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16 APRIL 2021 MODULE 4 F. MD RUISSON
CM3120



Michigan Tech

Requests for today?

2AP21

- ↘ . 4.3
- ↙ . 4.7
- . 4.8
- . 4.11
- .
- .

(see also Example 5
Module 4
Lecture II)

0.5

17. (WRF) Ammonia (NH_3) will be absorbed from an air mixture at $293K$ and $1.0 atm$ in a countercurrent packed tower, using water as the absorption solvent. The total inlet gas molar flow rate (air plus NH_3) is $5.03 \times 10^{-4} kmol/s$ and the ammonia composition in the inlet gas is 0.0352% mole fraction. Ammonia-free water (species B) at a mass flow rate of $L_S = 9.46 \times 10^{-3} kg/s$ will be used as the absorption solvent. If the ammonia concentration in the outlet gas is reduced to a mole fraction of 0.0129 , determine the ratio of the operating solvent molar flow rate to the minimum molar solvent flow rate. Equilibrium data for the NH_3 -water-air system at the tower's temperature and pressure are given by $Y_A = mX_A$, where $m = 0.82$ and Y_A is the molar ratio of ammonia to air in the gas and X_A is the molar ratio of ammonia to water in the liquid.

$$X_A = \frac{\text{moles A}}{\text{moles B}} = \frac{x_A}{(1-x_A)} \quad (\text{mixture of A and liquid B})$$

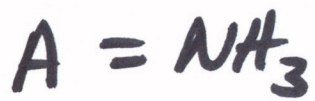
$$Y_A = \frac{\text{moles A}}{\text{moles I}} = \frac{x_A}{(1-x_A)} \quad (\text{mixture of A and gas I})$$

These problems are often carried out on a solute-free basis. See the notes for some help with this problem. Answer: ratio = 2.1

A good strategy is to change the provided information to be on a solute-free basis. The solute-free gas flow rate G_s is the (constant) molar flow rate of air. The solute-free liquid flow rate is the (constant) molar flow rate of water. Convert all the mole fractions to molar ratios, performing the appropriate balances to obtain missing values. The operating line is a balance cutting through the bottom streams and an arbitrary place within the column characterized by molar ratios of X_A, Y_A . The minimum liquid flow rate L_s (for the same gas flow rate G_s is determined as discussed in class.

16 April 2024 F. Morrison

rf WRF
PL67



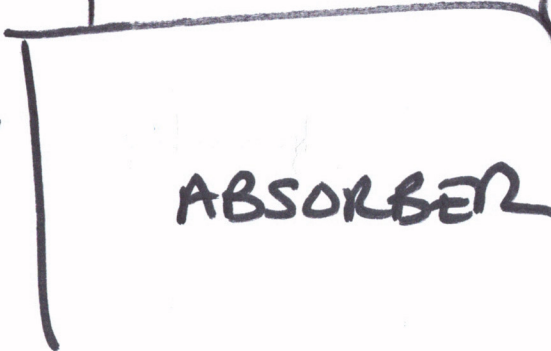
given

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$$\dot{M}_{\text{H}_2\text{O}} = 9.46 \times 10^{-3} \text{ kg/s}$$

\dot{G}_s NH_3 AIR

$$y_{A1} = 1.3069 \times 10^{-2}$$
$$4.8529 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$$



NH_3 $X_{A1} = 0$

Water $5.2556 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$

L_s

$$\dot{M}_{\text{gas}} = 5.03 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$$

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$$\dot{M}_{\text{tot}} = 5.3692 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$$

NH_3 $y_{A2} = 3.6484 \times 10^{-2}$

\dot{G}_s AIR $4.8529 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$

NH_3 $X_{A2} = 2.1622 \times 10^{-2}$

L_s = Water $5.2556 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$

NH_3 $1.1364 \times 10^{-5} \frac{\text{kmol}}{\text{s}}$

BOTTOM - GAS

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$$Y_{A_1} = \frac{\text{moles NH}_3}{\text{moles Air}} = \frac{Y_A}{1 - Y_A} \quad \frac{\text{moles NH}_3 / \cancel{\text{moles total}}}{\text{mole Air} / \cancel{\text{moles total}}}$$

$$Y_{A_2} = \frac{0.0352}{1 - 0.0352} = \boxed{3.6484 \times 10^{-2}}$$

$$\begin{aligned} \text{moles NH}_3 \text{ in GAS} &= Y_A \dot{M}_{\text{gas}} = \left(0.0352 \frac{\text{mole A}}{\text{mole total}} \right) \left(5.03 \times 10^4 \frac{\text{kmol}}{\text{s}} \right) \\ &= \boxed{1.7706 \times 10^5 \frac{\text{kmol}}{\text{s}}} \end{aligned}$$

