



Requests for today?

②

✓ • 2.11 Blocks of snow - troubleshooting

↘ • 2.9 Determine largest shaft diameter

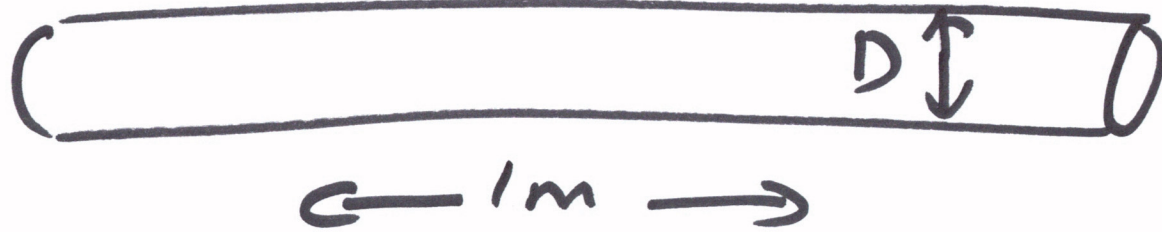
①

- try Gurney Lurie
- turn to semi-infinite slab

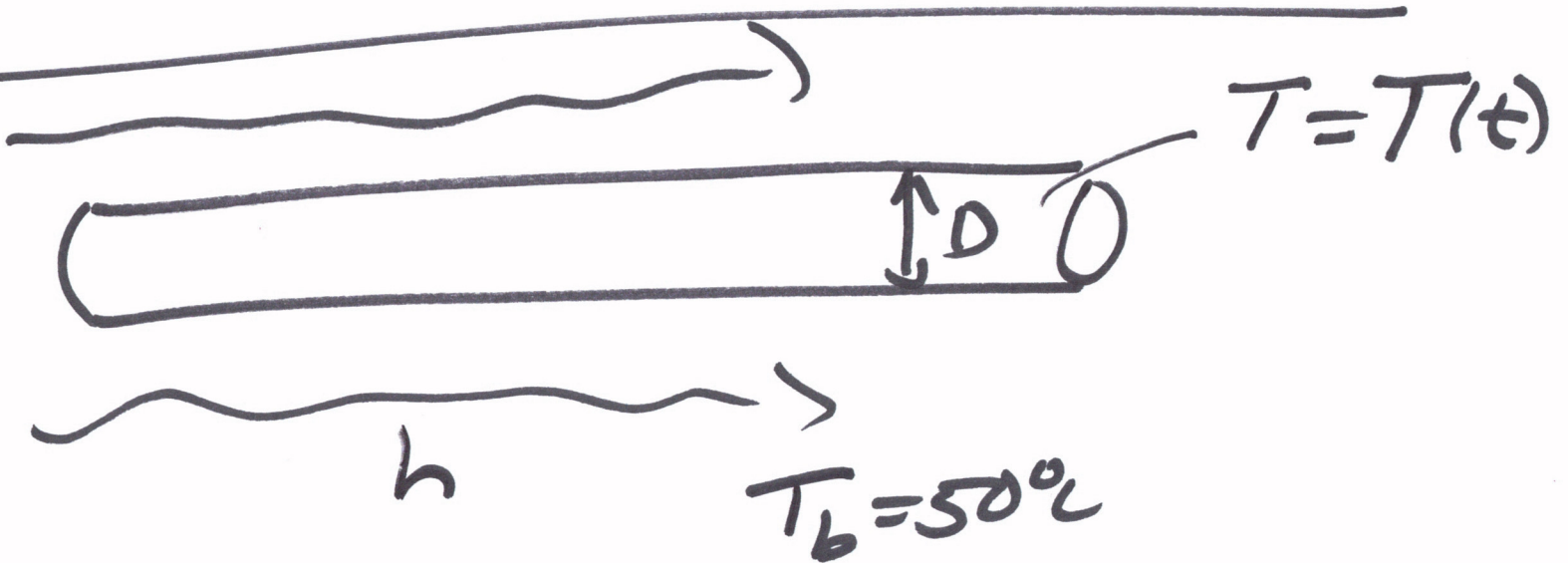
2.9

Q

$t < 0$
 $T = T_0$
 $= 400^\circ\text{C}$



Suddenly:

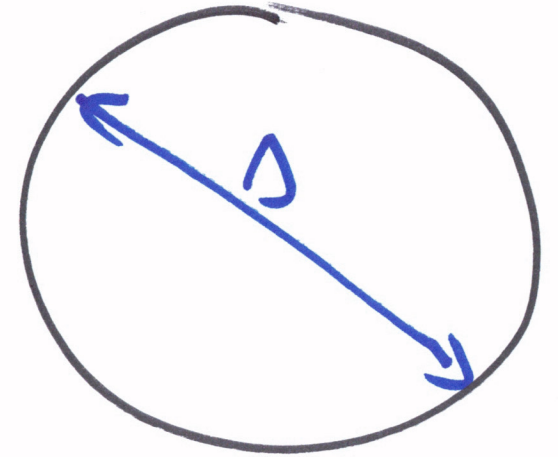


Biot # organizes what we see:

(2)

(ratio
of
resistances)

$$Bi = \frac{h D_{char}}{k_{solid}} = \frac{\frac{D}{k}}{\frac{1}{h}}$$



★
lumped
parameter
case

Bi small

T is uniform
w/in object

Bi medium

Bi large

$$T_w = T_b$$

criterion for lumped parameter case:

$$Bi = \frac{h D_{char}}{k} < 0.1$$

(3)

know \rightarrow

$$0.1 = \frac{h}{k} \frac{V}{A}$$

\leftarrow ~~$\pi R^2 L$~~

\leftarrow ~~$2\pi R L$~~

$$D_{char} = \frac{V}{SA}$$

\uparrow
surface area

Solve for $R = 2.5 \text{ cm}$

$$D_{char} = 5 \text{ cm}$$

second problem

(2)

2.11

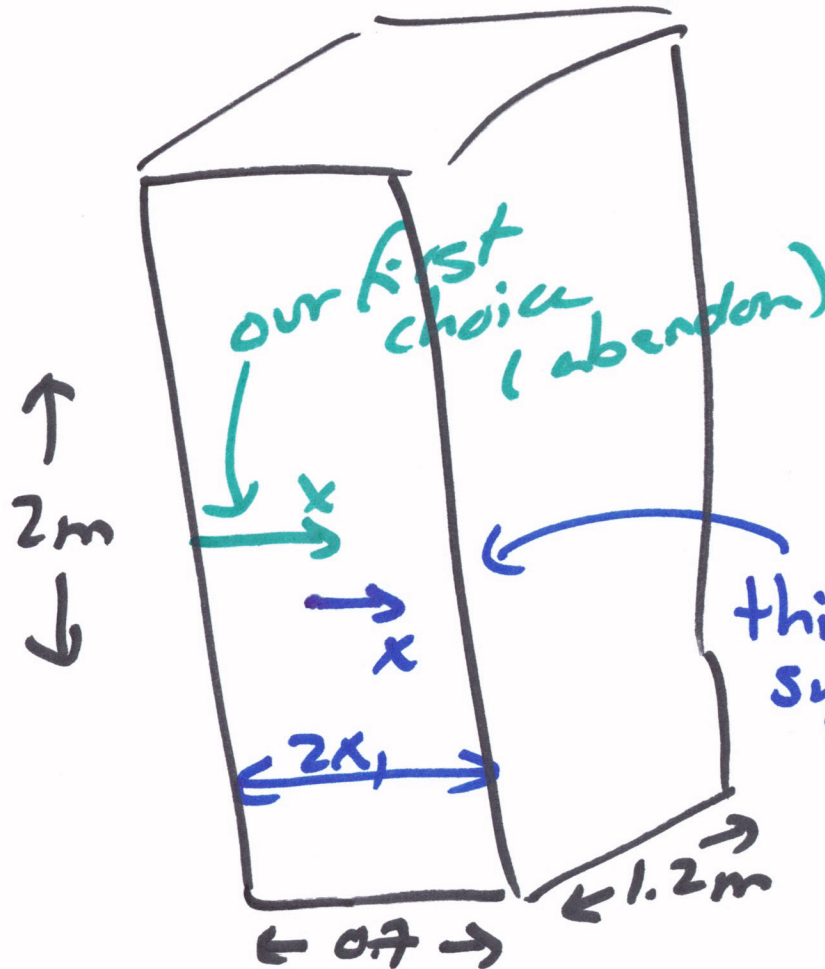
Blocks of compacted snow (dimensions 2 meters by 1.2 meters by 0.7 meters) are created to form part of a wintertime festive display (Winter Carnival). The weather has been such that the blocks are at a uniform temperature of -10.0°C . If the weather turns unseasonably warm (7.0°C) what will be the temperature near the surface of the block (5 and 10 centimeters from the surface) after 0.5 hours?

