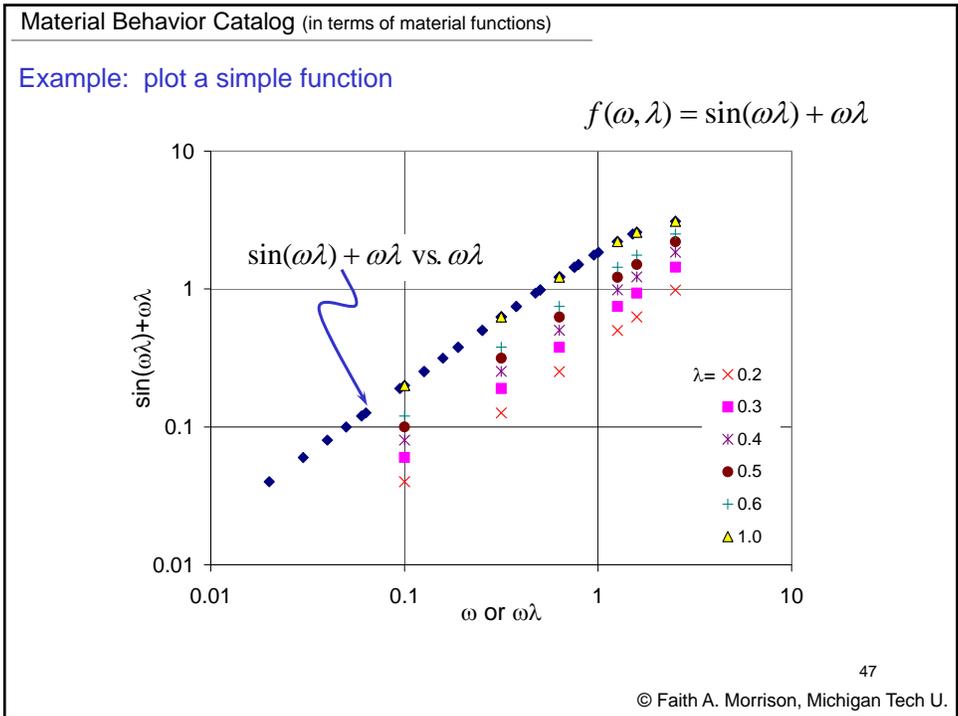
$$G'' = G''(\omega, \lambda_i, g_i)$$

$g_i, l_i$  are in turn functions of temperature and material properties

*Theoretical result:* in the linear-viscoelastic regime, material functions are a function of  $w/l_i$  rather than of  $w$  and  $l_i$  individually.

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Material Behavior Catalog (in terms of material functions)

In general,

$$G' = G'(\omega\lambda_1(T), \omega\lambda_2(T), \omega\lambda_3(T), K \quad )$$

Suppose that the temperature-dependence of  $l_i$  could be factored out. Let  $a_{Ti}(T)$  be the temperature-dependence of  $l_i$ .

$$\lambda_i(T) = a_{Ti}(T)\tilde{\lambda}_i$$

not a function of temperature

Then we could group the temperature-dependence function with the frequency.

$$G' = G'(a_{T1}\omega\tilde{\lambda}_1, a_{T2}\omega\tilde{\lambda}_2, a_{T3}\omega\tilde{\lambda}_3, K \quad )$$

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Material Behavior Catalog (in terms of material functions)

**Time-Temperature Superposition**

- Relaxation times decrease strongly as temperature increases
- Moduli associated with relaxations are proportional to absolute temperature; depend on density

*Empirical observation:* for many materials, all the relaxation times and moduli have the same functional dependence on temperature

(for the  $i^{\text{th}}$  relaxation mode)

$$\lambda_i(T) = \tilde{\lambda}_i a_T(T)$$

temperature dependence of all relaxation times

$$g_i(T) = \tilde{g}_i T \rho(T)$$

temperature dependence of all moduli

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Material Behavior Catalog (in terms of material functions)

*Second theoretical result:* the  $g_i$  enter into the functions for  $G'$ ,  $G''$  such that  $T\rho$  can be factored out of the function

$$\frac{G'}{T\rho} = \tilde{f}(a_T \omega, \tilde{\lambda}_i)$$

$$\frac{G''}{T\rho} = \tilde{h}(a_T \omega, \tilde{\lambda}_i)$$

Therefore if we plot reduced variables, we can suppress all of the temperature dependence of the moduli.

