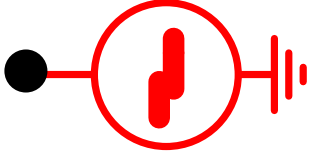


Topics for Today:

- Course Info:
 - Web page: <https://pages.mtu.edu/~bamork/ee5220/>
 - Book, references, syllabus, more are on web page.
 - Software - Matlab. ATP/EMTP [License - www.emtp.org] ATP tutorials posted on our course web page
 - EE5220-L@mtu.edu (participation = min half letter grade)
- HW#7 - due Tues 9am Mar 15th .
- Upcoming: HW#8 - Probs. 9.6, 9.12 due ~Tues Mar 22nd 9am.
- HW#9 - Probs. 9.2, 9.3, 9.4 due date TBA.
- Term Project - Mar 21st - a) complete reference list and b) fully-detailed table of contents according to format given in Term Project Guidelines.
- Line Models implemented in ATP
- ATP Simulation pointers
 - Freq scan - used for T-line Verify, filter design at DC terminus, etc.
 - Surge waveforms - Type 15 Surge source: for lightning, switching
 - Example: Prob. 9.2 (HW#9); Chapters 14 and 15
- Coming next: Transformer modeling - Section 11.1 of text, plus lecture notes
 - Study pre-req mats on mag circuits
 - Example single-phase transformer, Excitation, Inrush
 - Take stock of available ATP transformer models



Name : SURGE - Surge function. Two exponentials. TYPE 15.

Card : SOURCE

Data : U/I= 0: Voltage source.

-1: Current source.

Amp= Constant in [A] or [V].

Does not exactly correspond to the peak value of surge.

A= Negative number specifying falling slope.

B= Negative number specifying rising slope.

Tsta= Starting time in [sec.]. Source value zero for $T < T_{sta}$.

Tsto= Ending time in [sec.]. Source value zero for $T > T_{sto}$.

Node : SU= Positive node of exponential surge function.

Negative node is grounded.

$SU = Amp * (\exp(A * t) - \exp(B * t))$

RuleBook: VII.C.5

Component: SURGE

Attributes

DATA	UNIT	VALUE	NODE	PHASE	NAME
Amplitude	Volt	750000	SU	1	SRC
A	1/s	-20000			
B	1/s	-100000			
Tstart	s	0.01			
Tstop	s	1000			

Order: 0 Label:

Copy Paste entire data grid

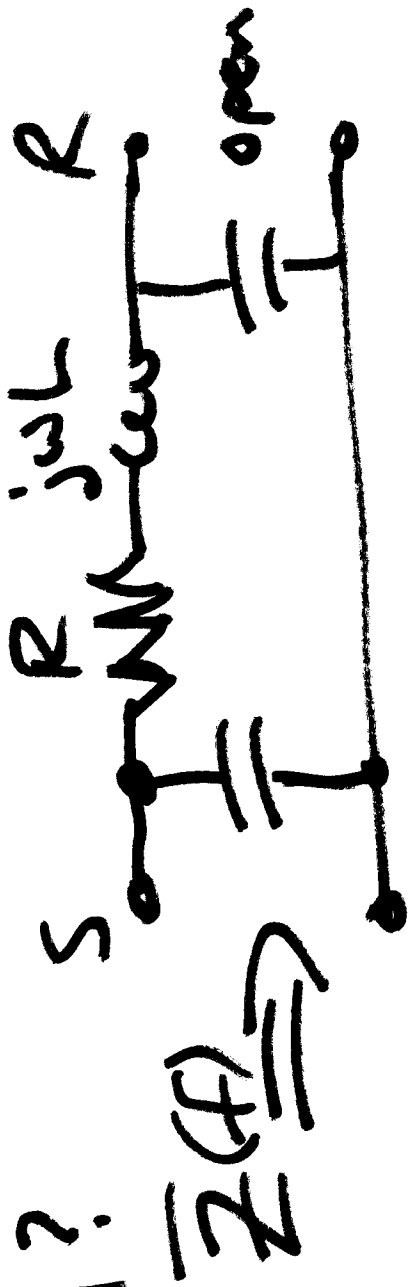
Comment:

Type of source
 Current
 Voltage

Hide
 Lock

Edit definitions OK Cancel Help

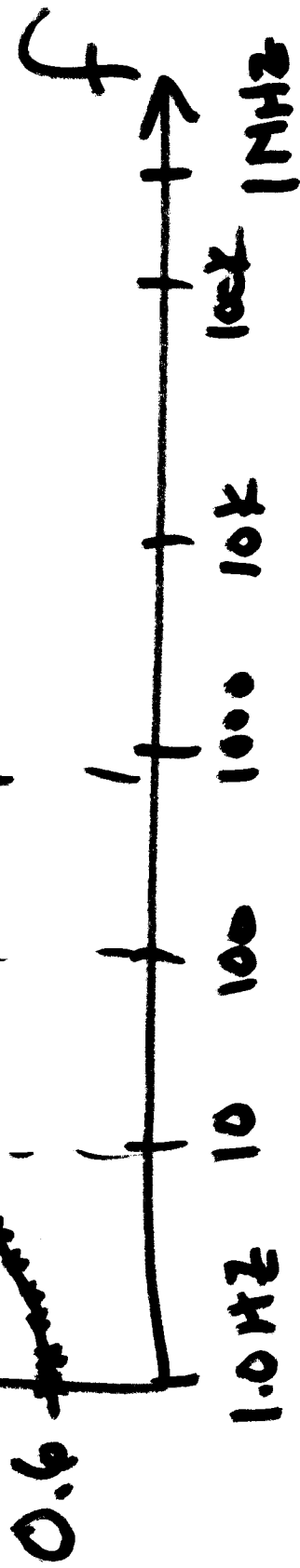
"Exact" Model?