$$t < 0$$
$$T = T_0 \quad \forall x, y, z$$

Suddenly,

$$t \geq 0$$

$$T_b$$



$$t = 0.5 \text{ h}$$
$$x_1 = 5 \text{ cm}$$
$$x_2 = 10 \text{ cm}$$

$$T(x, y, z, t)$$

this coord system is required by G-L chart

11. Blocks of compacted snow (dimensions 2 meters by 1.2 meters by 0.7 meters) are created to form part of a wintertime festive display (Winter Carnival). The weather has been such that the blocks are at a uniform temperature of -10.0°C . If the weather turns unseasonably warm (7.0°C) what will be the temperature near the surface of the block (5 and 10 centimeters from the surface) after 0.5 hours?

Physical property data for compacted snow: $k = 0.54 \frac{\text{W}}{\text{mK}}$, $\rho = 68 \frac{\text{kg}}{\text{m}^3}$, $\hat{C}_p = 2090 \frac{\text{J}}{\text{kgK}}$. The heat transfer coefficient under the prevailing weather conditions may be estimated to be $12 \text{W}/\text{m}^2\text{K}$. Answers: 5 cm, -2.5°C ; 10 cm, -6°C

physical property data provided

$$\alpha = \frac{k}{\rho C_p} = 3.8 \times 10^{-6} \text{ m}^2/\text{s}$$

(but may be approximate)

The **Equation of Energy** for systems with **constant k**

Microscopic energy balance, constant thermal conductivity; Gibbs notation

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S_e$$

Microscopic energy balance, constant thermal conductivity; Cartesian coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + S_e$$

Microscopic energy balance, constant thermal conductivity; cylindrical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + S_e$$

Microscopic energy balance, constant thermal conductivity; spherical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} \right) = k \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + S_e$$

no rxn
no current

Solid
v=0

1D
rect

heat
conduction

IC: $t \leq 0 \quad T = T_0 \quad \forall x$

BC: $t > 0 \quad \frac{\partial x}{\partial A} = 0 \quad x = 0$

$x = x_1, \quad \left| \frac{\partial x}{\partial A} \right| = h (T_b - T_w)$

Reference: F. A. Morrison, "Web Appendix to An Introduction to Fluid Mechanics," Cambridge University Press, New York, 2013 (pages.mtu.edu/~fmorriso/cm310/IFMWebAppendixDMicroEBalanceMorrison.pdf). This worksheet is on the web at pages.mtu.edu/~fmorriso/cm310/energy.pdf.

try Gurney Lurie
or² semi infinite slab



1D Unsteady Heat Transfer: Finite Bodies

Finite 1D Unsteady Heat Transfer, $T = T(t, x)$ or $T = T(t, r)$

Initial: Uniform initial temperature T_0 ; BC: exposed to bulk temperature T_1 ; h known

- Flat plate long, wide, thickness = $2x_1$ $T = T(t, x)$ $Y = Y(X, n)$
- Cylinder long, radius = x_1 $T = T(t, r)$ $Y = Y(X, n)$
- Sphere radius = x_1 $T = T(t, r)$ $Y = Y(X, n)$

The Gurney-Lurie charts may work for us:

$$Bi = \frac{hD_{char}}{k} = \frac{hx_1}{k} = \frac{1}{m}$$

$$Fo = \frac{\alpha t}{x_1^2} = X$$

$$\frac{x}{x_1} = \frac{r}{x_1} = n$$

$$\frac{T_1 - T}{T_1 - T_0} = Y \quad \left(\frac{T - T_0}{T_1 - T_0} = 1 - Y \right)$$