NH₃ in GAS ENTERING

$$\begin{aligned} \text{moles AIR in} &= (1 - Y_A) \dot{M}_{\text{gas}} = \boxed{4.8529 \times 10^4 \frac{\text{kmol}}{\text{s}}} \\ &= \text{moles AIR out} \end{aligned}$$

AIR MOLAR FLOW RATE

"solve for" (in & out)

How much NH₃ exits in GAS stream?

TOP ("1")
GAS:

$$\xrightarrow{4.8529 \times 10^{-4} \frac{\text{kmol AIR}}{\text{s}}}$$

$$\frac{y_{A1} = 0.0129}{1 - y_{A1}}$$

$$= \left(y_{A1} = 1.3069 \times 10^{-2} \frac{\text{mol A}}{\text{mol AIR}} \right)$$

$$\frac{1 \text{ kmol A}}{\text{s}}$$

$$= (y_{A1}) \left(4.8529 \times 10^{-4} \frac{\text{kmol AIR}}{\text{s}} \right)$$

NH₃
out
in sec

$$= \left(6.3423 \times 10^{-6} \frac{\text{kmol}}{\text{s}} \right)$$

BOTTOM LIQUID ("2"):

3.1

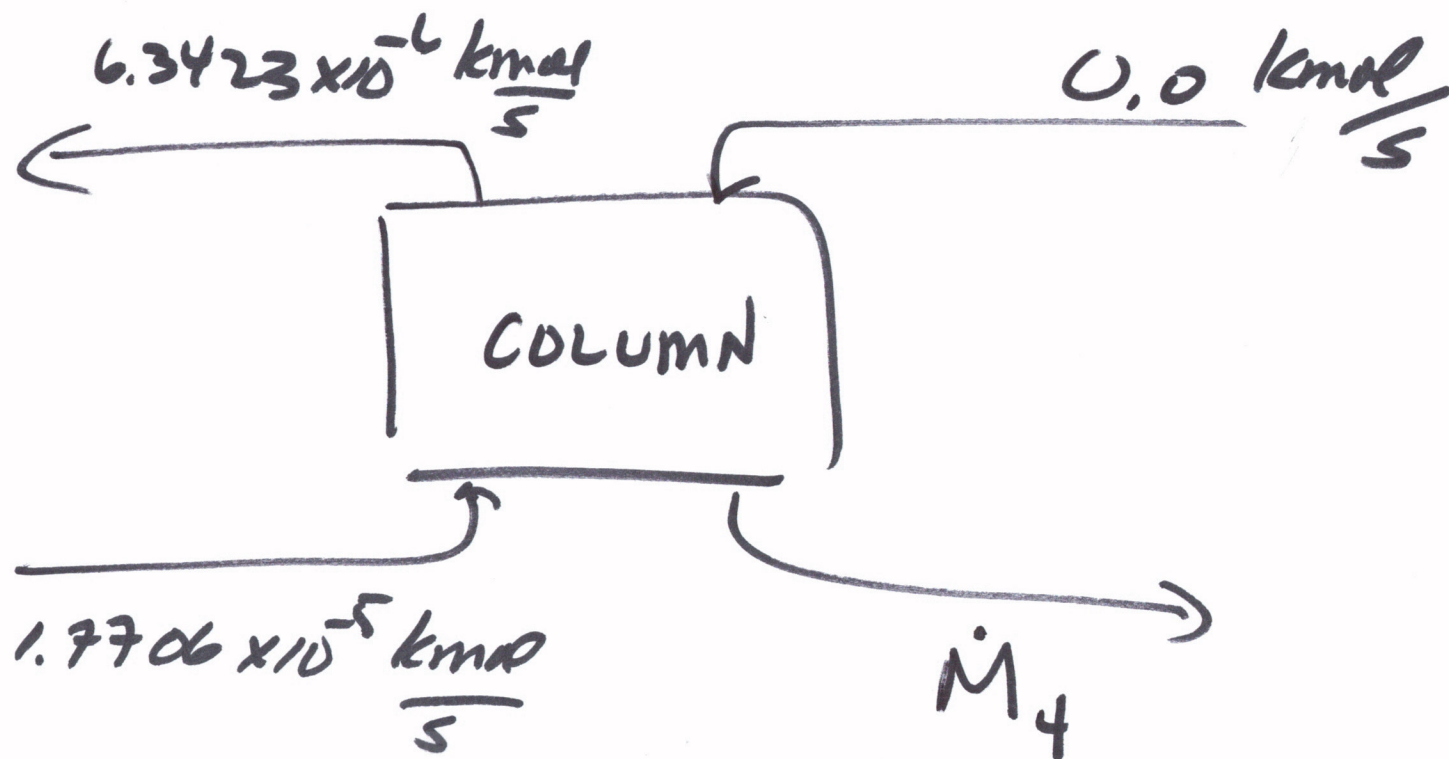
$$L_s = \frac{\text{mole water}}{\text{in}} = \left(9.46 \times 10^{-3} \frac{\text{kg}}{\text{s}} \right) \left(\frac{\text{kmol}}{18 \text{ kg}} \right)$$