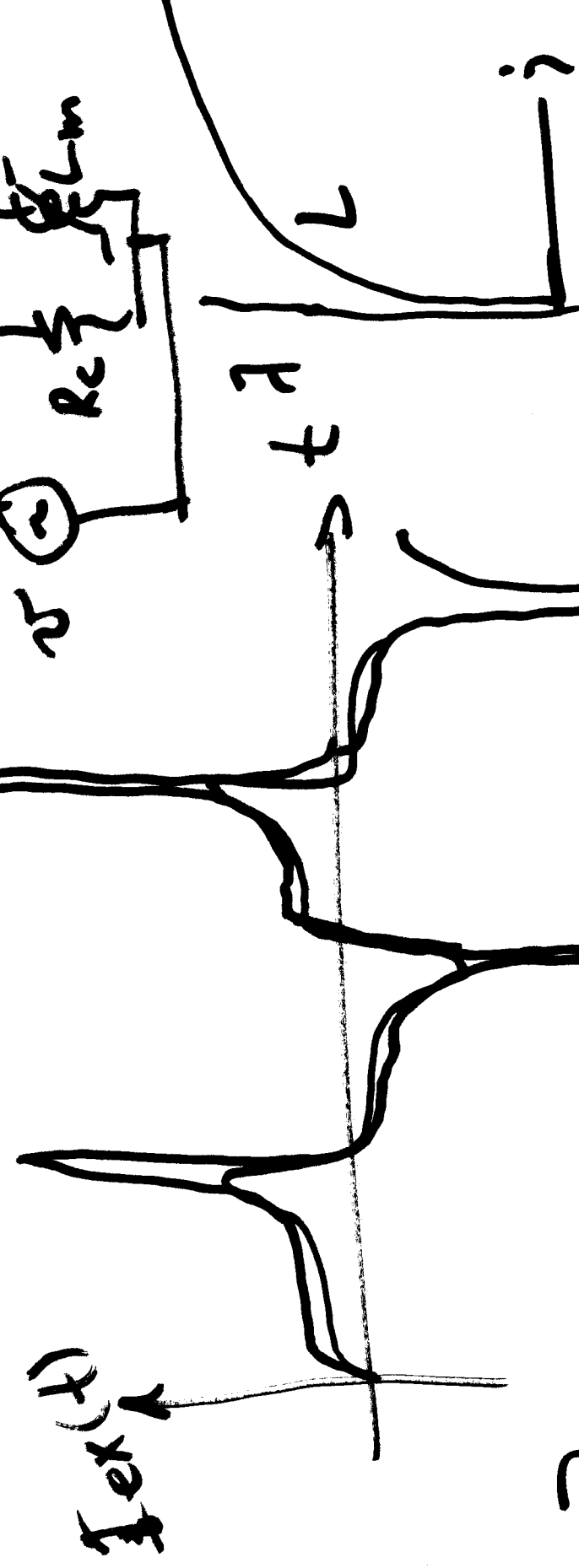
$|Z|$

10^5 pts/dec

601 pts
(discrete)

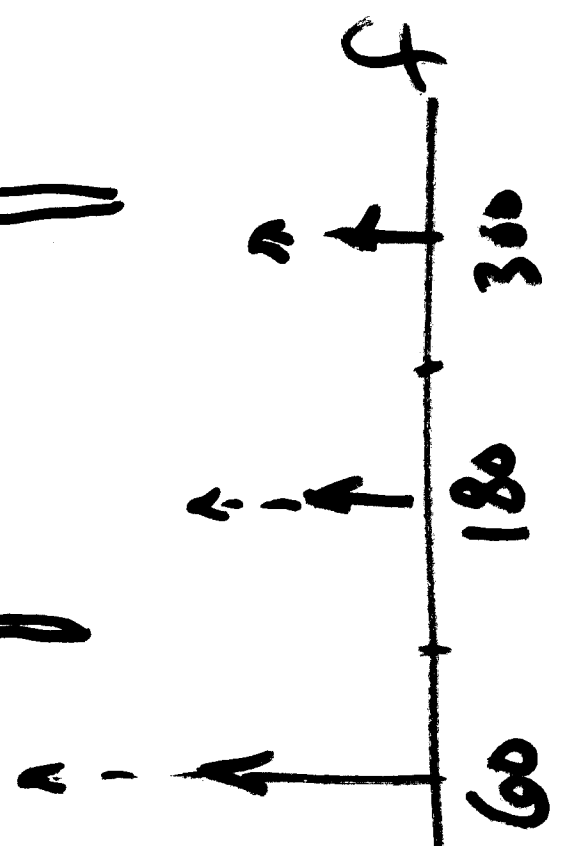
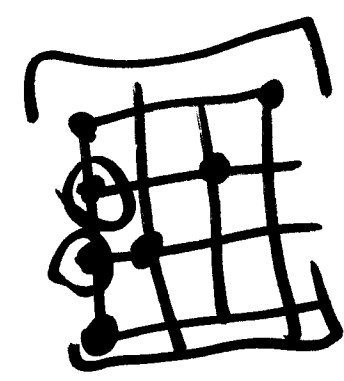


"Cause and effect"