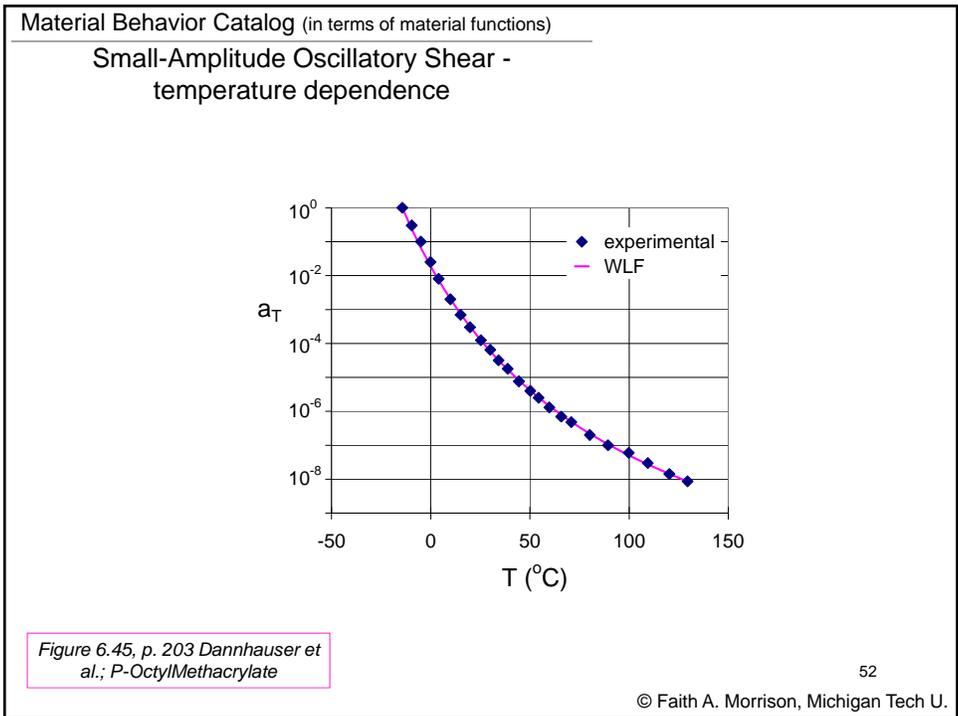
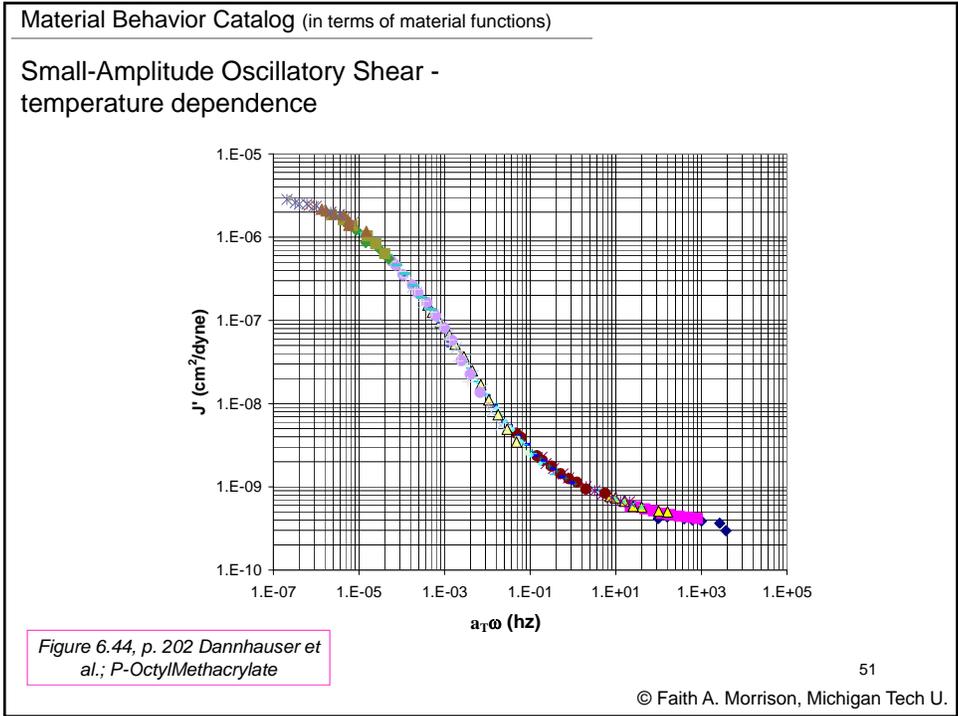
$$G'_r \equiv \frac{G'(T) T_{ref} \rho_{ref}}{T\rho} = f(a_T \omega, \tilde{\lambda}_i) T_{ref} \rho_{ref} = G'(T_{ref})$$

$$G''_r \equiv \frac{G''(T) T_{ref} \rho_{ref}}{T\rho} = h(a_T \omega, \tilde{\lambda}_i) T_{ref} \rho_{ref} = G''(T_{ref})$$

Plots of  $G'_r, G''_r$  versus  $a_T \omega$  will therefore be independent of temperature.

(will still depend on the material through the  $\tilde{\lambda}_i$ )

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Material Behavior Catalog (in terms of material functions)

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## Shift Factors

Arrhenius equation

$$a_T = \exp\left[\frac{-\Delta H}{R}\left(\frac{1}{T} - \frac{1}{T_{ref}}\right)\right]$$

found to be valid for  $T > T_g + 100^\circ C$

Williams-Landel-Ferry (WLF) equation

$$\log a_T = \frac{-c_1^0(T - T_{ref})}{c_2^0 + (T - T_{ref})}$$

found to be valid w/in  $100^\circ C$  of  $T_g$

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Material Behavior Catalog (in terms of material functions)

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### Shifting other Material Functions