70°C

-10°C

Note:

$$D_{char} = x_1, \quad \underline{\text{NOT } V/A}$$

TRY GURNEY-LURIE CHART

(8)

slab

$$2X_1 = 0.7$$

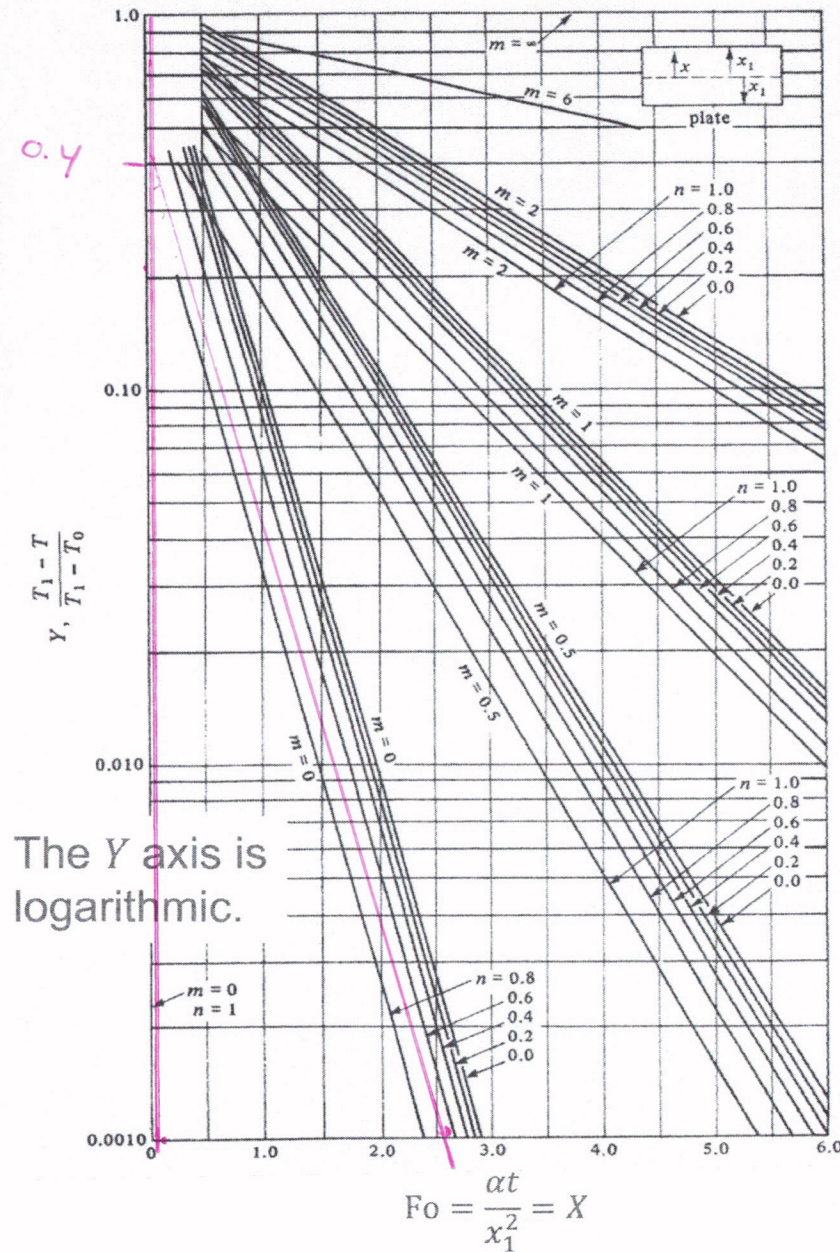
$$X_1 = 0.35 \text{ m}$$



$$m = \frac{l}{Bi} = \frac{k}{hD} = \frac{k}{hx_1} = 0.13 = m$$

$$n = \frac{x}{x_1} = \frac{0.35 - 0.05}{0.35} = 0.86 = 0.9$$

$$F_0 = \frac{\alpha t}{x_1^2} = \frac{3.8 \times 10^{-6} \frac{\text{m}^2}{\text{s}} (1800 \text{ s})}{(0.35 \text{ m})^2} = 0.056 = F_0$$



Gurney and Lurie Chart Finite 1D Unsteady Heat Transfer

Initial: Uniform initial temperature T_0

BC: Exposed to bulk temperature T_1

h known

- Flat plate, long, wide
- thickness $2x_1$
- $T = T(t, x)$
- $Y = Y\left(Fo, n = \frac{x}{x_1}\right)$