$$L_s = 5.2556 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$$

WATER
"SOLUTE-FREE"
FLOW

4

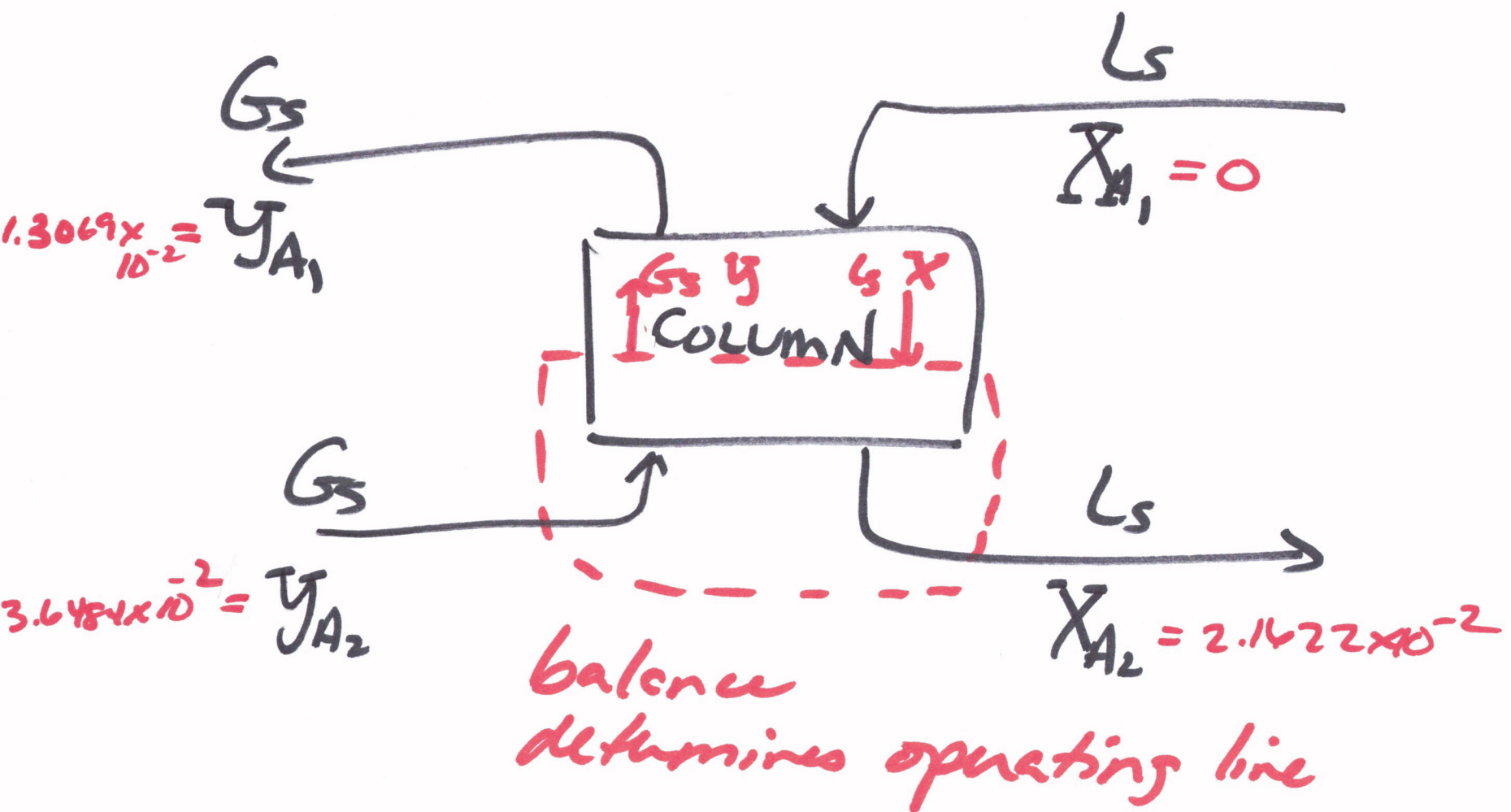
NH₃ BAL - OVERALL :



