



1D Unsteady Heat Transfer: In a Slab

Pum 2 unsteady  
"Short-cut" solns

**Example:** A long, wide rectangular slab of butter (46 mm thick) at  $4.4^{\circ}\text{C}$  is removed from refrigeration and placed on a table at room temperature. After five hours, what are the butter temperatures at the middle of the slab and at the bottom of the slab (in contact with the table)?

Properties of butter:

$$k_{butter} = 0.197 \frac{\text{W}}{\text{mK}}$$

$$\hat{C}_{p,butter} = 2.30 \frac{\text{kJ}}{\text{kg K}}$$

$$\rho_{butter} = 998 \frac{\text{kg}}{\text{m}^3}$$

Conditions of the room:

$$T_{bulk} = 24^{\circ}\text{C}$$

$$h_{conv} = 8.5 \frac{\text{W}}{\text{m}^2\text{K}}$$

# butler warming:

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The **Equation of Energy** for systems with **constant k**

**Microscopic energy balance**, constant thermal conductivity; Gibbs notation

$$\rho \hat{C}_p \left( \frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S_e$$

**Microscopic energy balance**, constant thermal conductivity; Cartesian coordinates

$$\rho \hat{C}_p \left( \frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) = k \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + S_e$$

**Microscopic energy balance**, constant thermal conductivity; cylindrical coordinates

$$\rho \hat{C}_p \left( \frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} \right) = k \left( \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + S_e$$

**Microscopic energy balance**, constant thermal conductivity; spherical coordinates

$$\rho \hat{C}_p \left( \frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} \right) = k \left( \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + S_e$$

no rxn  
no elec  
current

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \frac{\partial^2 T}{\partial x^2} \quad (\text{familiar})$$

IC:  $t < 0 \quad T = T_0 \quad \forall x$

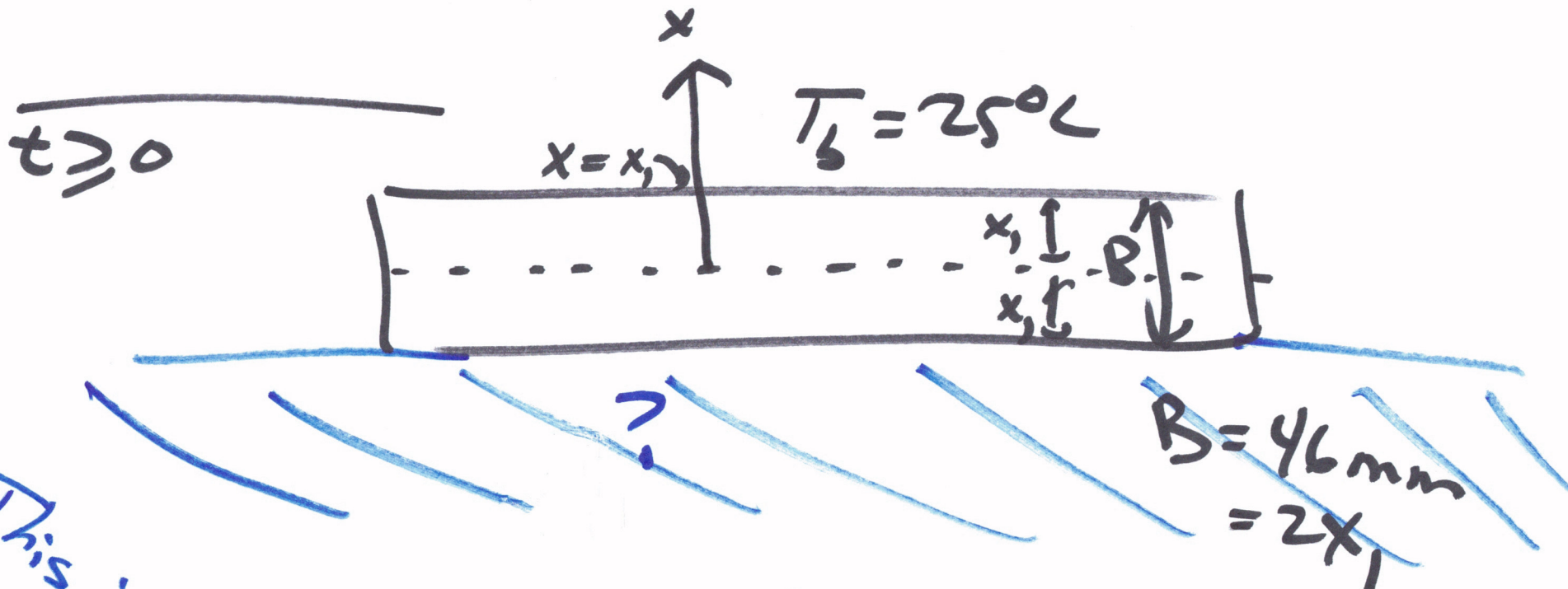
BC: top - Newton's law of cooling  
bottom - ??

