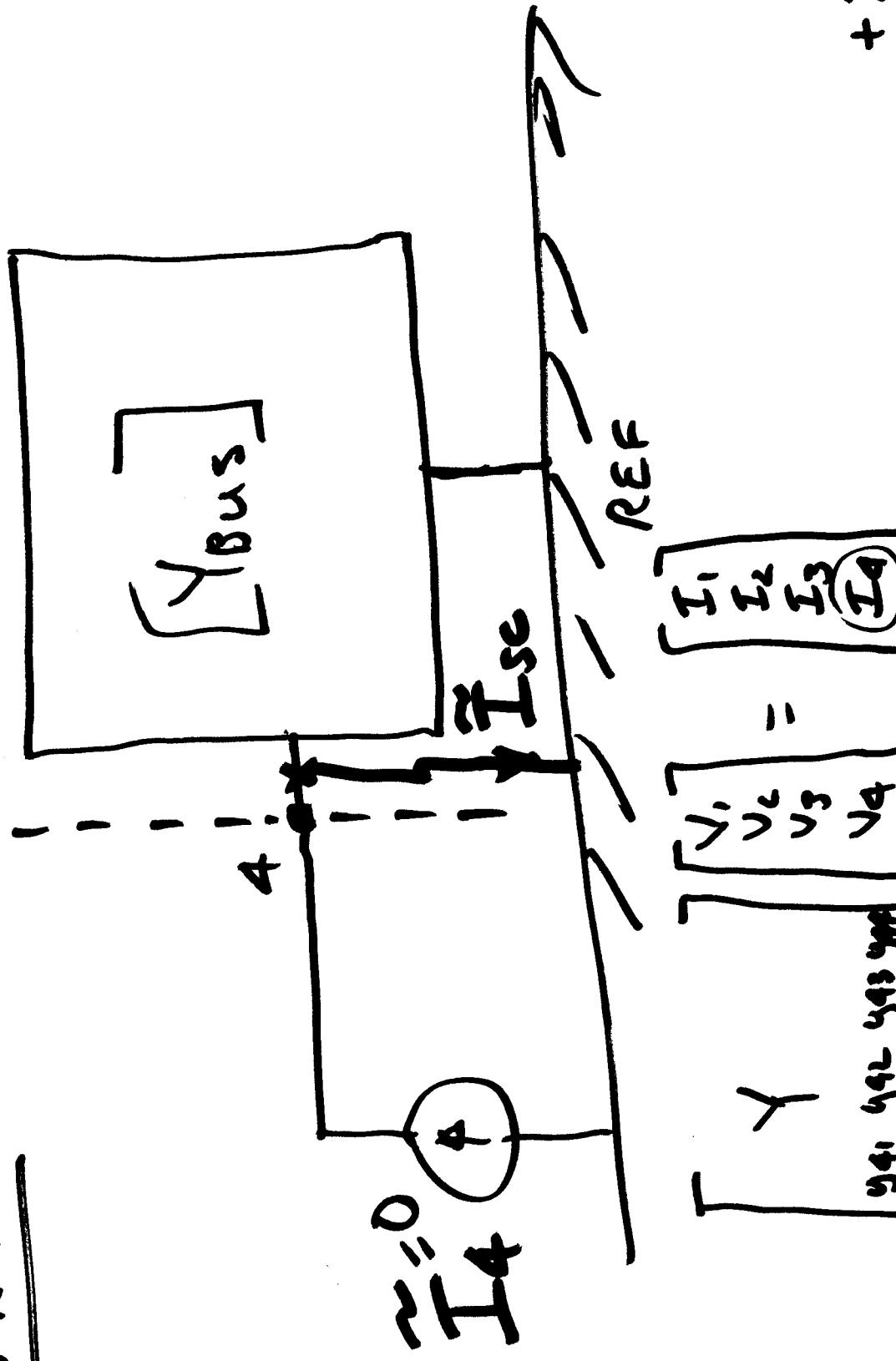


Topics for Today:

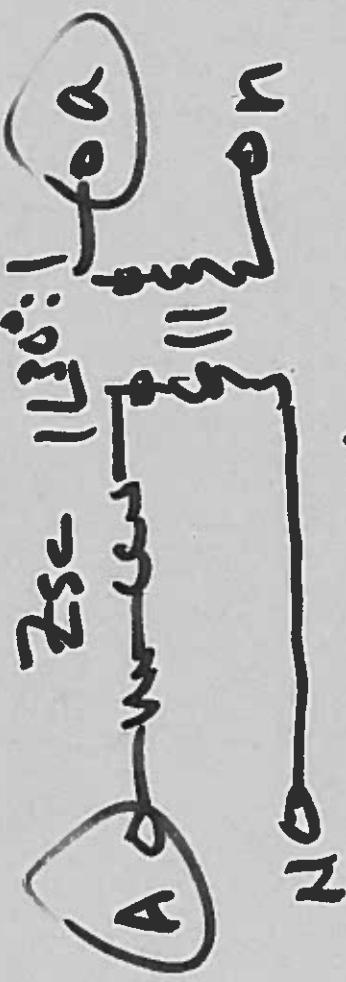
- Questions from last lectures?
- Comments on Homework #2
 - Augmentation for L-G Fault - signs !
- Today - system data for computer studies
 - Transformer Data
 - More on tap-changing transformers
- Coming up - keep studying Chapters 3 & 4.
 - Nonlinear systems of equations
 - Newton Iterative Method
 - Newton-Raphson Load Flow Formulation
 - Everybody have access to Aspen?

HWK #2



$$I_4 = y_{41}V_1 + y_{42}V_2 + y_{43}V_3 + y_{44}\sqrt{4} + I_{sc}$$

- * - Not matching P.U. Base Voltages
- * - LTC / TCU_L (V_1, Q)
- * - Phase-shifting $\times f_{mu}$ (P)
- Phase-shifting
- * - Per Phase Cables - $\Delta-\gamma$ phase shifts



$$\Rightarrow \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

A hand-drawn equation showing the transformation of currents from a primary side to a secondary side. On the left, there is a right-pointing arrow above a bracket containing three variables: y_1 , y_2 , and y_3 . To the right of the arrow is an equals sign followed by a bracketed matrix multiplication. The matrix is $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix}$, and it is multiplied by a column vector $\begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$.

EE 5240 - Lecture 7 - Incorporation of Transformers into [Ybus]
(extracted from lectures 5,6,8 of archive notes)

XFMRs - Use Δ $L-N$
Per Phase Equiv.



In $[Y_{bus}]$ $y_{56} = -\frac{1}{266}$

Basis 2-winding
 $XFMR$ is simple.

How about?

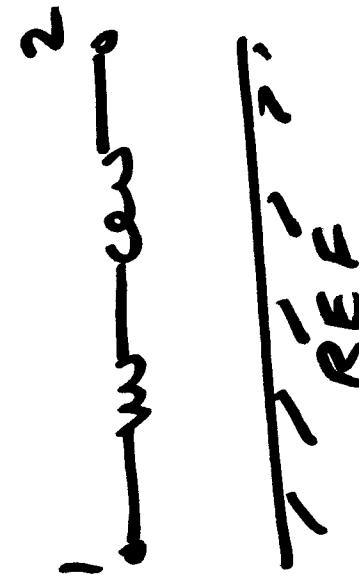
- LTC (or τ_{cuL})
- Phase Shifter (ρ_s)

Basic Approach: Develop π -Equiv and handle just like T-Line.

One-Line:

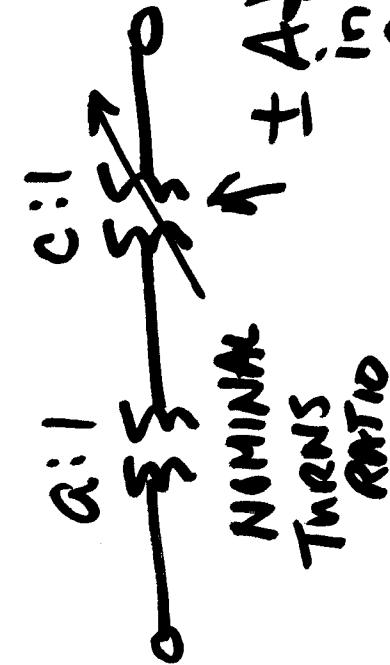


per-unit per-phase



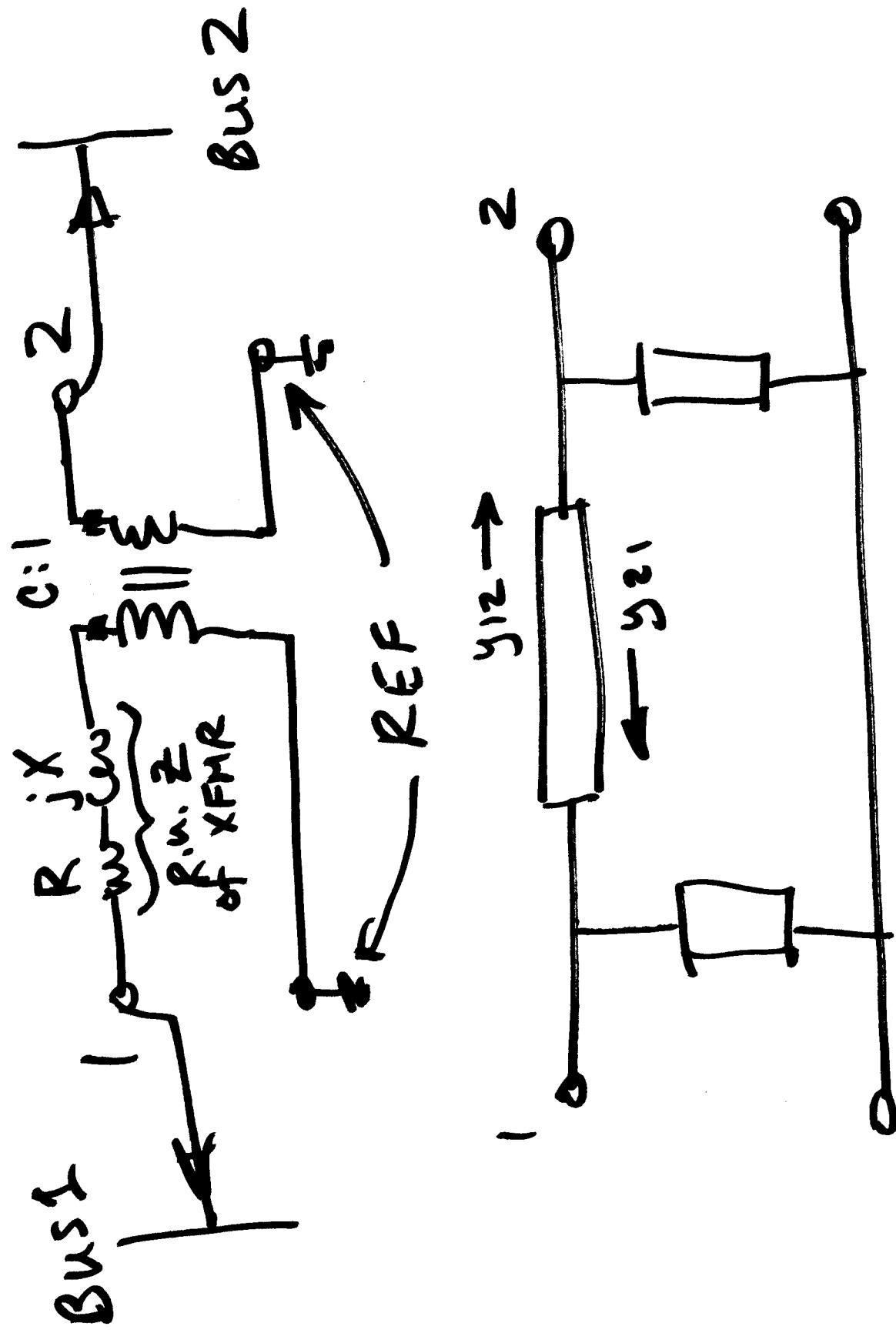
Tap-Changers

- LTC's
- Phase-Shift

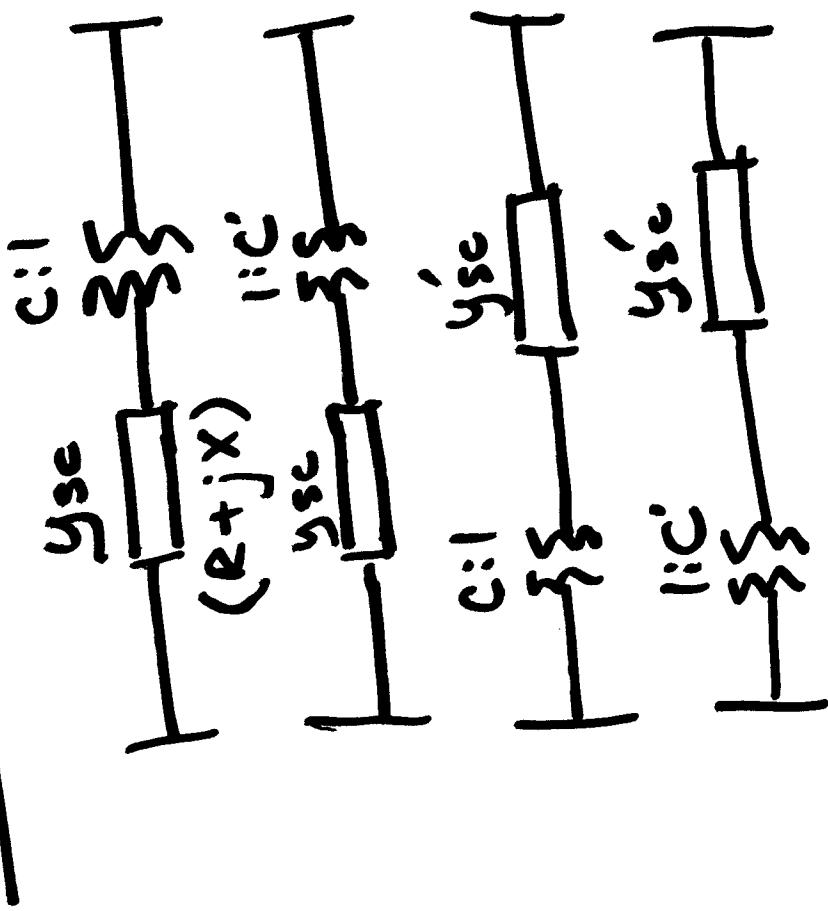


+ Adjustment
in phase angle (ψ_S)
or volt mag ($|T_C|$)

Note: a:1 represents nominal turns ratio, i.e. the ratio between the base voltages of the per unit system. Taken in the