






Topics for Today:

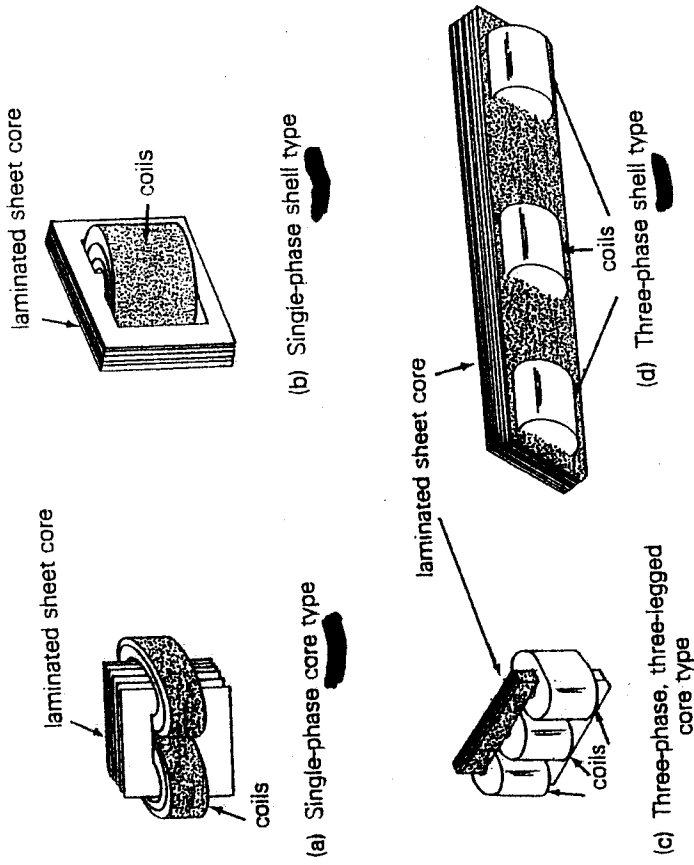
- Announcements
 - Everyone have a book now? Confirm. 
 - Software: Matlab? Will begin using as early as next week.
 - Room B45 is open from 9am onward.
 - Office hrs: 1:30-2:30pm, Mon, Wed, Fri
 - Office: EERC 623. Phone: 906.487.2857
 - Ch.1 Solutions posted on web page, with corrections. 
 - Exercises posted on web page, check e-mail for details. 
- Comments on Chapter 1 / Review: ✓
 - Sequence networks - correction to last Thursday's notes.
- Chapter 2 - Transformers and circuits w/transformers
 - Single phase transformers
 - Basic structure: winding R and Leakage, Core losses and saturation
 - 3-phase transformer banks and phase shifts

- IEE:  

- IEC: Dyn1

Figure 4.15

Transformer core configurations



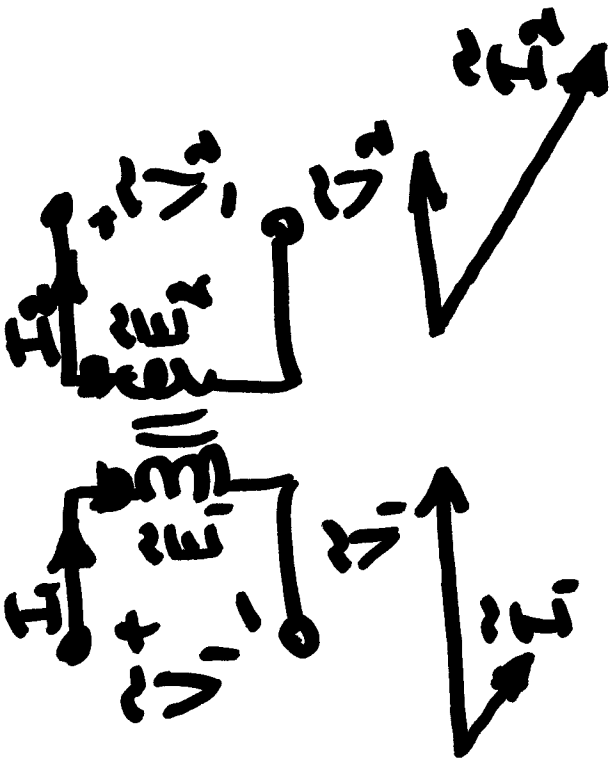
compared to replacement of only one phase of a three-phase bank. In either case, the equivalent circuits developed here and subsequent analyses are the same.*

