Instrument transformers - used to "step down" primary voltages and currents to lower standard levels.

- Current: 0-5A - CT Voltage: XI-X3:0-120V } Voltage Tranformen X2-X3:0-69.3V } (VT) XI-X3:0-115V } CVT or CCVT X2-X3:0-66.4V

ΦΑ

VI

(CVT)

(X2)

(49,3V)

(20)

(A)

(CVT)

(X2)

(49,3V)

(A)

(CVT)

(X2)

(41,5V)

(42)

(44,4V)

(44,4

Note that "PT" designation is obsolete - new designation is "VT". Economics usually point to use of CVT or CCVT for voltages above 69-KV, VTs for lower Voltages.

Note that linear couplers, which produce a secondary voltage proportional to the primary current, were in vogue for a while in the 50's \$ 60's but never caught on. Used mainly in bus differential schemes. Regnires special relays (voltage instead of current imput) - this additional cost hobbled it. (See p.35\$, Blackburn)

VT's and CCVTs will not experience overvoltage situations (except for ferroresonance) and so the extreme core saturation problems of the CT are not an issue, especially for system protection.

If VT or CCVT is to be used for metering, however, then accuracy is an issue.

1.2R accuracy class - relaying 0.3 accuracy class - metering

YT:

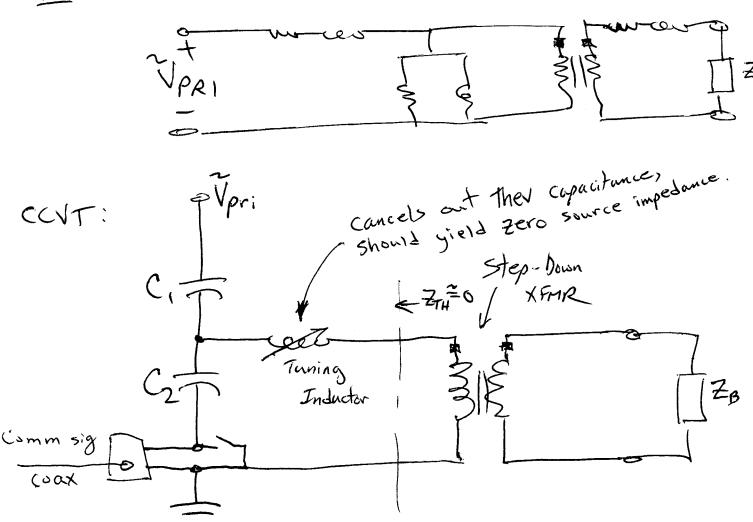


Table 3				
Voltage	Ratings	and	Marked	Ratios

Maximum	Maximum Rated	Performance Reference	Marked Ratio (Note 3)	
System Voltage (kV)	Voltage (Note 2) (kV)	Voltage (Note 3) (Volts)	Lower Ratio	Higher Ratio
Col 2	Col 3	Col 4	Col 5	Col 6
38 48.3 72.5 121 145 169 242 362	22 28 42 70 84 98 140 209	20 125 27 000 40 250 69 000 80 500 92 000 138 000 207 000 287 500	175:1 240:1 350:1 600:1 700:1 800:1 1200:1 1800:1 2500:1	300:1 400:1 600:1 1000:1 1200:1 1400:1 2000:1 3000:1 4500:1
	System Voltage (kV) Col 2 38 48.3 72.5 121 145 169 242	System Voltage (Note 2) Voltage (Note 2) (kV) (kV) Col 2 Col 3 38 22 48.3 28 72.5 42 121 70 145 84 169 98 242 140 362 209 550 317	System Voltage (Note 2) Voltage (Note 3) Voltage (kV) (Note 2) (Note 3) (kV) (Volts) Col 2 Col 3 Col 4 38 22 20 125 48.3 28 27 000 72.5 42 40 250 121 70 69 000 145 84 80 500 169 98 92 000 242 140 138 000 362 209 207 000 550 317 287 500	System Voltage (Note 2) Voltage (Note 3) Lower Ratio Col 2 Col 3 Col 4 Col 5 38 22 20 125 175:1 48.3 28 27 000 240:1 72.5 42 40 250 350:1 121 70 69 000 600:1 145 84 80 500 700:1 169 98 92 000 800:1 242 140 138 000 1200:1 362 209 207 000 1800:1 550 317 287 500 2500:1

^{*}These typical "nominal" voltages are in accordance with Section 2 of American National Standard Preferred Voltage Ratings for Alternating-Current Electrical Systems and Equipment Operating at Voltages above 230 Kilovolts Nominal, C92.2-1976.