context of a per unit system, a=1 and the transformer can be represented as a simple series impedance. c:1 represents the off-nominal turns ratio, and so its effect must be included in [Ybus].



Tap Changing XFRS - Variations (P.u. representations)



①

②

③

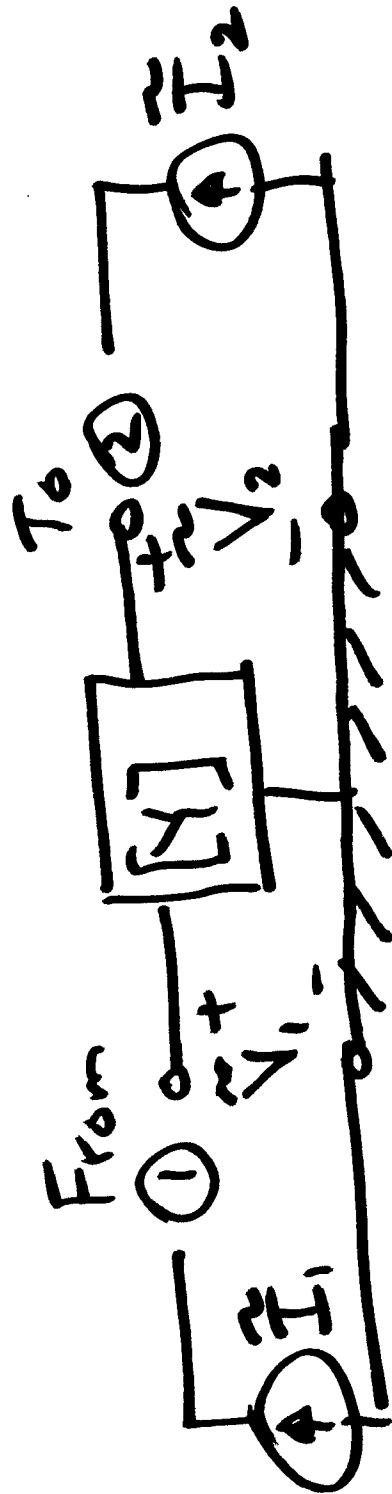
④

"C" is off-nominal turns ratio. In general C is complex.