Other linear viscoelastic material functions:

$$\eta' \equiv \frac{G''(T)}{\omega}$$

$$\eta'' \equiv \frac{G'(T)}{\omega}$$

$$\tan \delta = \frac{G''}{G'}$$

$$J' = \frac{1/G'}{1 + \tan^2 \delta}$$

$$J'' = \frac{1/G''}{1 + (\tan^2 \delta)^{-1}}$$

$$G'_r \equiv \frac{G'(T)T_{ref}\rho_{ref}}{T\rho} = f(a_r, \omega, \tilde{\lambda}_i)T_{ref}\rho_{ref} = G'(T_{ref})$$

$$G''_r \equiv \frac{G''(T)T_{ref}\rho_{ref}}{T\rho} = h(a_r, \omega, \tilde{\lambda}_i)T_{ref}\rho_{ref} = G''(T_{ref})$$

Independent of temperature

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Material Behavior Catalog (in terms of material functions)

**Shifting other Material Functions**

*linear viscoelastic*

$$\eta'_r \equiv \frac{G''(T)T_{ref}\rho_{ref}}{a_T\omega T\rho} = \frac{\eta'(T_{ref})T_{ref}\rho_{ref}}{a_T T\rho}$$

$$\eta''_r \equiv \frac{G'(T)T_{ref}\rho_{ref}}{a_T\omega T\rho} = \frac{\eta''(T_{ref})T_{ref}\rho_{ref}}{a_T T\rho}$$

$$J'_r \equiv \frac{J'(T)T\rho}{T_{ref}\rho_{ref}}$$

$$J''_r \equiv \frac{J''(T)T\rho}{T_{ref}\rho_{ref}}$$

*steady shear*

$$\eta_r(a_T\dot{\gamma}) = \frac{\eta(T)T_{ref}\rho_{ref}}{a_T T\rho}$$

$\tan \delta = \frac{G''}{G'}$ 
  
 = independent of temperature when plotted versus reduced frequency)

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Material Behavior Catalog (in terms of material functions)

**Steady shear viscosity - Temperature dependence**

Figure 6.46, p. 204 Gruber and Kraus; PB melt

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Material Behavior Catalog (in terms of material functions)

Another consequence of  $\lambda_i(T) = \tilde{\lambda}_i a_T(T)$  is the similarity between  $\log G'(\omega)$  and  $\log G'(T)$ .

Figure 6.30, p. 192 Plazek and O'Rourke; PS

Figure 6.39, p. 198 Cooper and Tobolsky; SIS block and SBS random

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Material Behavior Catalog (in terms of material functions)

Take data for  $G'$ ,  $G''$  at a fixed  $\omega$  for a variety of  $T$ .

$$G'_r \equiv \frac{G'(T)T_{ref} \rho_{ref}}{T\rho} = f(a_T \omega, \tilde{\lambda}_i)$$

but, what is  $a_T(T)$ ?  
We do not know.

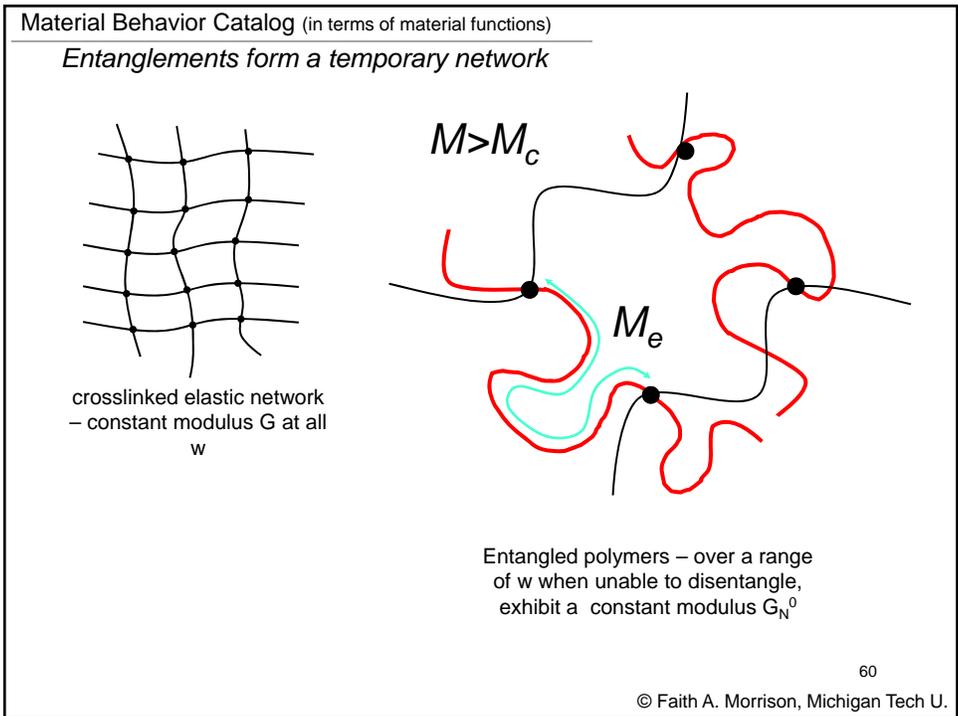
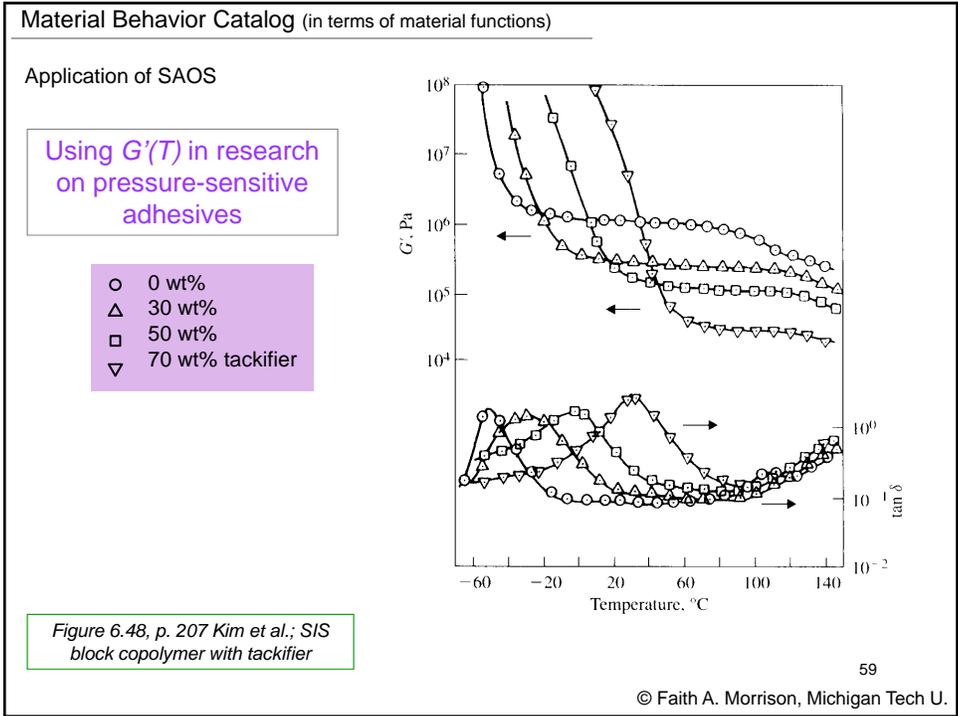
$$G''_r \equiv \frac{G''(T)T_{ref} \rho_{ref}}{T\rho} = h(a_T \omega, \tilde{\lambda}_i)$$