$$T\left(m = \frac{1}{Bi}, n = \frac{x}{x_1}, Fo\right)$$

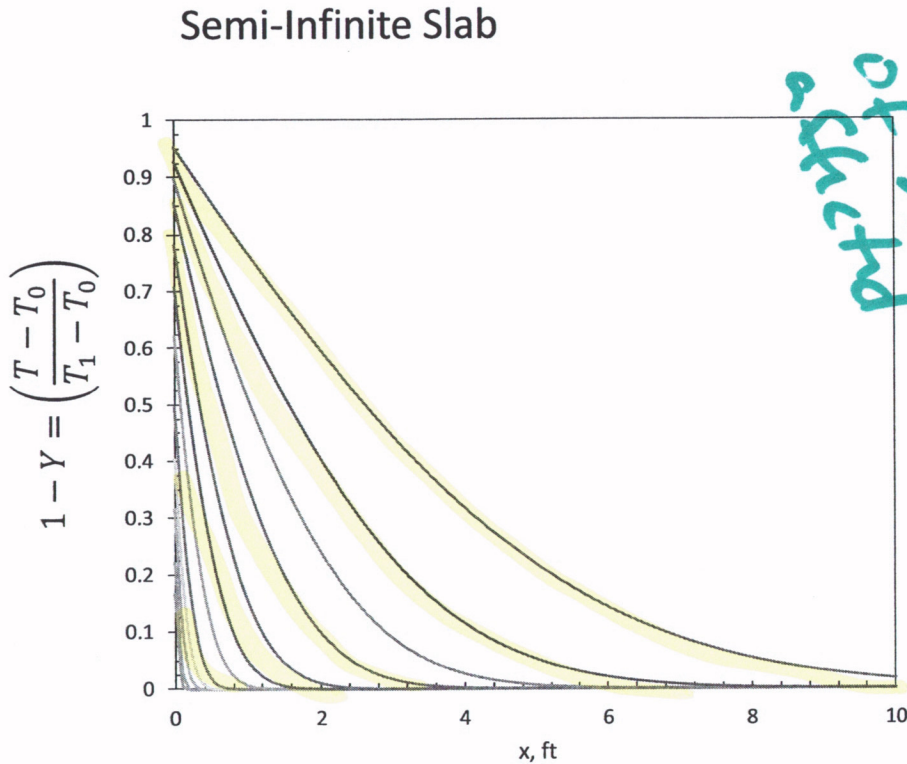
$m = 0.1 = 0$
 $n = 0.9 \sim 1$

$Fo = 0.06$

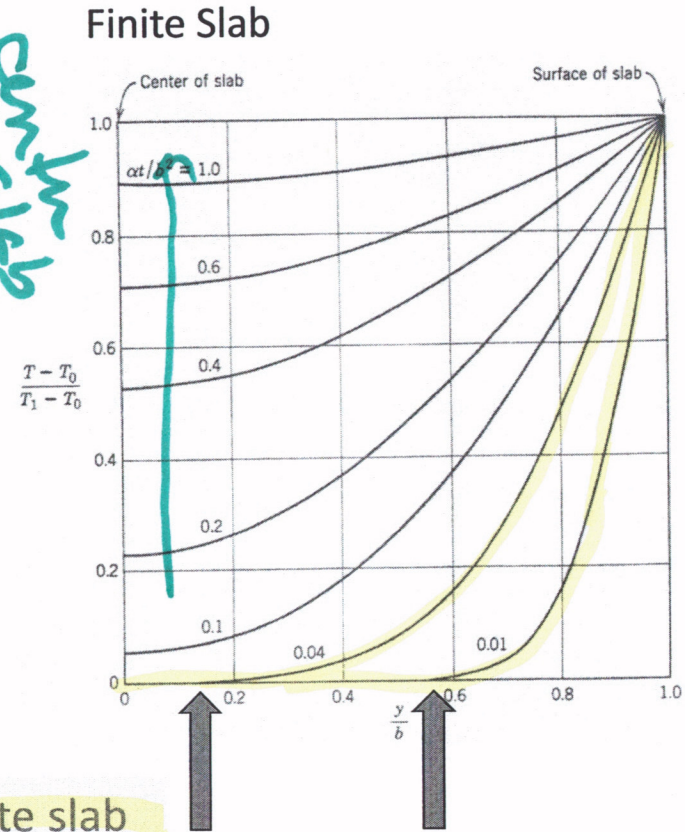
Not on the chart!