C is real for LTC.
C is complex for PS.

If $|C| \neq 1$ then magnitude change.

If C is complex, Phase shift.

Standard Approach:

$$\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$\begin{aligned} y_{11} &= y_{SER} + y_{SH1} \\ y_{12} &= y_{SER} \\ y_{21} &= y_{SER} \\ y_{22} &= y_{SER} + y_{SH2} \end{aligned}$$

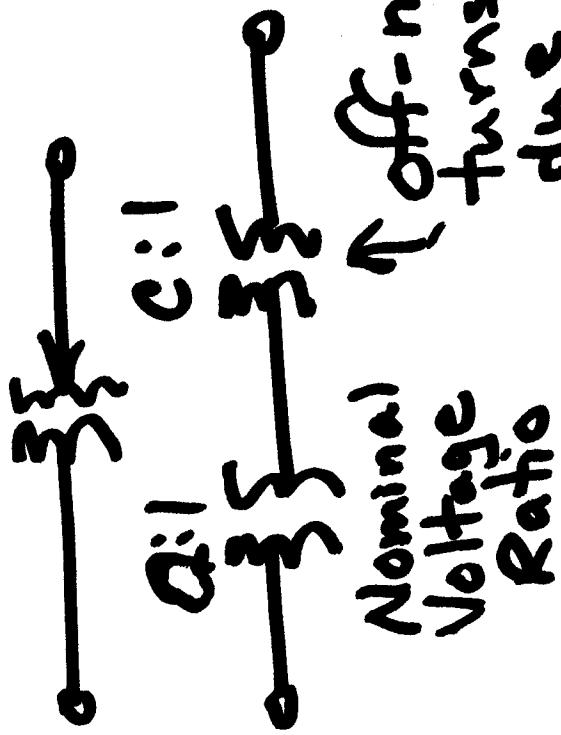


a

TAP-CHANGERS

On One-Line Diagrams:

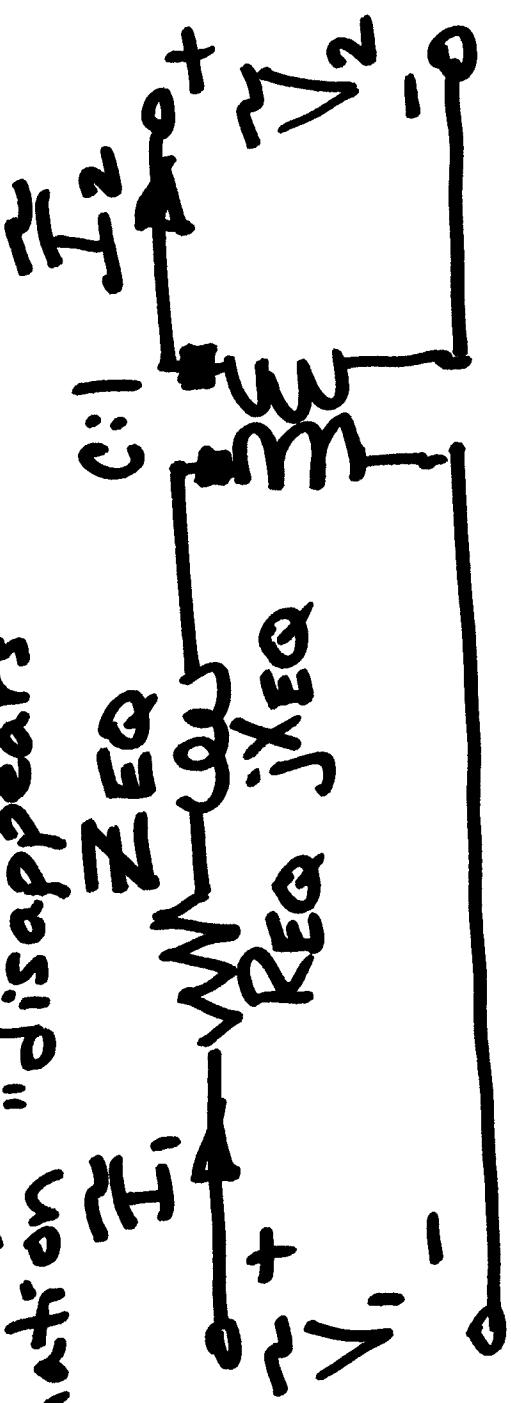
Conceptually:



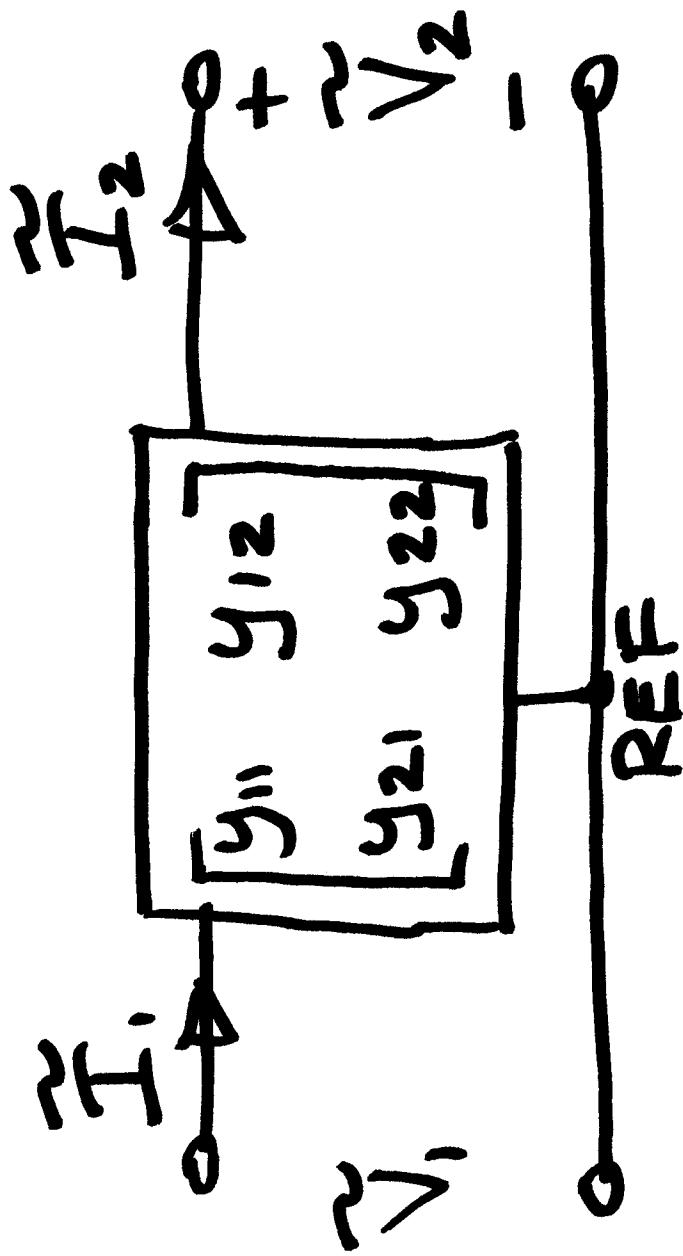
↑ off-nominal turns ratio
due to Tap Changer

