


# Power System Protection

## Ground faults in resonance grounded systems

# Briefly about the speaker



- Professor at Norwegian Univ. Science and Technology – Dept. Electrical Engineering
  - Power system transients and protection
  - High voltage engineering, stress calculations
  - Recent focus on Power Transformers
- Developer of ATPDraw
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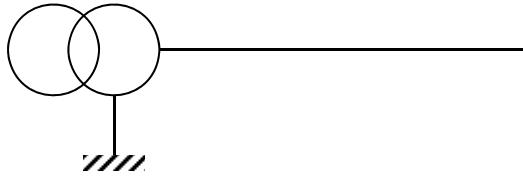
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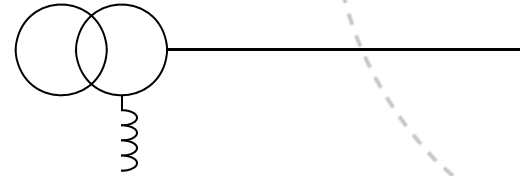
<http://www.elkraft.ntnu.no/~hansh/>

 **NTNU**  
Innovation and Creativity

# Solid vs. resonance neutral



- + No over-voltages in fault situations
- High fault current
- + Easy fault detection
- + Ground faults persist
  - Fast trip and reclosing
- Poor power quality
- Extra stress

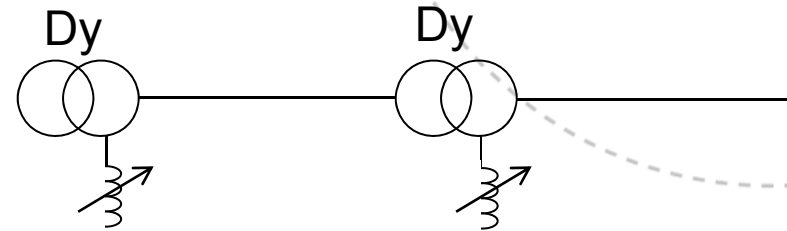


- Undefined voltages to ground. High at resonance.
- + Ideally zero fault current. Arc self-extinguish.
- Difficult fault detection/location. Requires special competence and maintenance.
- In dynamic systems the coil must adapt. Expensive equipment.
- + Can continue to operate during ground fault. Increased power quality.
  - Safety issues: down/broken conductors



# Usage of resonance grounding

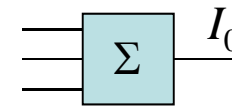
- In Norway
  - MV system 12-24 kV
  - Distribution level 66-132 kV
- Self-tuning Peterson coils used
- Weather conditions result in a lot of temporary ground fault
- Power quality is very important to the industry
  - Fast trip & reclosing not acceptable
- Increasingly a preferred solution in Europe



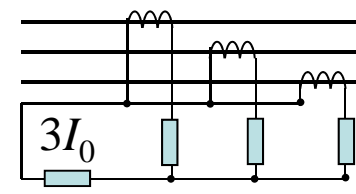
# Zero sequence measurements

- Current  $I_0$ : Sum  $I_a, I_b, I_c$

- Summing the current numerically

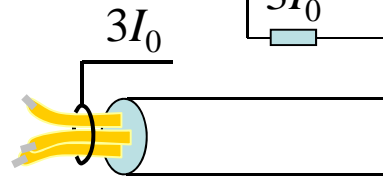


- Residual connection



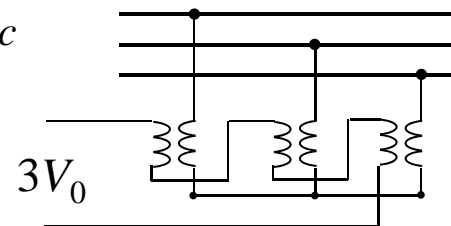
Lower accuracy due to CT differences

- Summation transformer (Toroidal/Rogowski coil)