NOTES:

(1) These values correspond to the preferred nominal system voltages given in American National Standard Voltage Ratings for Electric Power Systems and Equipment (60 Hz), C84.1-1977, except for the 345-, 500-, and 765-kV ratings.

(2) These values are the phase-to-ground voltages corresponding to the maximum voltage of the tolerable zone for voltages at substations and on transmission systems given in American National Standard C84.1-1977.

(3) For CCVTs in this table that have a double ratio achieved by means of a tap in the secondary winding(s), the nonpolarity end of the winding shall be the common terminal. Application of performance reference voltage between the high-voltage terminal and the ground terminal will result in 115 volts across the secondary windings having the lower ratio.

3.2 Unusual Service Conditions

- (1) Altitudes above 3300 feet (1000 meters). For CCVTs applied at altitudes greater than 3300 feet (1000 meters), the dielectric strength correction factors given in Table 2 should be applied.
 - (2) Gas-insulated substations.
 - (3) High-voltage power cable systems.

4. Ratings

4.1 General

4.1.1 Voltage Ratings and Marked Ratios. Voltage ratings and marked ratios shall be as listed in Table 3.

4.1.2 Dielectric Strength Requirements

- 4.1.2.1 Dielectric Strength of the Capacitor Divider. The dielectric strength of the capacitor divider shall be in accordance with Table 3 of American National Standard Requirements for Power Line Coupling Capacitors, C93.1-1972.
- 4.1.2.2 Dielectric Strength of the Electromagnetic Unit
- 4.1.2.2.1 Dielectric Strength of the Intermediate-Voltage Circuit. The dielectric strength of

the electromagnetic unit at the intermediate-voltage terminal shall be equal to the appropriate capacitor divider dielectric test values as specified in Table 3 of American National Standard C93.1-1972 multiplied by the ratio $C_1/(C_1+C_2)$. The sparkover voltage of protective equipment, such as gaps, may be lower than the dielectric strength rating.

4.1.2.2.2 Dielectric Strength of the Secondary Circuit. The secondary windings of the intermediate-voltage transformer and the reactive element of any auxiliary equipment to be connected to the secondary winding(s) shall withstand a test voltage of four times normal operating voltage for 1 minute and a power-frequency rms dielectric test voltage of 2.5 kV for 1 minute between the secondary circuit and ground and between secondary windings.

4.1.3 Capacitance and Dissipation Factor of the Capacitor Divider

- 4.1.3.1 Prior to Dielectric Tests. The stack capacitance at rated power frequency shall not differ from the nominal nameplate value by more than -5% or +10%.
- 4.1.3.2 After Dielectric Tests. The capacitance at rated power frequency shall differ from that measured

Burdens*		Characteristics on 120-Volt Basis		Characteristics on 69.3-Volt Basis				
Designation	Volt-Amperes	Power Factor	Resistance (ohms)	Inductance (henries)	Impedance (ohms)	Resistance (ohms)	Inductance (henries)	Impedance (ohms)
М	35	0.20	82.3	1.07	411	27.4	0.356	137
W	12.5	0.10	115.2	3.04	1152	38.4	1.01	384
X	25	0.70	403.2	1.09	576	134.4	0.364	192
Y	75	0.85	163.2	0.268	192	54.4	0.0894	64
Z	200	0.85	61.2	0.101	72	20.4	0.0335	24
ZZ	400	0.85	30.6	0.0503	36	10.2	0.0168	12

Table 4
Burdens for Accuracy Rating

prior to the dielectric tests by less than the equivalent of one capacitor element. The dissipation factor at rated power frequency shall not differ from that measured prior to the dielectric tests by more than 0.1%.

NOTE: The purpose of checking the dissipation factor is to check the uniformity of the production method and effectiveness of the processing cycle.

- 4.1.4 Radio-Influence Voltage. The maximum radio-influence voltage of a CCVT shall be in accordance with Table 4 of American National Standard C93.1-1972.
- 4.1.5 Short-Time Overvoltage Operation. The CCVT shall be capable of withstanding 140% of performance reference voltage for 1 minute.

"Capable of withstanding" shall be interpreted to mean that, after being subjected to this duty, the CCVT shall show no damage and shall be capable of meeting the requirements of this standard.