But since  $\log a_T$  is approximately a linear function of  $T$ ,

curves of  $\log G'$  versus  $T$  (not  $\log T$ ) at constant  $\omega$  resemble slightly skewed plots of  $\log G'$  versus  $\log a_T \omega$ . (mirror image)

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Material Behavior Catalog (in terms of material functions)

Small-Amplitude Oscillatory Shear -  $G'$   
molecular weight dependence

Level of plateau  $G_N^0$   
is related to  $M_e$   
(molecular theory for temporary networks)

$$G_N^0 = \frac{4}{5} \frac{\rho N_A k_B T}{M_e}$$

Larger the MW between entanglements, the softer the network

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Material Behavior Catalog (in terms of material functions)

Using  $G'(T)$  in research on pressure-sensitive adhesives

Height of plateau modulus and temperature of glass transition are key performance factors for PSAs.

**Tack** – if not tacky, will not produce bond  
**Shear holding** – if too fluid, will slide under shear

Figure 6.48, p. 207 Kim et al.; SIS block copolymer with tackifier

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Material Behavior Catalog (in terms of material functions)

Small-Strain Unsteady Shear Summary:

1. General traits
2. Effect of MW (linear polymers)
3. Effect of architecture
4. Relationship to steady flow material functions
5. Measurement issues
6. Effect of chemical composition
7. Effect of temperature

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Material Behavior Catalog (in terms of material functions)