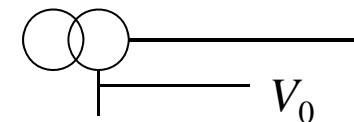


- Voltage  $V_0$ : Sum  $V_a, V_b, V_c$

- Open delta



- Neutral point (isolated or resonance earth)

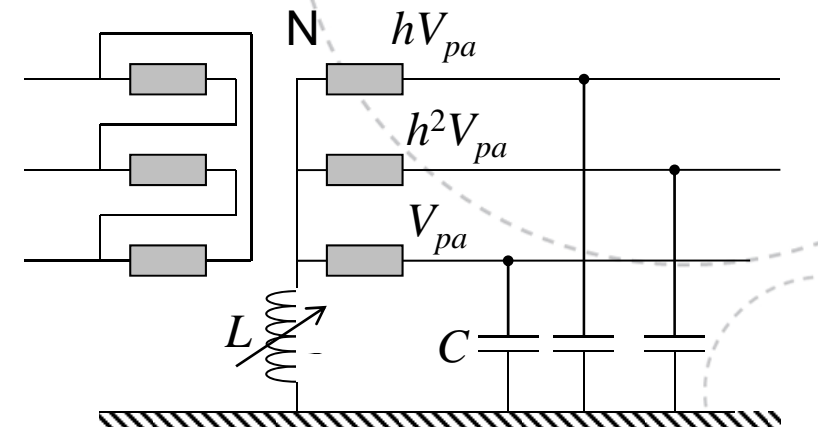
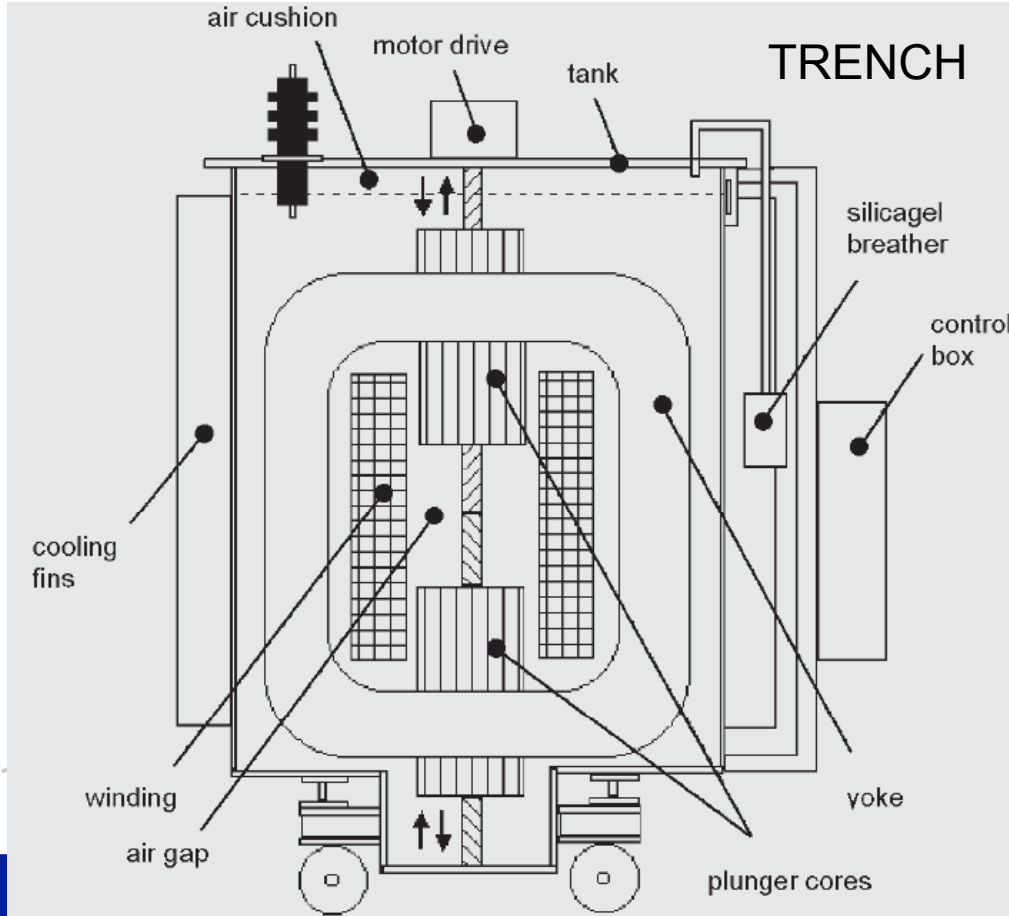


