

Friday 9 Apr 2021

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①

Modeling practical devices involving mass transfer

Example 6: Height of a packed bed absorber

How can we use mass transfer to design a packed bed gas absorber to achieve a desired separation?

K_x can also be related to DAB (EXAMPLE 9)

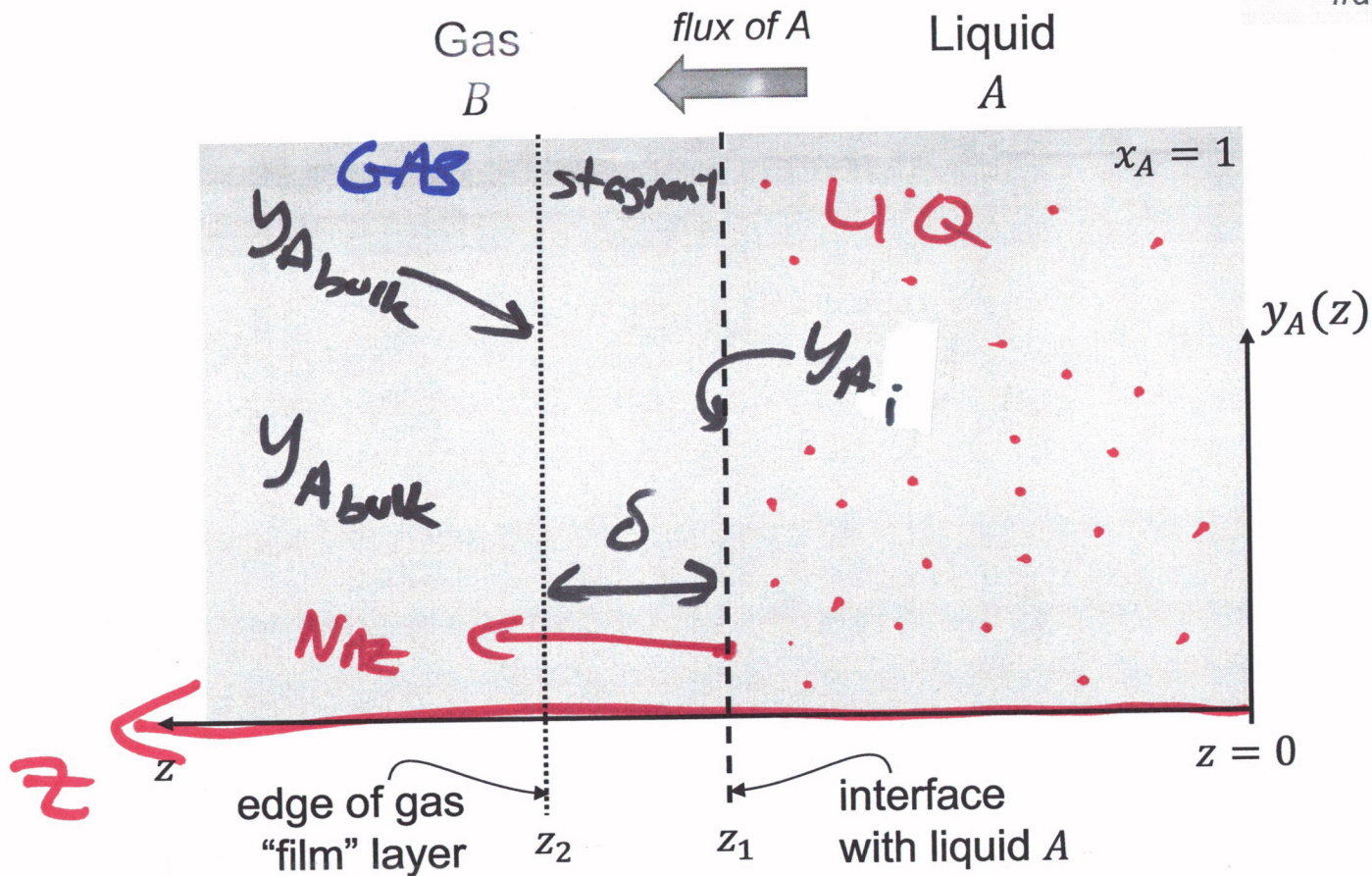
Example 6 is presented as a series of **linked examples** that navigate around apparent “dead ends” in modeling mass-transfer units

★ REVISIT MOD 4 LECT IV

Identify a question	Invent something	Try to use it
<ol style="list-style-type: none">1. How can we model a large, practical device dependent on mass transfer?2. How can we account for A going between phases?3. How can we improve LDF model to cross the boundary (bulk-to-bulk transfer)?4. Can we model a large, practical device, incorporating K_L, K_G to account for mass xfer between phases?	<ol style="list-style-type: none">1. Apply the species A mass balance to a macroscopic C.V.2. Invent k_x through linear driving force (LDF) model3. Write LDF in both phases and combine to create overall effect of multiple resistances4. Yes	<ol style="list-style-type: none">1. Lack a system to account for A going between phases2. Gets A <u>to</u> the boundary, but not <u>across</u>3. Working, but can we devise a convenient shorthand?

Example 9: The film model of 1D steady diffusion yields a composition distribution and an expression for the flux. What is the mass-transfer coefficient in the film model?