**Experimental Data (continued)**

*Unsteady shear flow*



- Small strain - SAOS, step strain

*linear polymers, material effects, temperature effects*



- Large strain - start-up, cessation, creep, large-amplitude step strain

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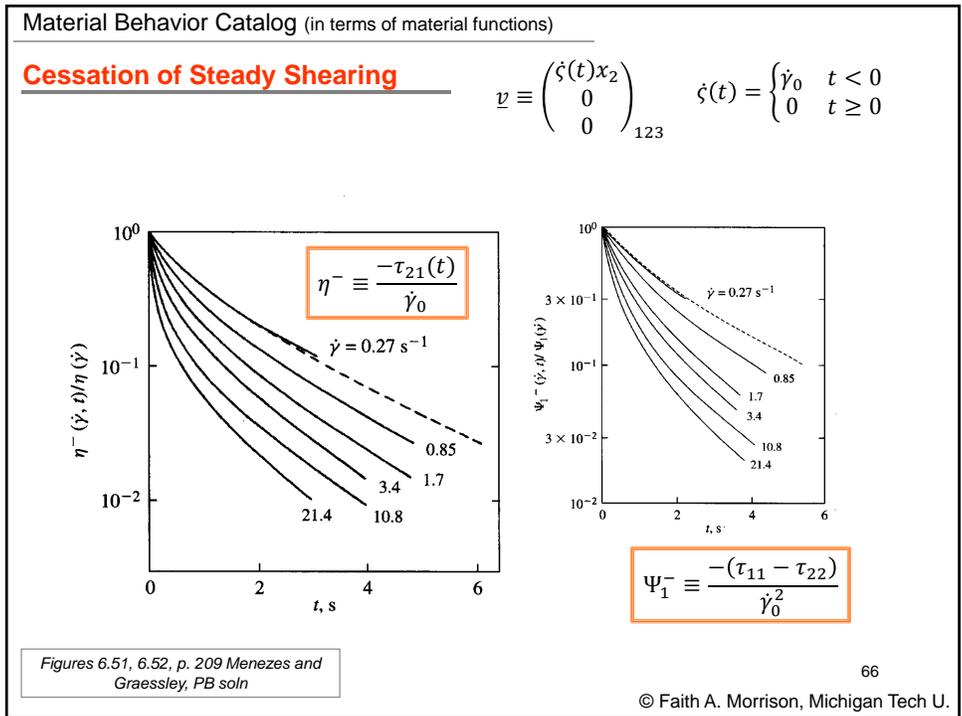
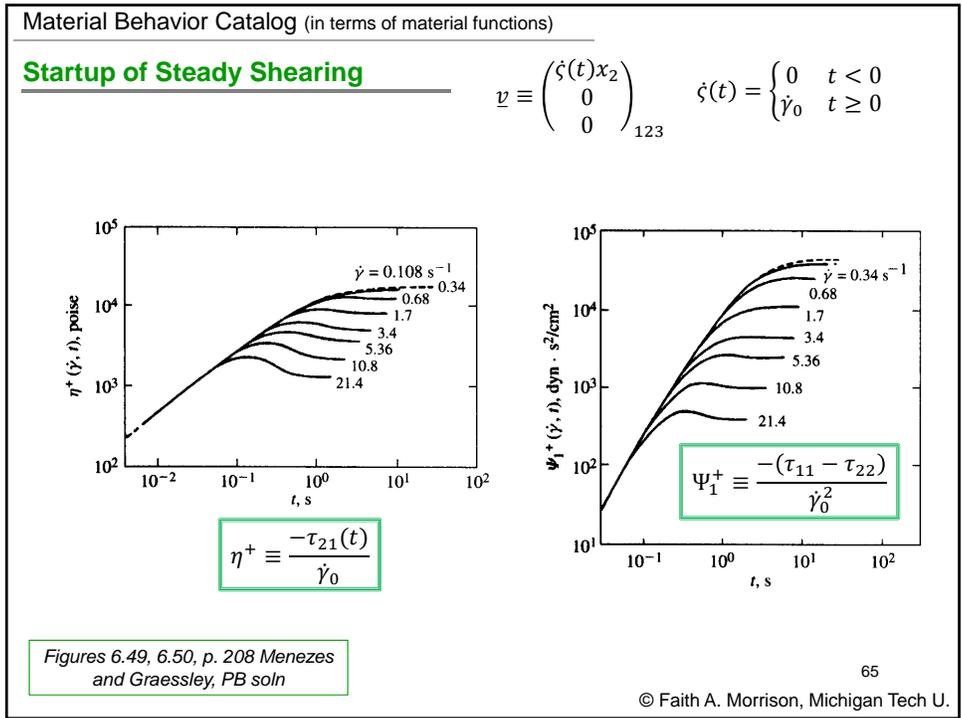
*lastly ...*