4.1.6 Burdens

4.1.6.1 Burdens for Accuracy Rating. Burdens for accuracy rating purposes shall be expressed in voltamperes at a specified lagging power factor as listed in Table 4, at one of the voltages given as follows:

Burdens are based on two secondary voltages, 120 volts and 69.3 volts, and rated power frequency. The burden designations and the same physical burdens are used in applying accuracy ratings to CCVTs irrespective of the exact secondary voltages resulting from the voltage applied to the high-voltage terminal and ratios. For example, for those CCVTs having ratios that result in secondary voltages of 115 or 66.4 volts at performance reference voltage, the actual voltamperes for a designated burden is reduced to 91.8% of the values listed in Table 4.

4.1.6.2 Burdens for Transient Response Rating.
Burdens for transient response rating purposes shall be

expressed in volt-amperes at a specified lagging power factor. Burdens are based on a 120-volt secondary voltage and rated power frequency. The burden shall consist of two impedances connected in parallel as in Fig. 1. One impedance shall be a pure resistance (R_p) and the other $(R_s$ plus $X_s)$ shall have a lagging power factor of 0.5. The inductive reactor shall be of the air-core type.

Burden values for transient response tests shall be 100% of the CCVT maximum rated accuracy class winding volt-amperes and 25% of the maximum rated accuracy class winding volt-amperes at 0.85 power factor. Burdens for CCVTs rated ZT or ZZT are shown in Table 5.

4.1.7 Thermal Burden Rating. The thermal burden rating of a CCVT shall be specified in terms of the maximum burden that the CCVT can carry continuously at maximum rated voltage without exceeding the temperature rise, above a 30°C ambient, permitted by the dielectric materials used in construction.

Each winding, including the primary winding of a

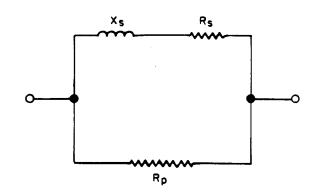


Fig. 1
Circuit Diagram of Burden to Be
Used for Transient Response Test

^{*} These burden designations have no significance at frequencies other than 60 Hz.

Table 6
Accuracy Class Limits for Relaying Service

Accuracy Class		of Rutio ion Factor	
	Minimum	Maximum	Limits of Phase Angle
1.2R	0.988	1.012	± 63 minutes (± 18 milliradians)

- 4.2 Relaying Service CCVTs. The CCVT shall be within the limits of ratio correction factor and phase angle from zero burden to accuracy burden rating.
- 4.2.1 Accuracy Class. Accuracy class and corresponding limits of ratio correction factor and phase angle shall be as shown in Table 6 and Fig. 2.
- 4.2.2 Allowable Variation in Ratio Correction Factor and Phase Angle with Operating Conditions
- 4.2.2.1 Voltage Variations. The limits of ratio correction factor and phase angle for variations in ap-

- plied voltage with constant linear burden shall be as shown in Table 7.
- 4.2.2.2 Frequency Variations. Over the range of 58 Hz through 62 Hz, the ratio correction factor shall be within the limits of 0.95 to 1.05 and the phase angle shall be within the limits of $\pm 5^{\circ}$ degrees (± 87 inrad) from the 60-Hz values.
- **4.3 Metering Service CCVTs.** The CCVT shall be within the limits of ratio correction factor and phase angle from zero burden to accuracy burden rating.
- 4.3.1 Accuracy Classes. Accuracy classes and corresponding limits of ratio correction factor and phase angle shall be as shown in Fig. 3. A metering service CCVT shall be assigned an accuracy class rating for each of the burdens for which it is designed.
- 4.3.2 Allowable Variation in Ratio Correction Factor and Phase Angle with Operating Conditions
- 4.3.2.1 Voltage Range. A CCVT shall remain within its metering accuracy class limits when operating continuously between 90% of performance reference voltage and maximum rated voltage.

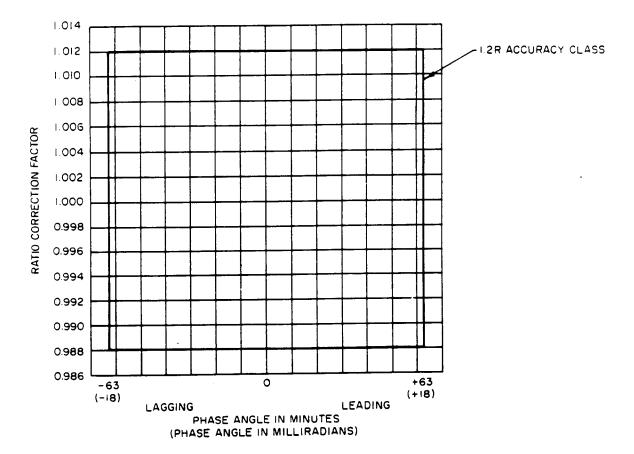


Fig. 2
Limits for Accuracy Class 1.2R for
Coupling Capacitor Voltage Transformers for
Relaying Service