BOTTOM LIQ ("2"):

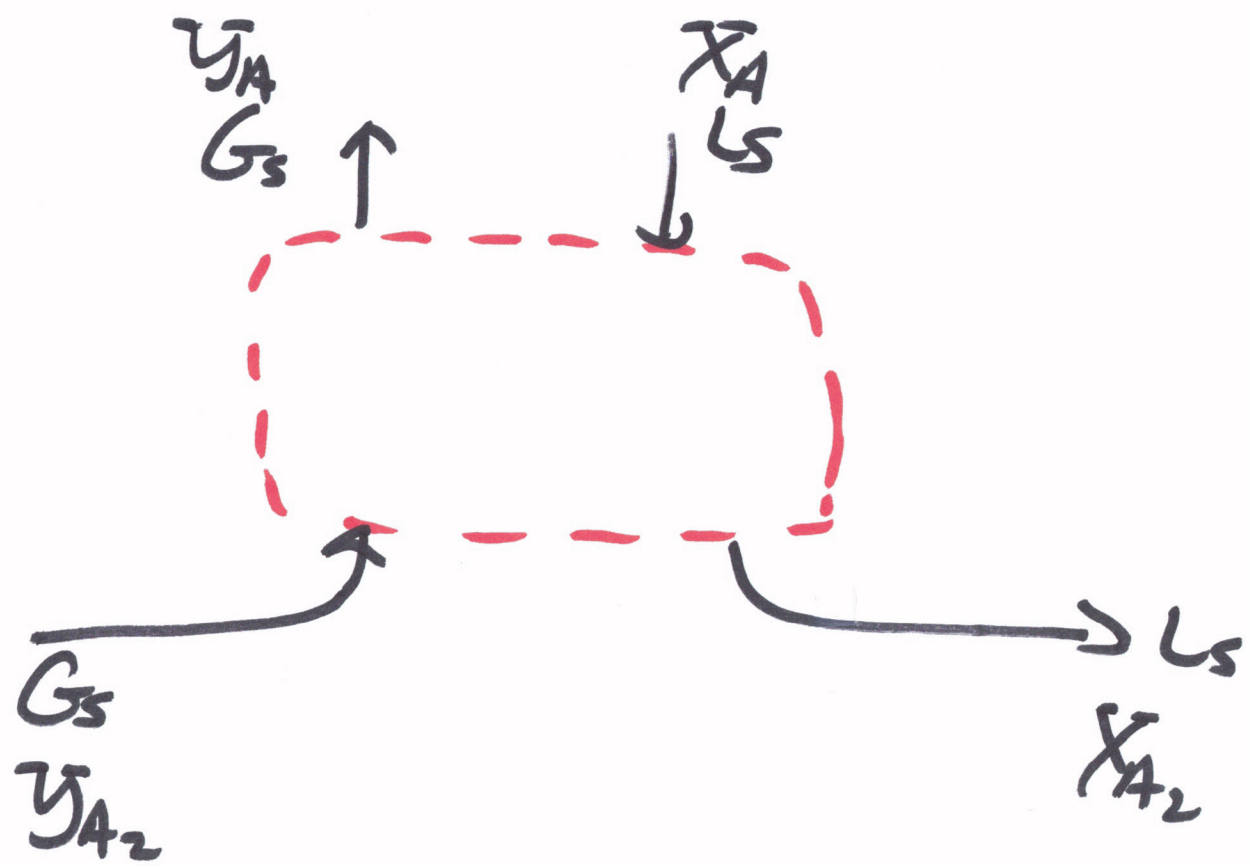
$$\dot{M}_4 = 1.1364 \times 10^{-5} \frac{\text{kmol NH}_3}{\text{s}}$$

$$X_{A_2} = \frac{\text{mols NH}_3}{\text{mols Water}} = \frac{1.1364 \times 10^{-5}}{5.2556 \times 10^{-4}} = \boxed{2.1622 \times 10^{-2}}$$