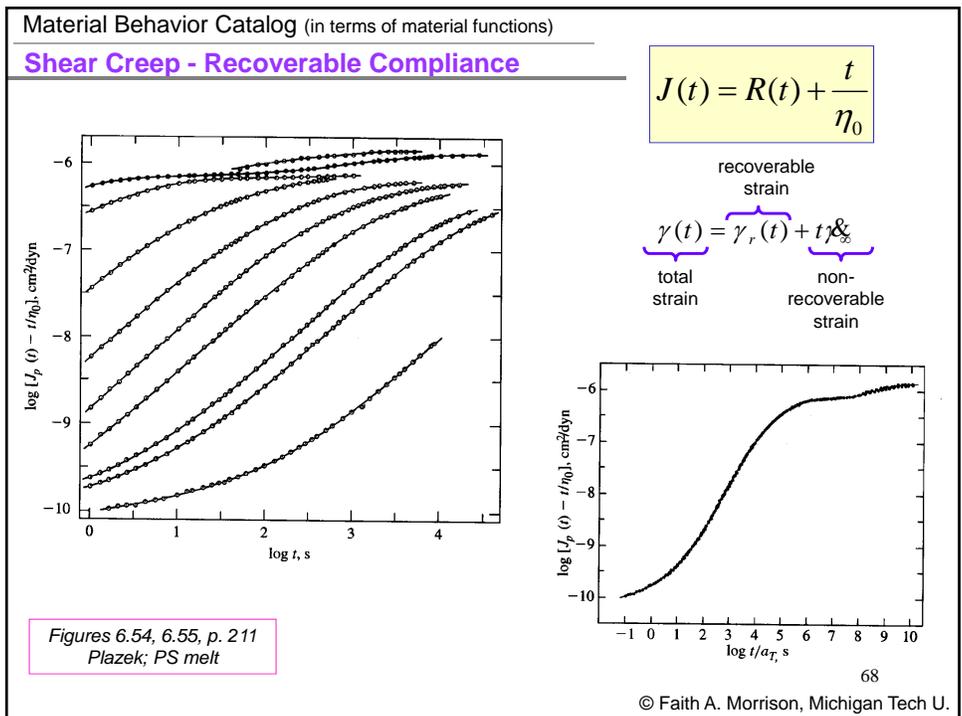
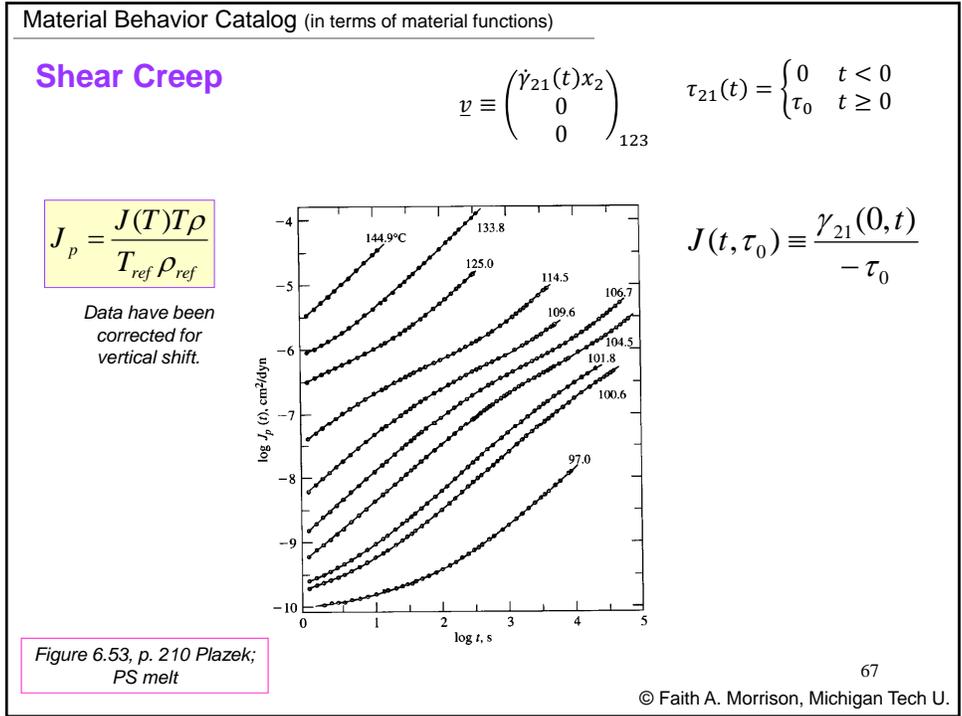
*Steady elongation*

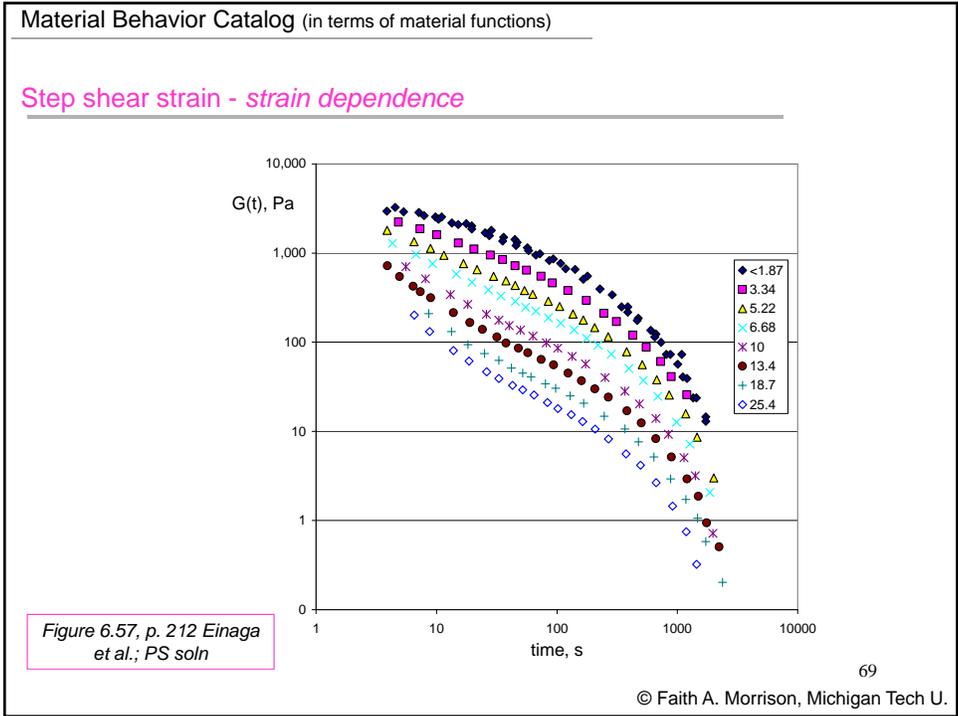
*Unsteady elongation*

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Material Behavior Catalog (in terms of material functions)

Shear Damping Function

Observation: step-strain moduli curves have similar shapes and appear to be shifted down with strain.