(we use x for liquid and y for gas mole fractions)



RECALL:

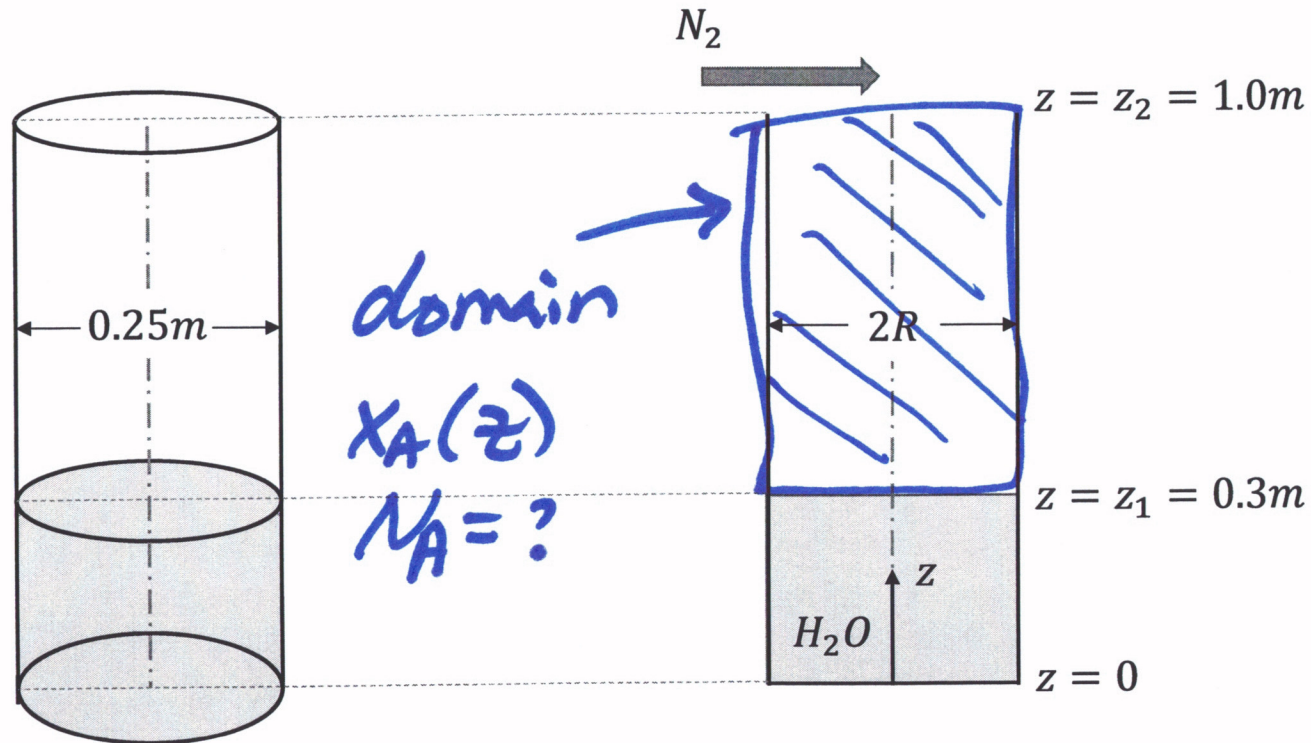
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1D Evaporation from tank

QUICK START

Example 1: Water (40°C , 1.0 atm) slowly and steadily evaporates into nitrogen (40°C , 1.0 atm) from the bottom of a cylindrical tank as shown in the figure below. A stream of dry nitrogen flows slowly past the open tank. The mole fraction of water in the gas at the top opening of the tank is 0.02. The geometry is as shown in the figure. **What is the rate of water evaporation?**

origin
of
"film
model"



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Film model (see Ex 1, Lec II, Mod 3)

$$N_{Az} = \frac{c D_{AB}}{\delta} \ln \left(\frac{1 - y_{A,b}}{1 - y_{A,i}} \right)$$

We could not get this from shells.

LINEAR DRIVING FORCE MODEL
(GAS)

$$N_{Az} = k_y (y_{A,i} - y_{A,b})$$

- Equate.

ANSWER

(remember $y_A + y_B = 1$)

- obtain: $k_y = \left(\frac{c D_{AB}}{\delta y_{B,im}} \right)$

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There are numerous concentration units in use (practical consideration)

Linear-driving-force model (film coefficients): the flux of A from the bulk in the gas is proportional to the difference between the bulk composition and the composition at the interface.

The defining equations for the film mass-transfer coefficients:

Table 29.1 Individual mass-transfer coefficients

GAS

Gas film		
Driving force	Flux equation	Units of k
Partial pressure (p_A)	$N_A = k_G(p_A - p_{A,i})$	$\text{kgmole}/\text{m}^2 \cdot \text{s} \cdot \text{atm}$
Concentration (c_A)	$N_A = k_c(c_{AG} - c_{AG,i})$	$\text{kgmole}/(\text{m}^2 \cdot \text{s} \cdot (\text{kgmole}/\text{m}^3))$ or m/s
Mole fraction (y_A)	$N_A = k_y(y_A - y_{A,i})$	$\text{kgmole}/\text{m}^2 \cdot \text{s}$
Liquid film		
Concentration (c_{AL})	$N_A = k_L(c_{AL,i} - c_{AL})$	$\text{kgmole}/(\text{m}^2 \cdot \text{s} \cdot (\text{kgmole}/\text{m}^3))$ or m/s
Mole fraction (x_A)	$N_A = k_x(x_{A,i} - x_A)$	$\text{kgmole}/\text{m}^2 \cdot \text{s}$

mole frac
y_A



And repeat for Example 10



Bulk convection present—Linear-driving-force model

Example 10: The penetration model of 1D steady diffusion yields a composition distribution and an expression for the flux. What is the mass-transfer coefficient in the penetration model?

(we use x for liquid and y for gas mole fractions)