# Resonance grounding

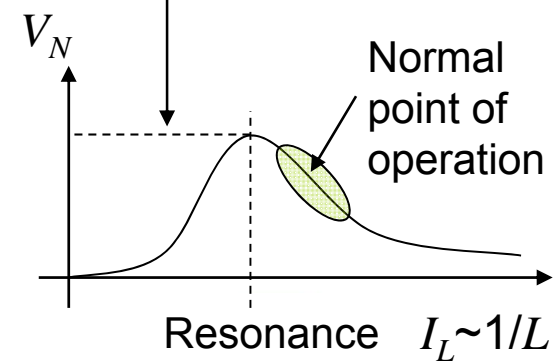
- Inductance added in the neutral point
- Compensate for the capacitive current through  $C_g$ ; help the arc self extinguish
- The coil can be automatically tuned when the system changes (Petersen-coil (patent from around 1920))
  - Adjust air gap
  - The coil changes its value incrementally and notice how the neutral voltage changes. From a theoretical curve the resonance point is estimated.
- Over-compensation preferred to limit  $V_N$ 
  - Avoid resonance also when parts of the system become disconnected
- The unit Ampere is used to quantify the coil;  $I_L = V_p / \omega L$

# Variable inductance

- Adjust air gap



Increases with  
asymmetry and  
resistance

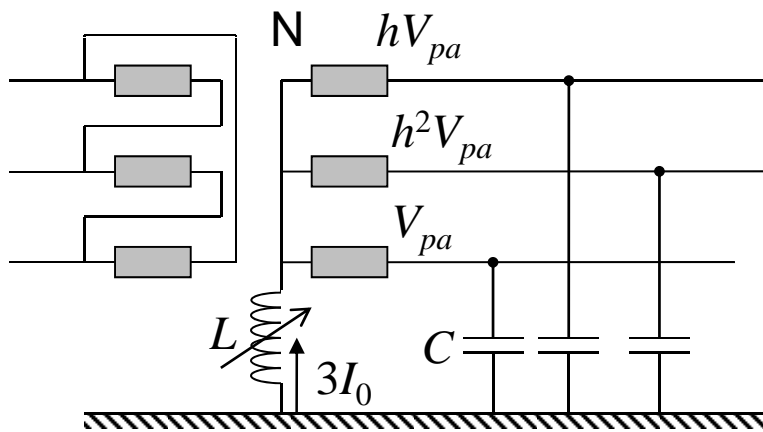


No-fault situation



# First attempt to analyze the neutral voltage

- Need to know: Maximum neutral voltage in normal operation. Set  $U_0$  pick-up above this limit