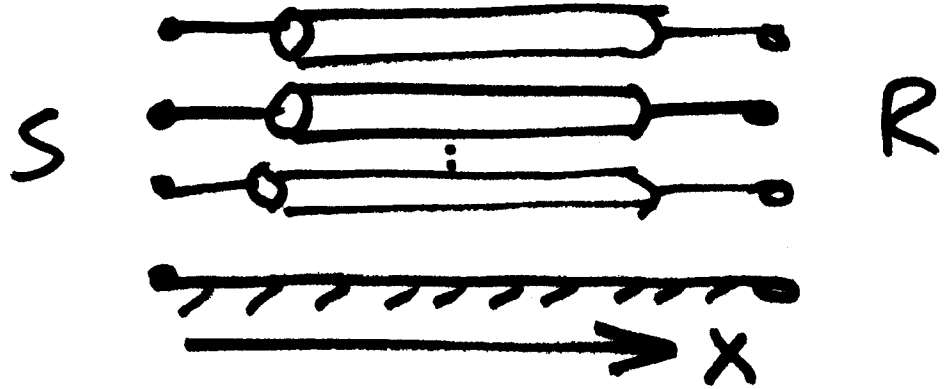


$i_{ex}(t)$

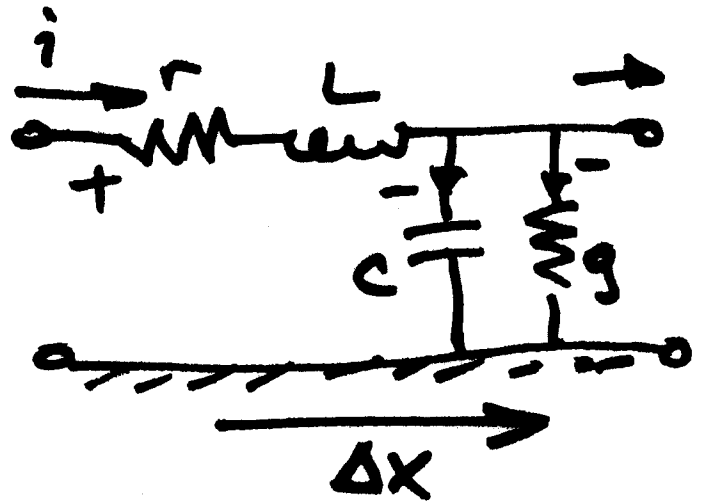
t



Multi-Conductor Line Models: 3



$$v = \begin{bmatrix} v_{AG} \\ v_{BG} \\ v_{CG} \end{bmatrix}$$



$$\begin{cases} -\frac{\partial v}{\partial x} = Zi \\ -\frac{\partial i}{\partial x} = Yv \end{cases}$$

$[Z] \neq [Y]$ are matrices

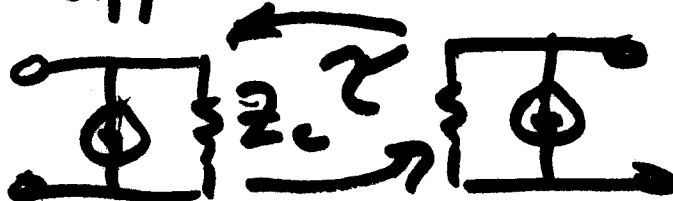
$[i] \neq [v]$ are vectors

$$Z_{ij} = R_{ij} + L_{ij} \frac{\partial}{\partial t}$$

$$y_{ij} = G_{ij} + C_{ij} \frac{\partial}{\partial t}$$

Problem:

- T-Line Eqs are developed in the frequency domain. - Coupled P's
- Must pick one freq that model is valid for, or use some type of fitting technique. - Beggs
- Freq Domain? - J. Marti
 - Can't use superposition for nonlinear or freq-dependent systems.
- Approach: Use convolution & deconvolution to move back & forth from Theo. freq-domain model to applied time-domain model.



Why continue in freq. domain? 5

- Tradition

- Numerical Efficiency

Approach - Choose a freq ω so $[Z]$ & $[Y]$ can be calculated. (convert to phasor domain).

$$-\frac{\partial V}{\partial x} = [Z][I] \quad Z_{ij} = R_{ij} + j\omega L_{ij}$$

$$-\frac{\partial I}{\partial x} = [Y][V] \quad Y_{ij} = G_{ij} + j\omega C_{ij}$$