SECTION 4.5

PER-UNIT SEQUENCE MODELS OF THREE-PHASE TWO-WINDING TRANSFORMERS

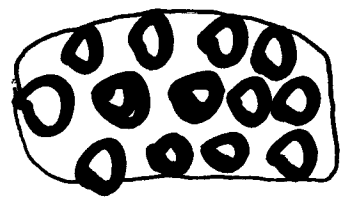
Figure 4.16(a) is a schematic representation of an ideal Y-Y transformer grounded through neutral impedances Z_N and Z_n . Figure 4.16(b-d) show the per-unit sequence networks of this ideal transformer. Throughout the remainder of this text per-unit quantities will be used unless otherwise indicated. Also, the subscript "p.u.," used to indicate a per-unit quantity, will be omitted in most cases.

By convention, we adopt the following two rules for selecting base



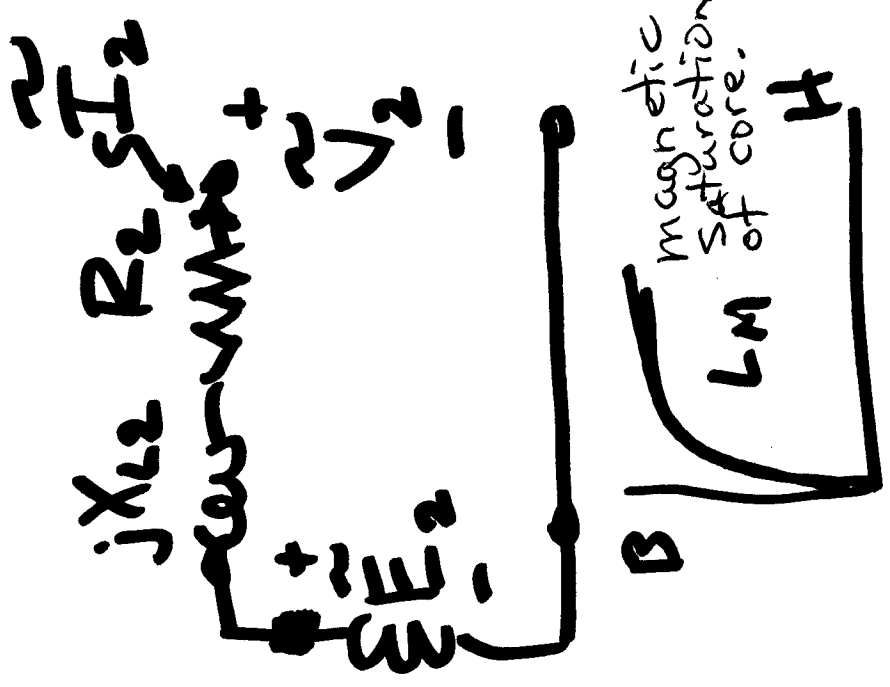
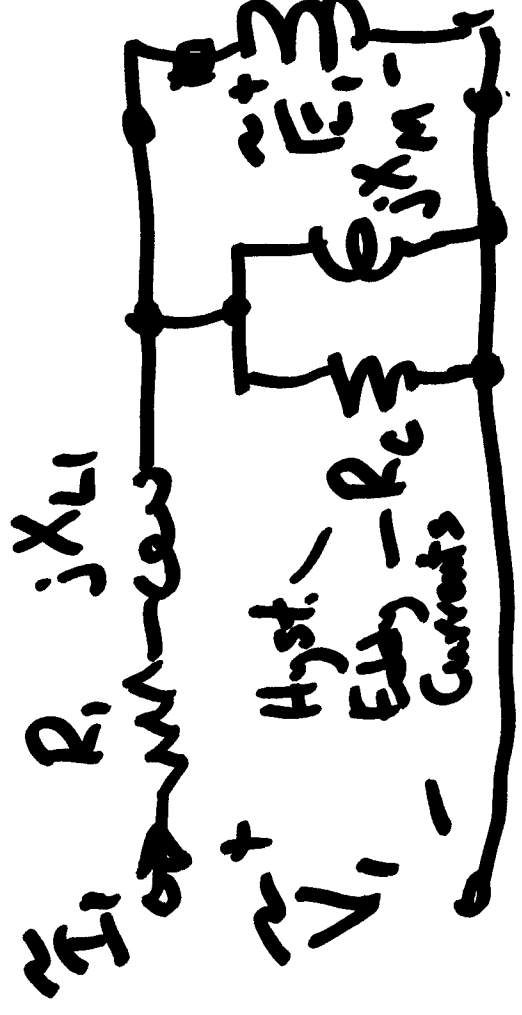
R_1, R_2
Windings