$$I_a = (V_N + V_{pa}) \cdot j\omega C$$

$$I_b = (V_N + h^2 \cdot V_{pa}) \cdot j\omega C$$

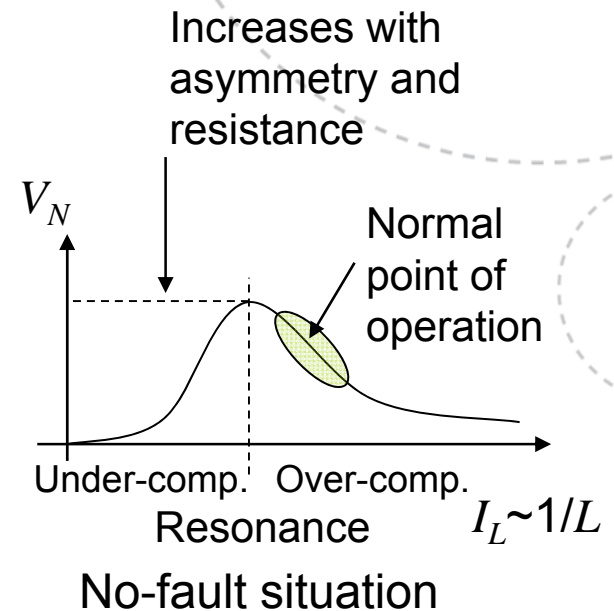
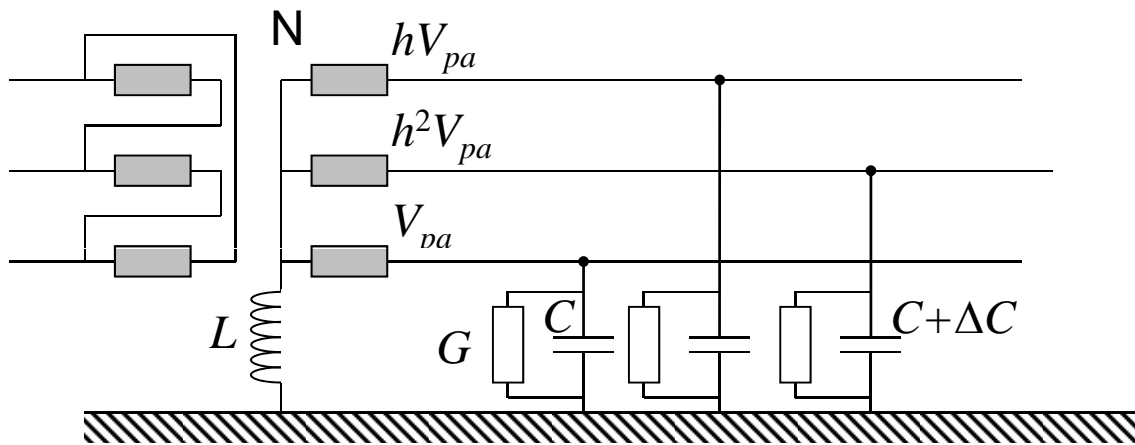
$$I_c = (V_N + h \cdot V_{pa}) \cdot j\omega C$$

$$3I_0 = (I_a + I_b + I_c) = V_N \cdot j\omega 3C = \frac{-V_N}{j\omega L}$$

$$\Rightarrow V_N = \frac{0}{j\omega 3C + 1/j\omega L} ??$$

- At resonance  $j\omega 3C + 1/j\omega L = 0$  and the neutral voltage becomes undefined... ( $\rightarrow \infty$ )
- Need to add sophistication here...

# Effect of asymmetry and conductive line charging



$$I_a = (V_N + V_{pa}) \cdot (G + j\omega C)$$

$$I_b = (V_N + h^2 \cdot V_{pa}) \cdot (G + j\omega (C + \Delta C))$$

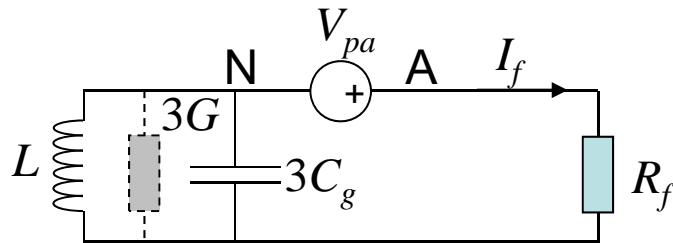
$$I_c = (V_N + h \cdot V_{pa}) \cdot (G + j\omega C)$$

$$3I_0 = (I_a + I_b + I_c) = 3V_N \cdot (G + j\omega C) + (V_N + h^2 \cdot V_{pa}) \cdot j\omega \Delta C = \frac{-V_N}{j\omega L}$$

$$\Rightarrow V_N = \frac{-h^2 \cdot V_{pa} \cdot j\omega \Delta C}{3G + j\omega 3C + j\omega \Delta C + 1/j\omega L} \Rightarrow V_N = \frac{V_p}{1 + \frac{s}{u} - j \frac{d}{u}} \Rightarrow |V_{N, \max}| \approx \frac{V_p \omega \Delta C}{3G}$$