$$G(t, \gamma_0) = G(t)h(\gamma_0)$$

Damping function

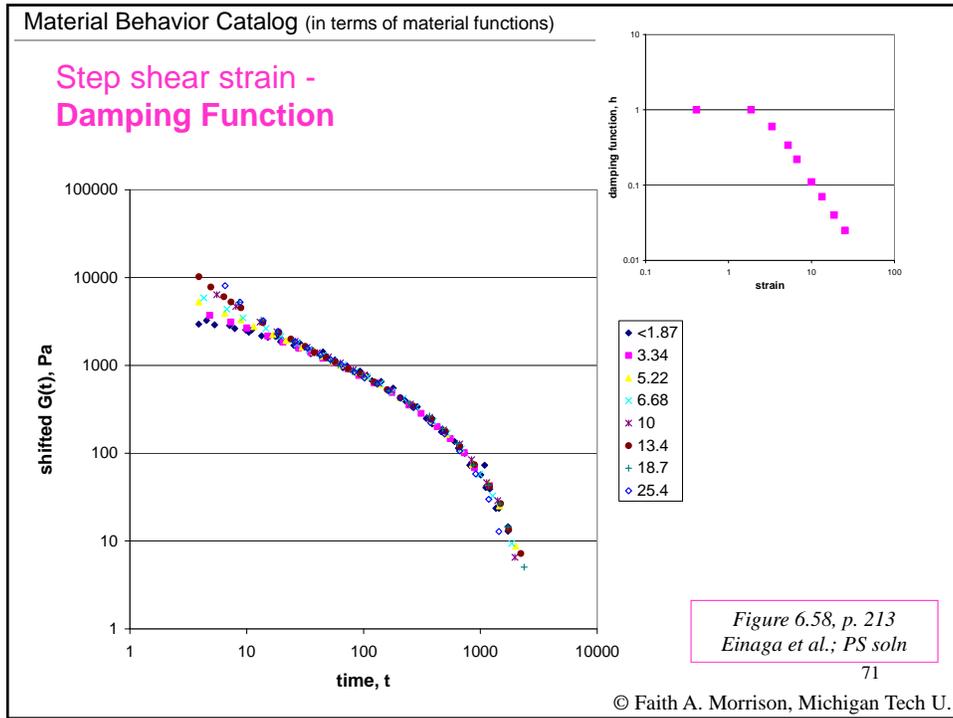
$$\log G(t, \gamma_0) = \log G(t) + \log h(\gamma_0)$$

The damping function gives the strain-dependence of the step-strain relaxation modulus.

When  $G(t, \gamma_0) = G(t)h(\gamma_0)$  the behavior is called time-strain separable.

This behavior is predicted by some advanced constitutive equations.

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Material Behavior Catalog (in terms of material functions)

### Large-Strain Unsteady Shear Summary:

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1. General traits
2. Measurement issues

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Material Behavior Catalog (in terms of material functions)

### Experimental Data (continued)

*Unsteady shear flow*

- ✓ • Small strain - SAOS, step strain  
*linear polymers, material effects, temperature effects*
- ✓ • Large strain - start-up, cessation, creep, large-amplitude step strain

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➔ *lastly ...*  
*Steady elongation*  
*Unsteady elongation*