R as $f \uparrow$
- skin effect
- proximity effect.



Transformer coil cross-section

"Non-Ideal" Transformer



Magnetic Saturation of core.
LM

see fig 3.1

Faraday's Law:

$$e_i = N \cdot \frac{d\phi}{dt}$$

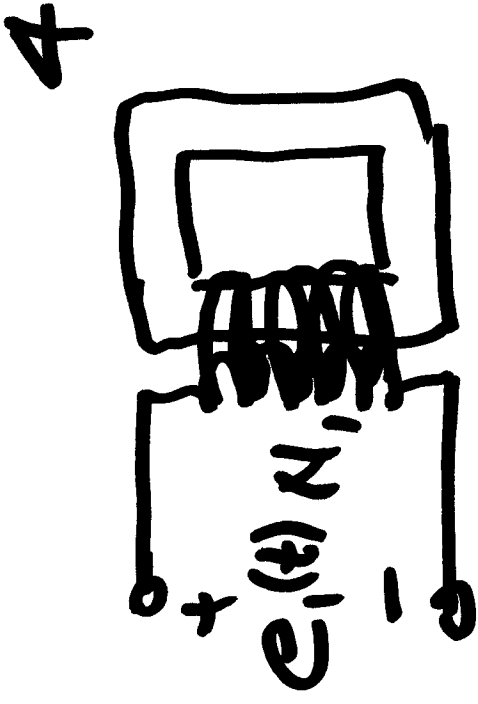
Problem: Faraday's Law

does not handle
polarity of induced
voltage.

\Rightarrow Lenz's Law Does

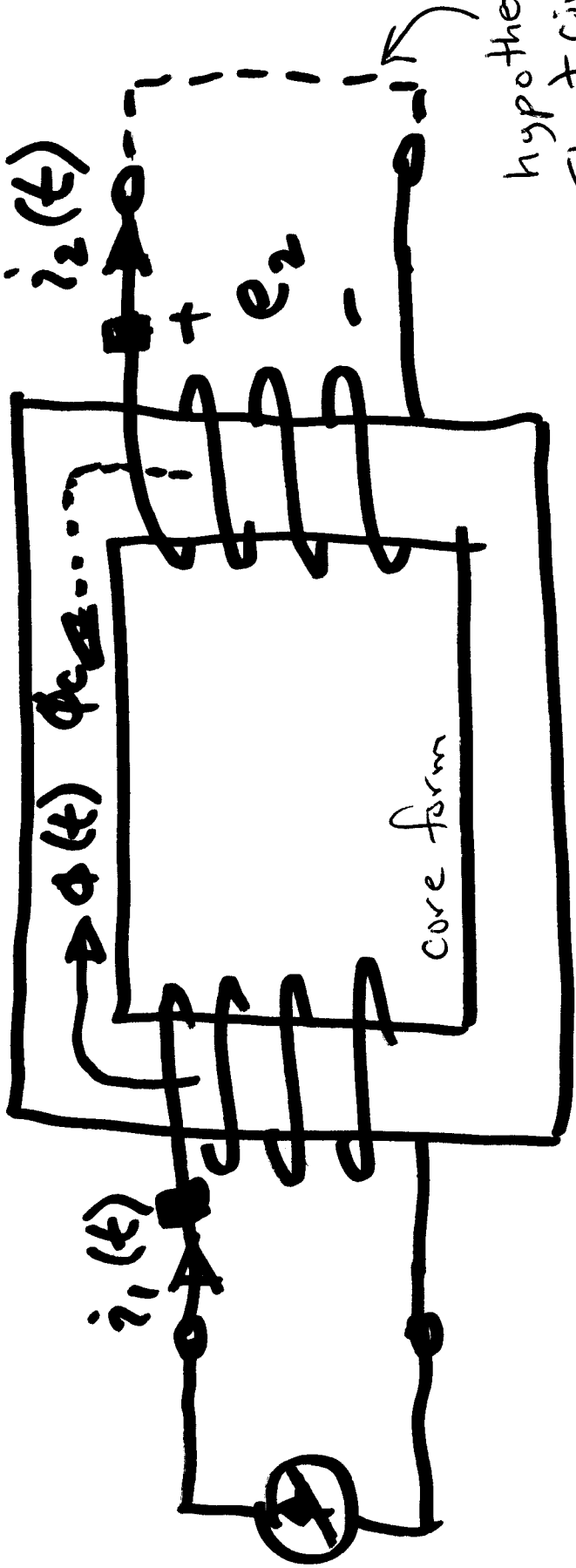
$$e = N \frac{d\phi}{dt} = \frac{d\lambda}{dt}$$