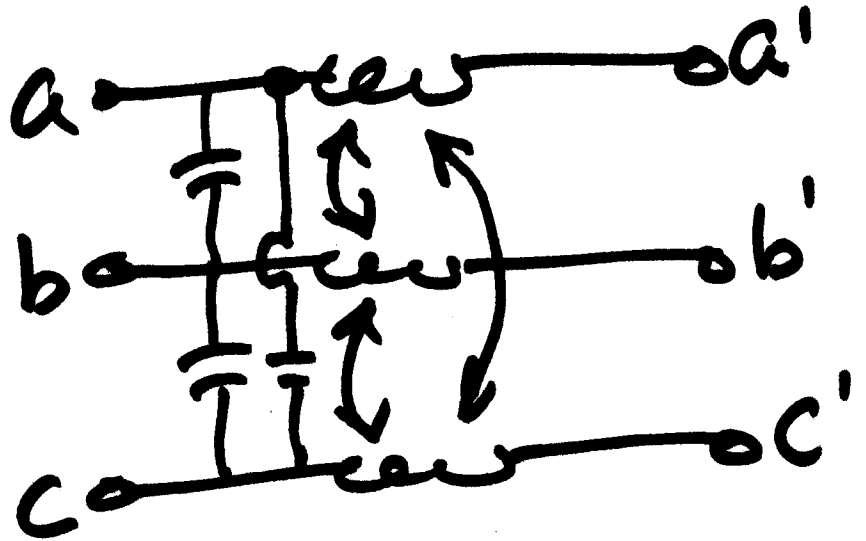
$$\frac{\partial^2 V}{\partial x^2} = \underline{\underline{[Z]}} \underline{\underline{[Y]}} [V]$$

$$\frac{\partial^2 I}{\partial x^2} = [Y] \underline{\underline{[Z]}} [I]$$

Consider structure of $[Z] \neq [Y] \in$

- ~~Sparse?~~

* - Full?



\Rightarrow All equations are "coupled" to all other equations!

Solution is computation-intensive

- Gauss Elim.