# Resonance grounded system during fault ( $L=\text{constant}$ )

- Equivalent circuit (fault phase A)



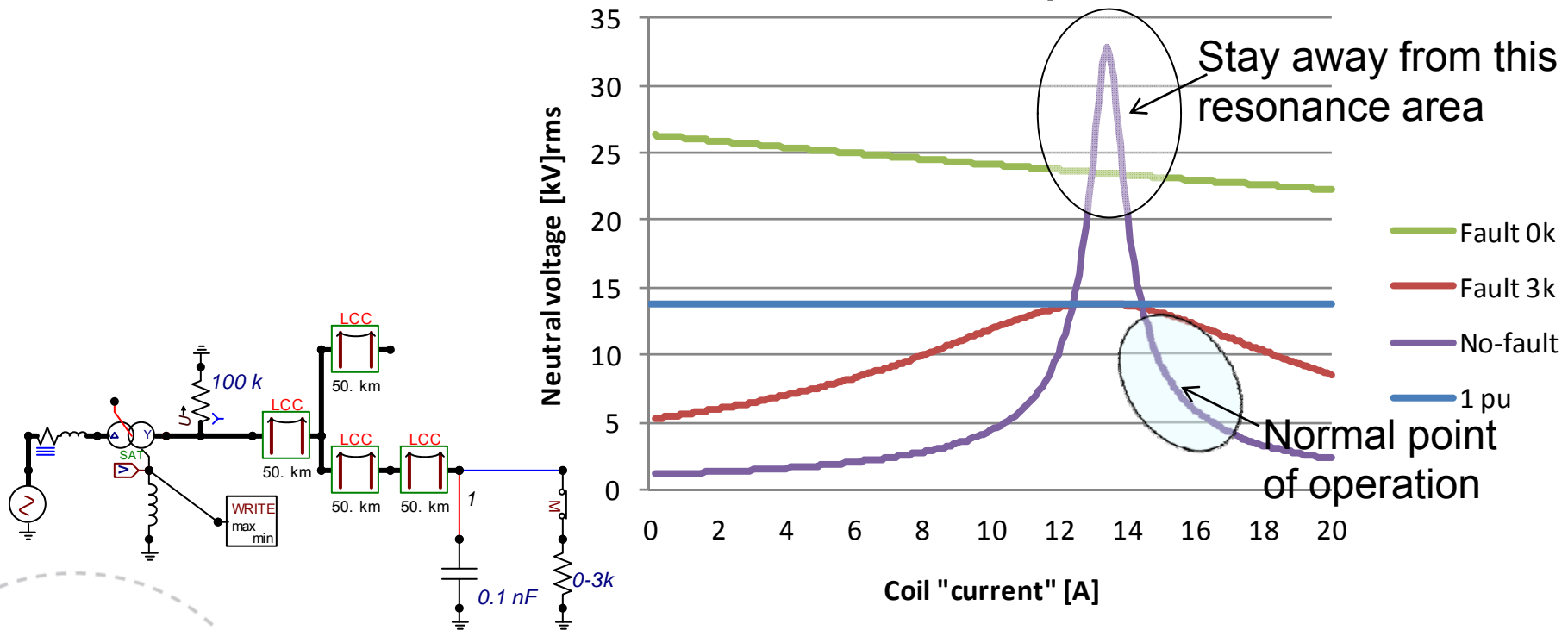
$$I_f = \frac{V_{pa} \cdot (1 - \omega^2 L \cdot 3C_g)}{j\omega L + R_f (1 - \omega^2 L \cdot 3C_g)}$$

$$V_N = V_0 = \frac{-V_{pa} \cdot j\omega L}{j\omega L + R_f (1 - \omega^2 L \cdot 3C_g)} \longrightarrow V_{pa} \text{ at resonance, also for large } R_f$$