Nominal
Voltage
Ratio

In per unit, nominal
transformation \tilde{I}_1



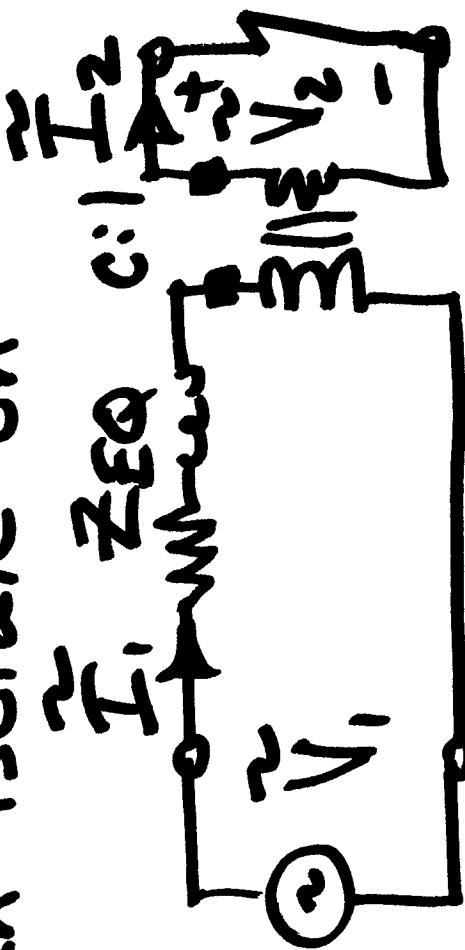
Generally, we can describe this b
as a 2-node $\begin{bmatrix} \gamma \end{bmatrix}$



where

$$\begin{bmatrix} \tilde{Y}_1 \\ \tilde{Y}_2 \end{bmatrix} = \begin{bmatrix} \tilde{I}_1 & -\tilde{I}_2 \\ -\tilde{I}_2 & \tilde{I}_1 \end{bmatrix}$$

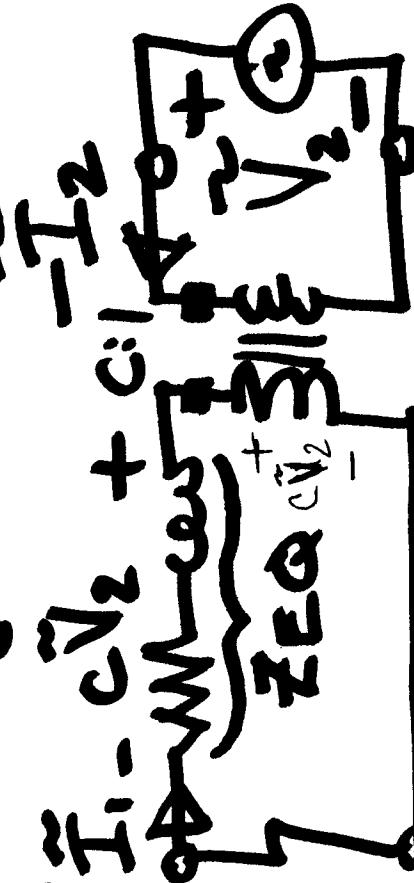
Strategically using shorts we can isolate on the values of $[Y]$.



$$y_{11} = \frac{\tilde{I}_1}{V_1} \Big|_{V_2=0} = \frac{1}{Z_{EQ}}$$

$$Y_{EQ}$$

$$= -\frac{\tilde{I}_1 + jX_{EQ}}{R_{EQ} + jX_{EQ}}$$



$$y_{22} = -\frac{\tilde{I}_2}{V_2} \Big|_{V_1=0}$$

$$= -\frac{Z_{EQ}/|C|^2}{Z_{EQ}/|C|^2} = |C|^2 Y_{EQ}$$

$$Y_{12}^* = \frac{\tilde{I}_1 / V_2}{V_1 = 0} = -\frac{-C \tilde{V}_2 / Z_{EQ}}{V_2} = -C Y_{EQ}$$

$$Y_{21} = \left| \frac{-\tilde{I}_2 / V_1}{V_2 = 0} \right| = \frac{\tilde{I}_2}{V_1}$$