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Operating line - both phases, specific A:

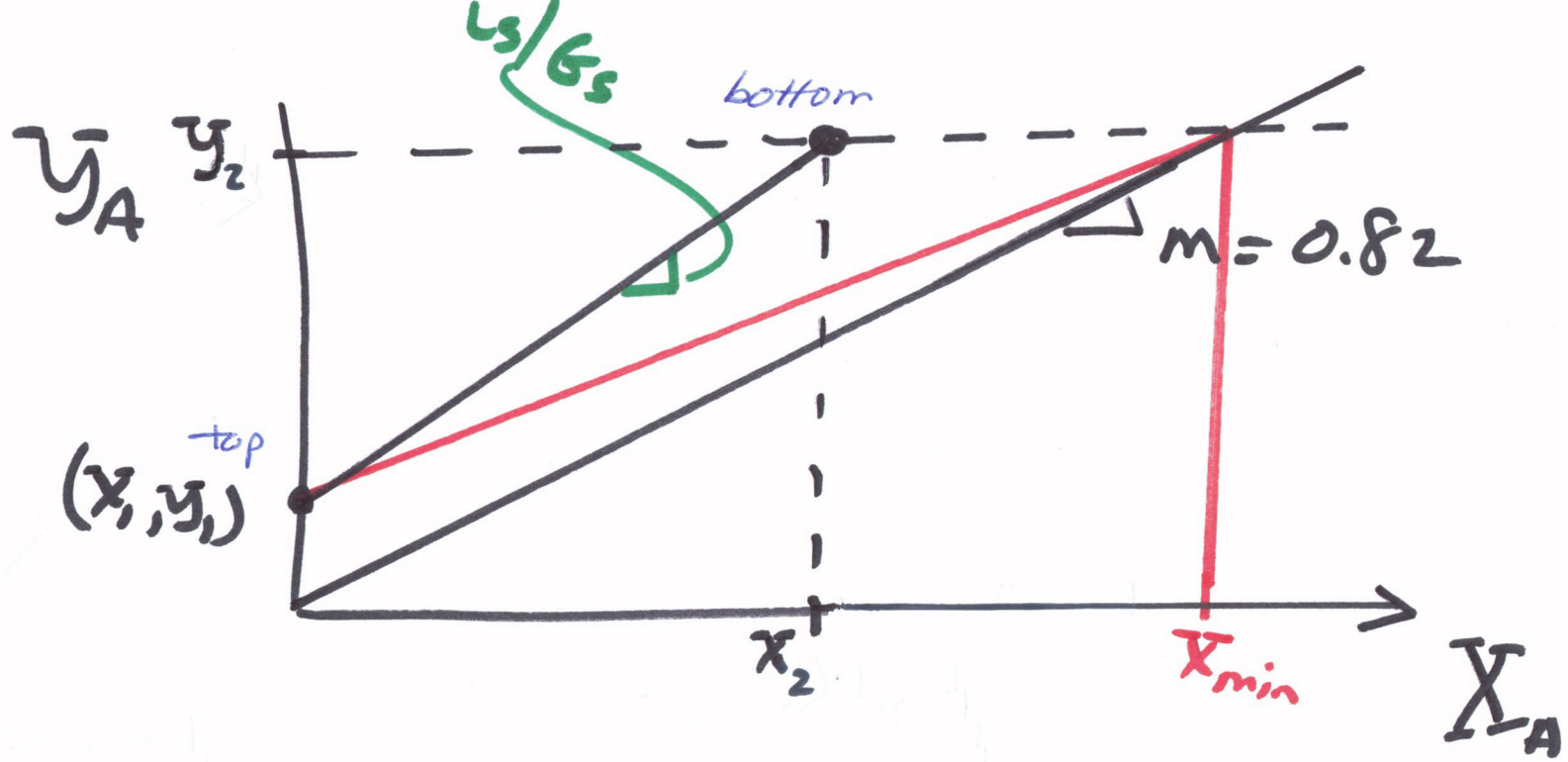


$$\cancel{G_s} Y_{A2} + \cancel{L_s} X_A = \cancel{G_s} Y_A + \cancel{L_s} X_{A2} \quad *$$

$$Y_A = \frac{L_s}{G_s} X_A + Y_{A2} - \frac{L_s}{G_s} X_{A2}$$

SLOPE = $\frac{L_s}{G_s}$

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$$m = 0.82$$
$$(X_{min})(slope) = y_2$$
$$X_{min} = \frac{y_2}{(slope)} = \frac{3.6484 \times 10^{-2}}{0.82} = 4.4493 \times 10^{-2}$$