- In reality asymmetry ( $\Delta C$ ) and conductive elements ( $G // 1/R_f$ ) affect fault current and  $V_N$
- A resistance across  $L$  is often actively connected to “find” the fault (identify faulty feeder)

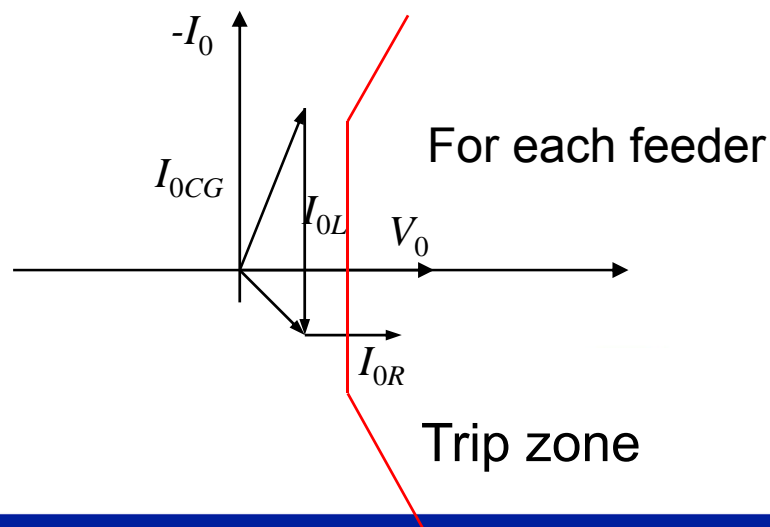
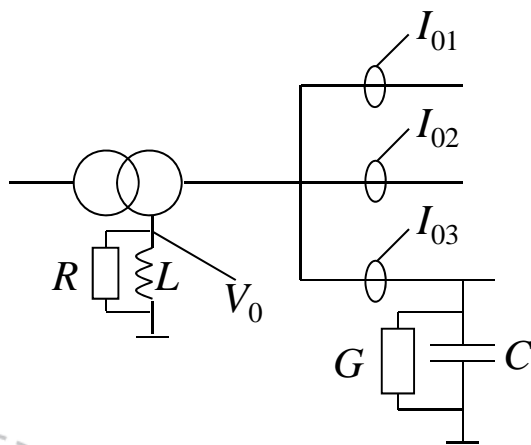
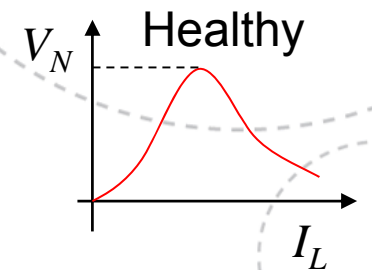
# Example of neutral voltage

- From ATP simulations
  - In reality the resonance peak is typically lower
  - ...and measurements are required



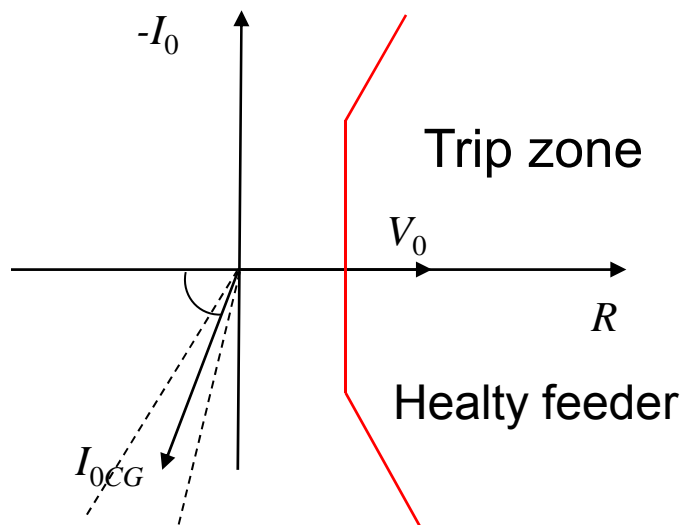
# Directional over-current relay – resonance grounded systems