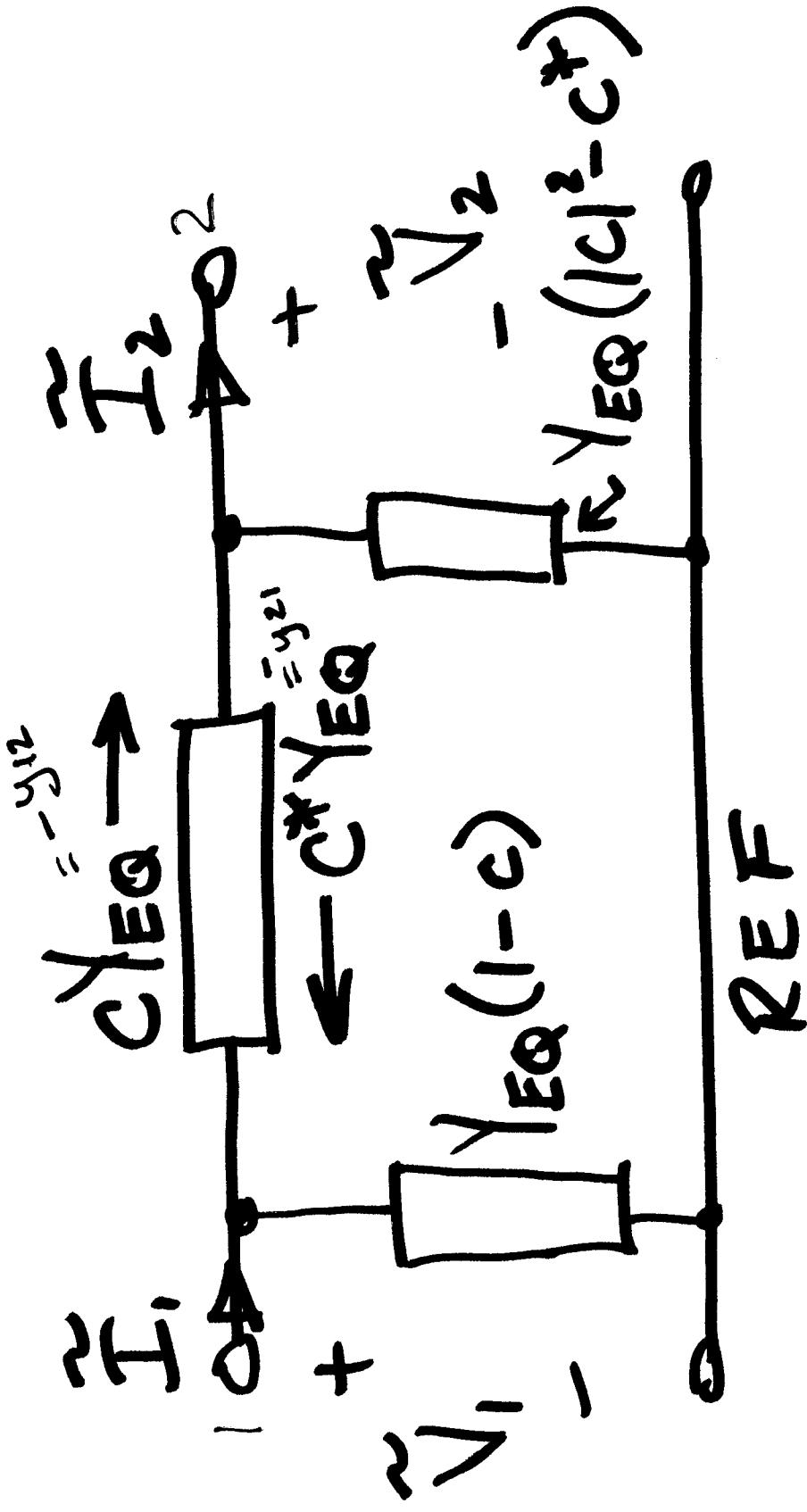
$$= -\frac{-C^* \tilde{V}_1 / Z_{EQ}}{V_1} = C^* Y_{EQ}$$

Note: Ideal XFR, by definition, has "C" is voltage ratio.

$C = \frac{V_2}{I_1} = \frac{V_2}{\tilde{I}_1^*} = \frac{V_2 \tilde{I}_2^*}{\tilde{I}_1^* \tilde{I}_2^*} = \frac{V_2 \tilde{I}_2^*}{V_1 \tilde{I}_1^*} = \frac{V_2}{V_1} = \frac{V_{out}}{V_1}$

e)
If we "reverse engineer" our  into an equivalent 2-bus network, then

then



Observations:

- LTC (τ_{CuL}) has a c that is Real.
 - \therefore Transfer Admittances
- $CY_{EQ} = C^* Y_{EQ}$
 \Rightarrow Bilateral. ($y_{12} = y_{21}$)
- Phase - Shifter (ρ_S) has complex c.
 - \therefore Transfer admittances
- $CY_{EQ} \neq C^* Y_{EQ}$
 - $y_{12} \neq y_{21}$
 - $\boxed{[Y]}$ not symm.
 - Not Bilateral.
 - about main diag.