Reference: F. A. Morrison, "Web Appendix to An Introduction to Fluid Mechanics," Cambridge University Press, New York, 2013 ([pages.mtu.edu/~fmorriso/cm310/IFMWebAppendixDMicroEBalanceMorrison.pdf](http://pages.mtu.edu/~fmorriso/cm310/IFMWebAppendixDMicroEBalanceMorrison.pdf)). This worksheet is on the web at [pages.mtu.edu/~fmorriso/cm310/energy.pdf](http://pages.mtu.edu/~fmorriso/cm310/energy.pdf).

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$t < 0$

$T_0 = 4.4^\circ\text{C}$



This is a "new" case  
std BC

$x = x_1$

$$\left| \frac{q_x}{A} \right| = h |T_b - T|$$

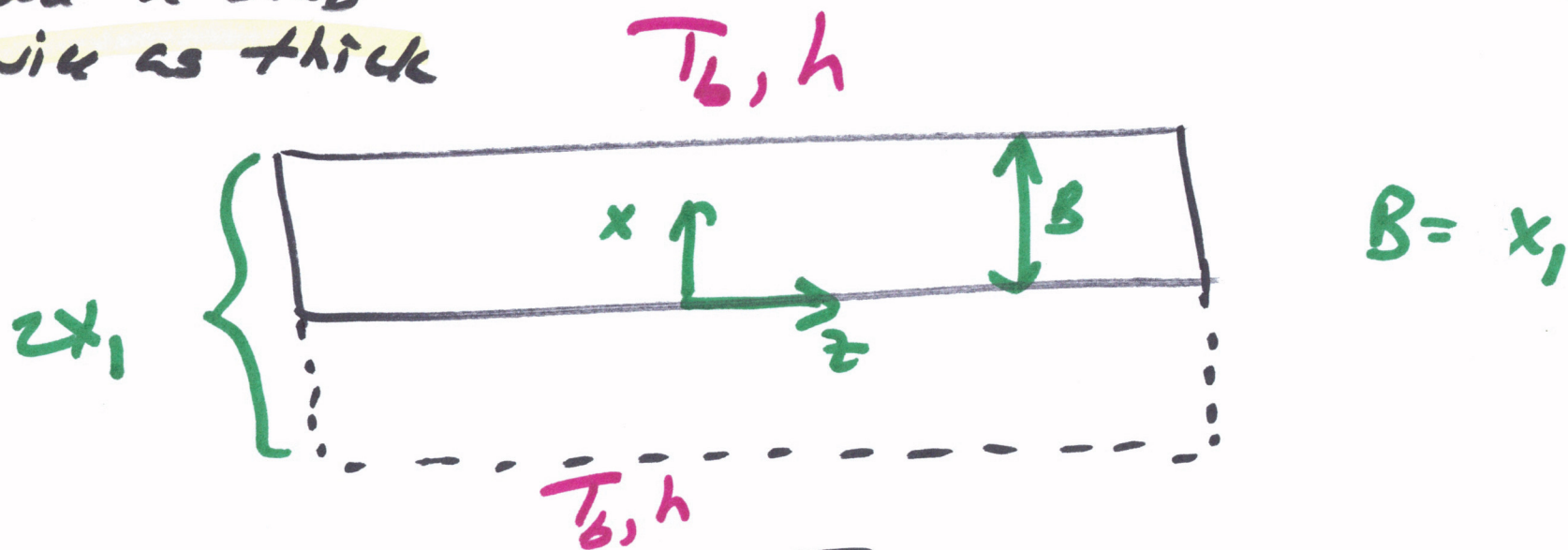
$x = 0$

$$\frac{q_x}{A} = 0$$

To match w/ Gurrey-Lurie:

★ Model a slab  
twice as thick

(4)



$$x = B \quad -k \frac{dT}{dx} = h(T - T_b)$$

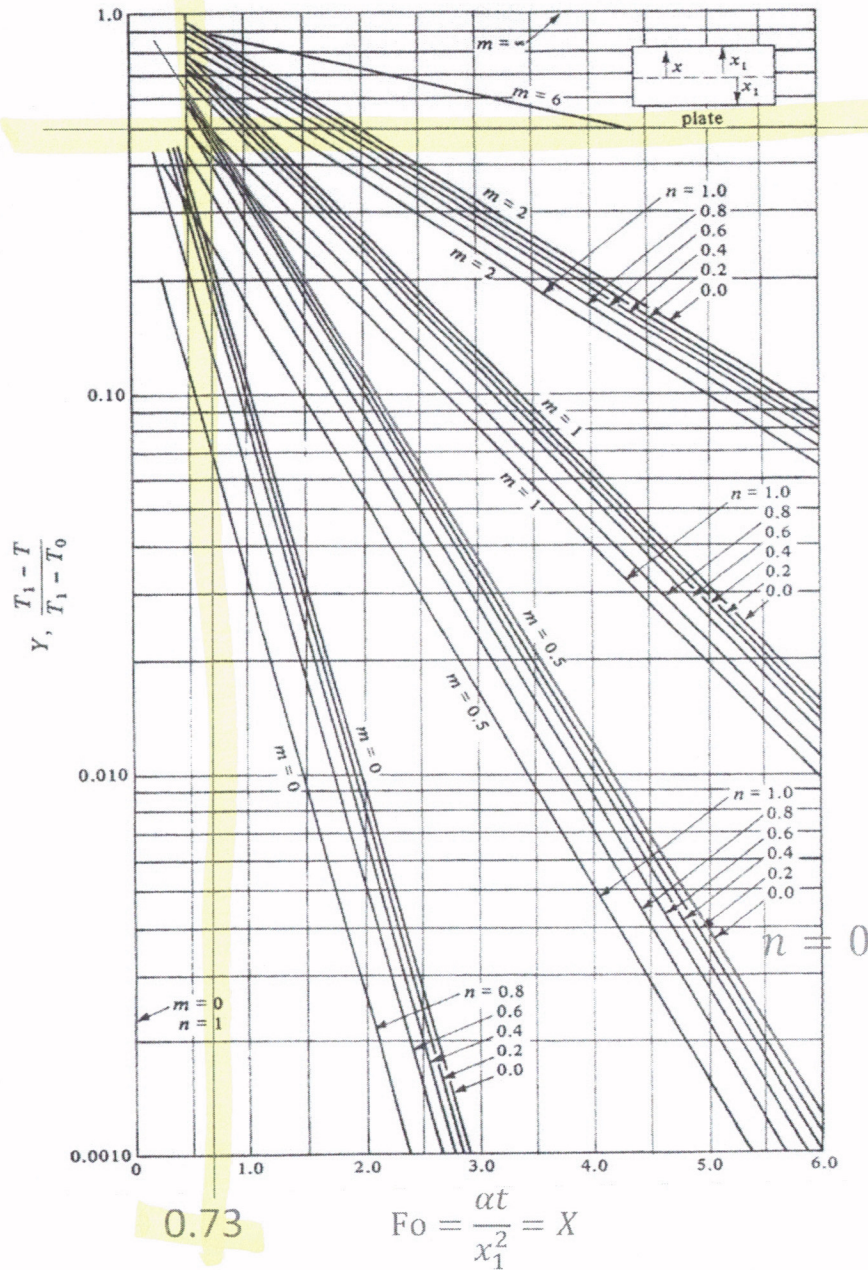
$$x = 0 \quad \frac{q_x}{A} = 0$$

This set  
up forces  
the correct BC  
at the bottom of the real slab.