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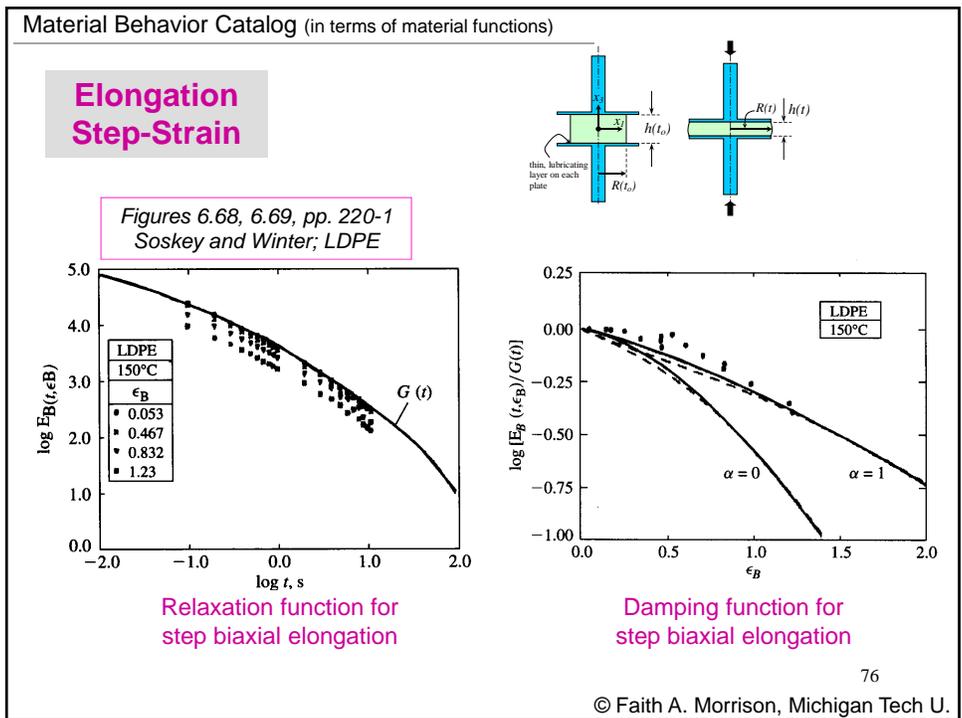
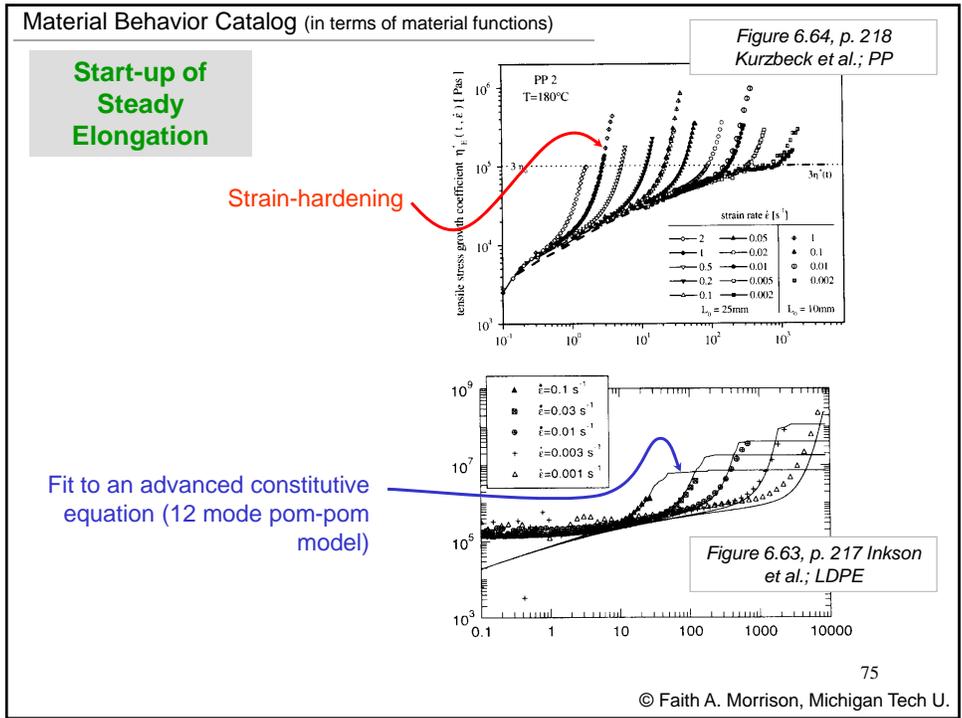
**Steady State Elongation Viscosity**

Both tension thinning and thickening are observed.

Trouton ratio:  $Tr \equiv \frac{\bar{\eta}}{\eta_0}$

Figure 6.60, p. 215 Munstedt.; PS melt

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Material Behavior Catalog (in terms of material functions)

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Elongational Flow Summary:

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1. General traits
2. Measurement issues

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Material Behavior Catalog (in terms of material functions)

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[More on Material Behavior](#)

**Polymer Behavior**

Larson, Ron, *The Structure and Rheology of Complex Fluids* (Oxford, 1999)  
Ferry, John, *Viscoelastic Properties of Polymers* (Wiley, 1980)

**Suspension Behavior**

Mewis, Jan and Norm Wagner, *Colloidal Suspension* (Cambridge, 2012)

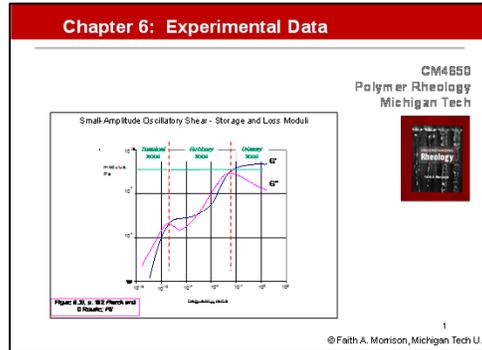
**Journals**

*Journal of Rheology*  
*Rheologica Acta*  
*Macromolecules*

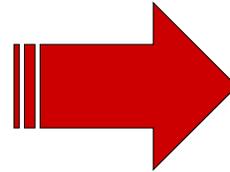
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Done with  
Experimental Data.

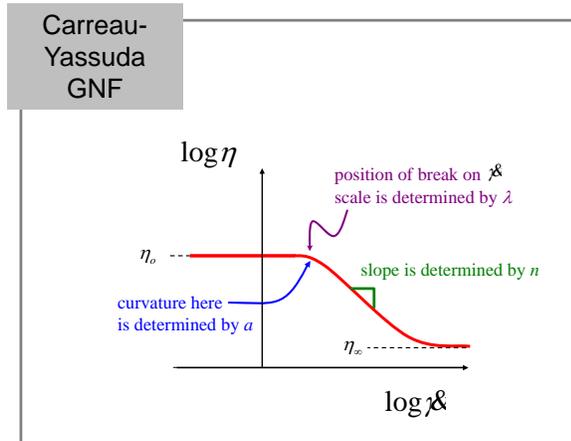


Let's move on to  
Generalized  
Newtonian Fluids



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## Chapter 7: Generalized Newtonian fluids



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