Table 7
Limits of Ratio Correction Factor and Phase Angle with Voltage Variations

Applied Voltage	Ratio Correction Factor Limits	Phase Angle Limits
90% performance reference voltage to maximum	Accuracy class limits	Accuracy class limits
rated voltage 25% performance	0.97 to 1.03	± 3° (± 52 mrad)
reference voltage 5% performance reference voltage	0.95 to 1.05	± 5° (± 87 mrad)

- 4.3.2.2 Temperature Range. A CCVT shall remain within its metering accuracy class limits over the ambient temperature range specified in 3.1.
- 4.3.2.3 Interrelation of Voltage and Temperature. The provisions of 4.3.2.1 and 4.3.2.2 shall be considered simultaneous effects.

5. Testing

5.1 General

- **5.1.1 Test Conditions.** Units shall be tested as specified in 5.1.1.1 through 5.1.1.4.
- 5.1.1.1 The ambient temeprature range for testing shall be from + 10°C through + 40°C, with + 20°C as the reference temperature.
- 5.1.1.2 The test units shall be new and in clean, dry condition.
 - 5.1.1.3 The test units shall be mounted vertically.
- 5.1.1.4 The sequence of testing shall be optional, except where otherwise noted.
- **5.1.2 Production (Routine) Tests.** The following production tests shall be performed by the manufacturer on each CCVT:
 - (1) Capacitance and dissipation factor (see 5.2.1)
 - (2) Dielectric (see 5.2.2)
 - (3) Accuracy (see 5.2.3)
 - (4) Polarity (see 5.2.4)
 - (5) Protective-gap setting (see 5.2.5)

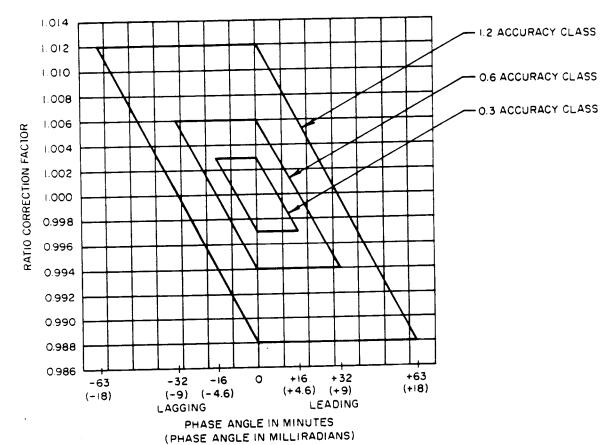


Fig. 3
Limits for Accuracy Classes 0.3, 0.6, and 1.2 for Coupling Capacitor Voltage Transformers for

Metering Service

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Appendix A Coupling Capacitor Voltage Transformer Circuit Diagram

A typical diagram of a coupling capacitor voltage transformer with carrier coupling accessories is shown in Fig. A1. Note, however, that electromagnetic unit overvoltage protective gaps and ferroresonance suppression networks are not included in this diagram.

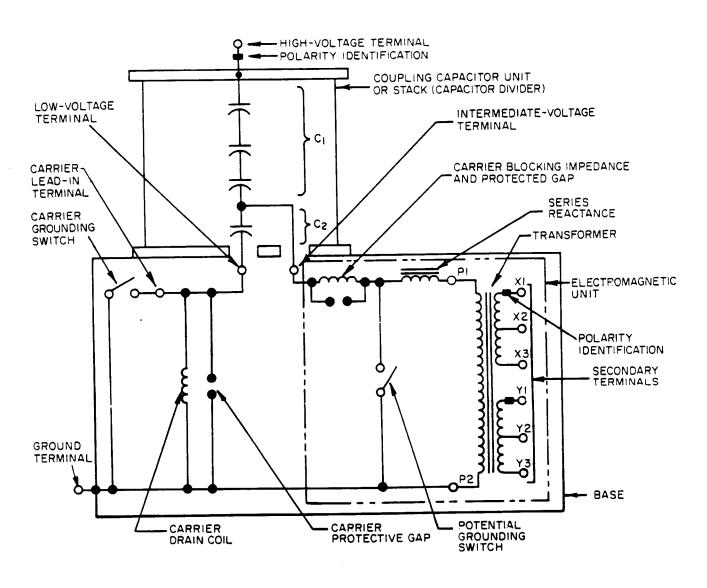


Fig. A1 Typical Diagram of Coupling Capacitor Voltage Transformer with Carrier Coupling Accessories