(equivalent to  $x = -B$ ,

Newton's law of  
cooling)

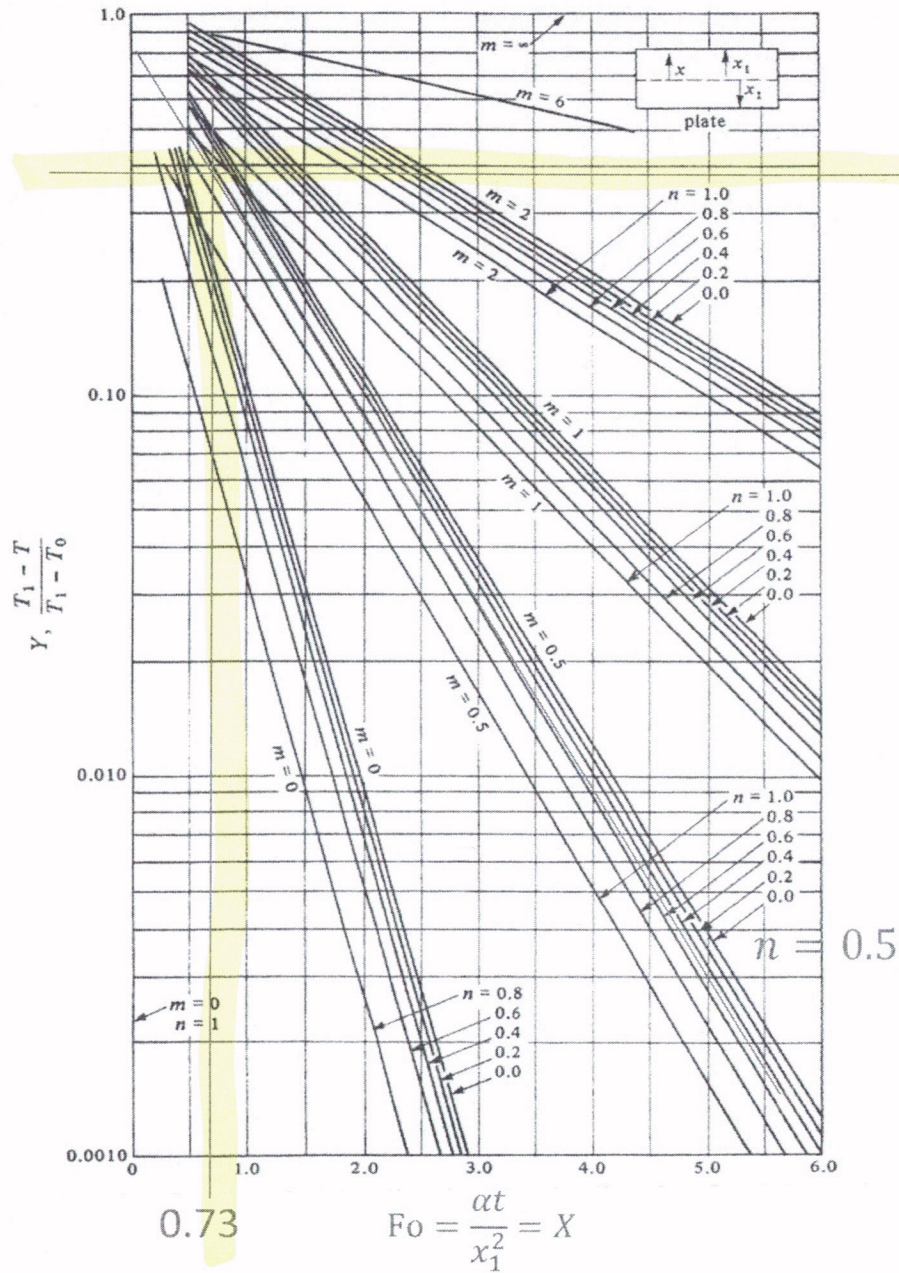
At the bottom,  $x = 0$



$$\frac{T_1 - T}{T_1 - T_0} = 0.5$$

$$T = 14^\circ C$$

Ref: Geankoplis, 4<sup>th</sup> Ed, 2003



$$\frac{T_1 - T}{T_1 - T_0} = 0.38$$

$$T = 17^\circ\text{C}$$

Ref: Geankoplis, 4<sup>th</sup> Ed, 2003