- Gauss-Jordan

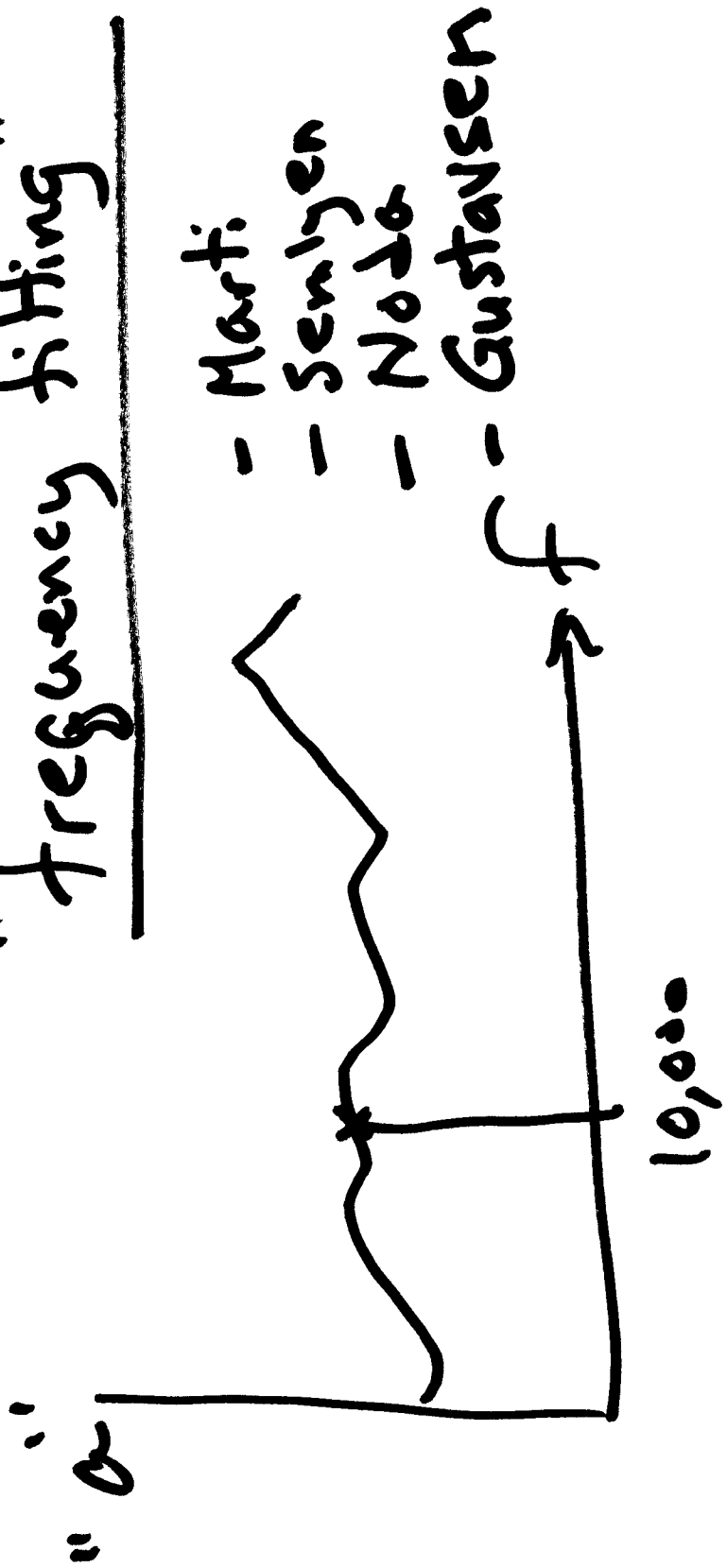
- LU Factorization \leftarrow **

It would help to "decouple" the family of equations.

(Also known as an "Orthogonal" set of equations).

Structurally this means that all off-diagonal terms of $[Z] \neq [Y] = 0$

"frequency fitting"



Freq weighting matrix

$$[Z_c] [a] \Rightarrow [Z_c] [f]$$

Method of decoupling:

7

MODAL Transformation

$$Ax = B$$

$$\begin{bmatrix} \textcircled{1} & \textcircled{0} & \textcircled{0} \\ \textcircled{0} & \textcircled{1} & \textcircled{0} \\ \textcircled{0} & \textcircled{0} & \textcircled{1} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix}$$

⇓ Transform

$$\begin{bmatrix} \textcircled{1} & - & - \\ - & \textcircled{1} & - \\ - & - & \textcircled{1} \end{bmatrix} \begin{bmatrix} x_{1,T} \\ x_{2,T} \\ x_{3,T} \end{bmatrix} = \begin{bmatrix} B_{1,T} \\ B_{2,T} \\ B_{3,T} \end{bmatrix}$$

⇓ undo transform

Reclaim x_1, x_2, x_3

Types of Modal Transforms

- Symm Comp: 0, 1, 2
 - Park's Transf: $d, q, 0$
 - Clarke's Transf: $\alpha, \beta, 0$
 - Karrenbauers: 0, 1, 2, ... $N-1$
- } 3-PT

General Idea

8

$$\underline{\underline{[V]}} = [T_v][V_m]$$

V_m = modal voltages

$[T_v]$ = Transform Matrix

$$[T_v] \frac{\partial^2 V_m}{\partial^2 x} = [Z][Y][T_v][V_m]$$

$$\frac{\partial^2 V_m}{\partial^2 x} = [T_v]^{-1}[Z][Y][T_v][V_m]$$

To cut to the chase:

choose $[T_v]$ as eigenvectors
of $[Z][Y]$

$$[T_v]^{-1}[Z][Y][T_v] = [\Lambda] = \begin{bmatrix} \lambda_1 & 0 & \dots & 0 \\ 0 & \lambda_2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \dots & 0 & \lambda_n \end{bmatrix}$$