- Start when  $V_0$  goes above a fixed limit; pre-measure the coil response  $\max(V_{N,healthy})$ ;
- After a delay connect resistor  $R$  ( $\parallel$  to  $L$ )
- Trip if current  $I_0$  enters trip zone (2<sup>nd</sup> quadrant)
- Trip zone set based on natural conductive current and asymmetry



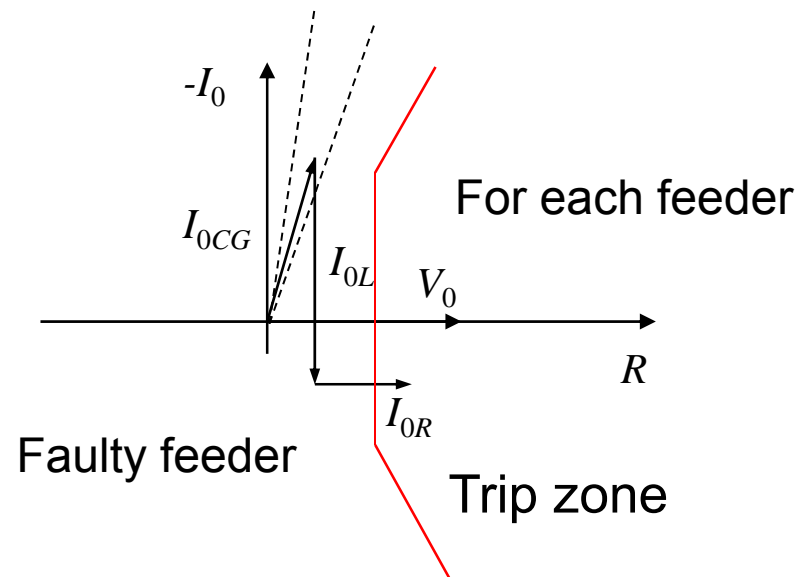
# Trip zone

- The resistive component of  $I_0$  (in phase with  $V_0$ ) is used



$$\begin{aligned} -3I_{0i} &= (I_{ai} + I_{bi} + I_{ci}) \\ &= -V_0 \cdot (3G_i + j\omega 3C_i) \end{aligned}$$

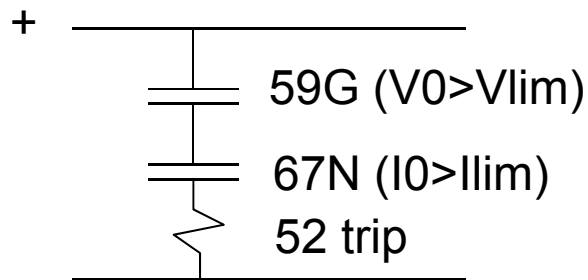
Angle quite close to  $90^\circ$



$$\begin{aligned} -3I_{0i} &= -(I_{ai} + I_{bi} + I_{ci}) \\ &= V_0 \cdot (3G_i + j\omega 3C_i) + (V_0 + V_{pa}) / R_f \\ &\approx V_0 \cdot \left( 3(G_t - G_i) + j\omega 3(C_t - C_i) + \frac{1}{j\omega L} \right) \end{aligned}$$

# Relaying logic

- Is zero sequence voltage above threshold?
  - $V_0 > V_{lim}$  (type 59G over-voltage relay)
- Is zero sequence current above threshold and in correct quadrant (4th)?
  - $I_0 > I_{lim}$  (type 67N directional over-current relay)



# Wave/Wischer relays

- Used in the 132 kV resonance earthed system
- Measure the transient surge and use time of arrival principles
- Communication required
- Trip the two relays that first identify the fault
- Sensitive to disturbances like lightning