X_{min}

(8)



$$\text{slope} = \frac{y_2 - y_1}{x_{min} - x_1} = \frac{L_{min}}{G_S}$$

$$L_{min} = \frac{(3.648 \times 10^{-2})(1.3069 \times 10^{-2})}{(4.4493 \times 10^{-2}) - 0} \left(4.8529 \times 10^{-4} \frac{\text{kmol}}{\text{s}} \right)$$

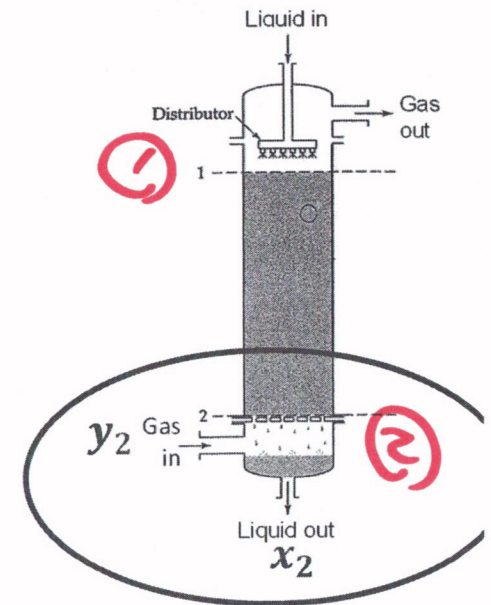
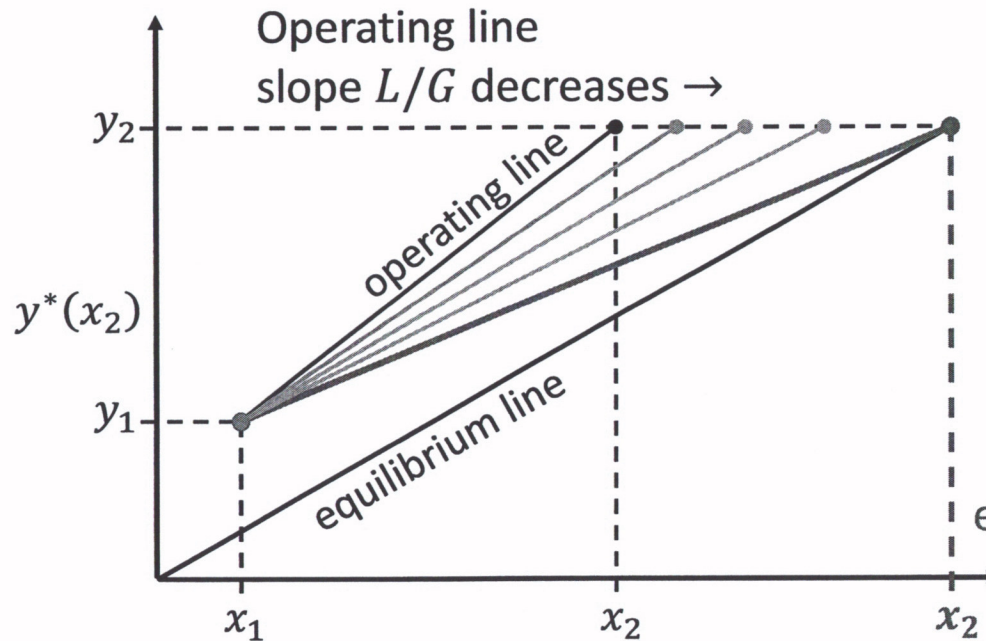
$$L_{min} = 2.55344 \times 10^{-4} \frac{\text{kmol}}{\text{s}}$$

$$G_S / L_{min} = 2.06 \sim \text{Twice the min} //$$



Mass Transfer in an Absorption Column:

- operating line slope = $\frac{L}{G}$
- equilibrium line slope = $H = m$



Minimum slope, minimum L/G ratio, results when exit liquid condition x_2 is in equilibrium with the entering gas condition y_2 (cannot go lower)