The question is about short times + locations near the surface - maybe the semi infinite slab is a better picture

Note: We can use the semi-infinite slab solution for finite slabs, within limits



perfectly correct



BSL1, p356, 1960

For some cases, the finite slab looks semi-infinite

- Short time
- Thicker slab

The temp change at most is by $T_1 - T_0$ degrees.
 When $1 - Y = 0.01$, 99% of the max temp change has occurred

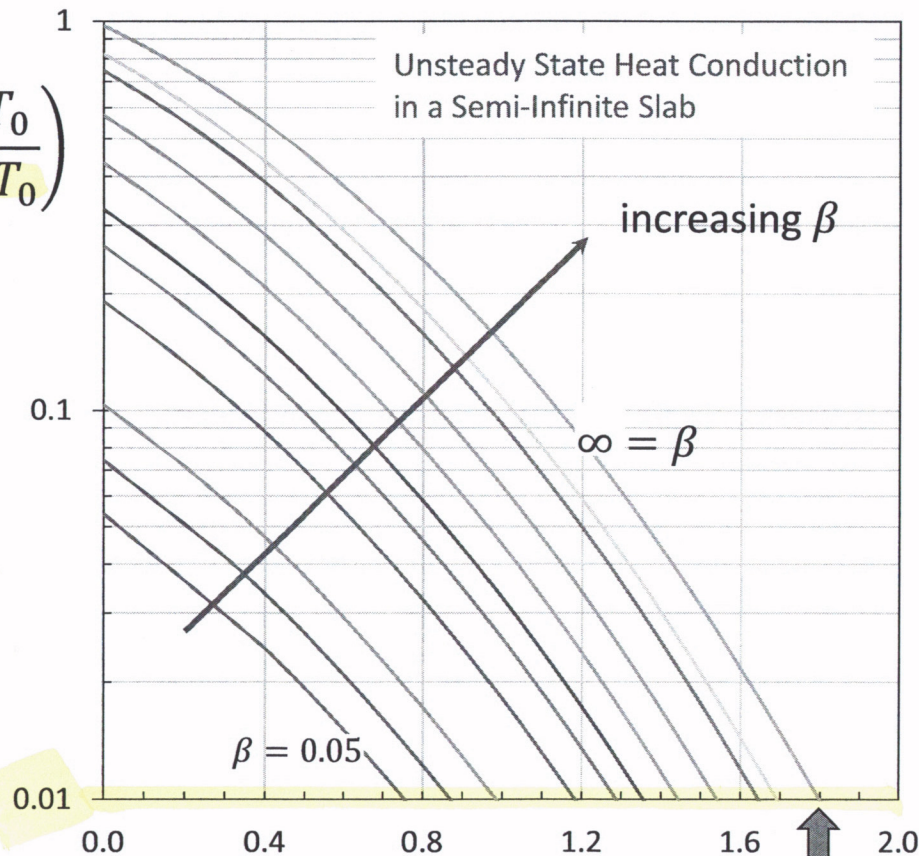
Note: We can use the semi-infinite slab solution for finite slabs, within limits



$$1 - Y = \left(\frac{T - T_0}{T_1 - T_0} \right)$$

$\zeta = \text{ZETA}$

For values of $\zeta(t, x)$ that predict $T \approx T_0$ or $(1 - Y) = 0.01$ at a distance equal to the half-slab thickness b , the semi-infinite slab solution is equivalent to the finite slab; this occurs $\forall \beta$ when $\zeta_{half-slab} = \frac{b}{2\sqrt{\alpha t}} > 1.8$



$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

— 20
 — 3
 — 2
 — 1
 — 0.6
 — 0.4
 — 0.3
 — 0.2
 — 0.1
 — 0.07
 — 0.05

$$\zeta = \frac{x}{2\sqrt{\alpha t}}$$

When $\zeta_b > 1.8$, no matter what h is, the temp at $x=b$ is still T_0

Try semi-infinite slab:

12

$$\sum x_i > 1.8 ?$$

$$\frac{x_i}{2\sqrt{\alpha t}} = \frac{(0.35 \text{ m})}{2\sqrt{3.8 \times 10^{-6} \frac{\text{m}^2}{\text{s}} \cdot 1800 \text{ s}}}$$

$$= 2.1 \checkmark$$

To calc $T(5 \text{ cm})$, $T(10 \text{ cm})$ \longrightarrow

(3)

$$\beta = \frac{h}{k} \sqrt{\alpha t} = 1.84 \sim 2$$

$$\zeta = \frac{x}{2\sqrt{\alpha t}}$$

5cm $\zeta = 0.3$ $T = -2.5^{\circ}\text{C}$
 10cm $\zeta = 0.6$ $T = -6^{\circ}\text{C}$

(read off graph
1-sig-fig)

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