(polarity
explanation
on pages 5-6)

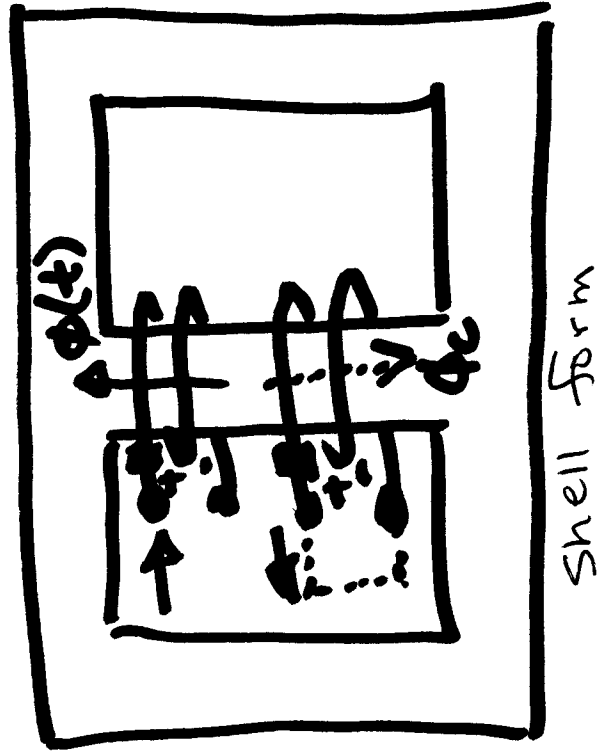


$\lambda = \text{flux linked}$
 $= N\phi$

5



hypothetical
short circuit.

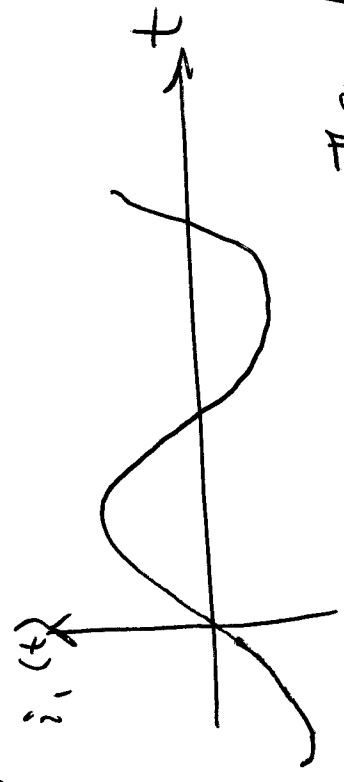


(refer to page 5)

Lenz's Law

The voltage induced has a polarity such that the resulting current flowing through a hypothetical short circuit would produce a counter flux Φ_c that opposes the change in flux $\frac{d\Phi}{dt}$ that induced the voltage in the first place.

One simple way to apply this, as shown on page 5, is to consider an injected current, $i_1(t)$, which could be a sinusoid, which is increasing with time:

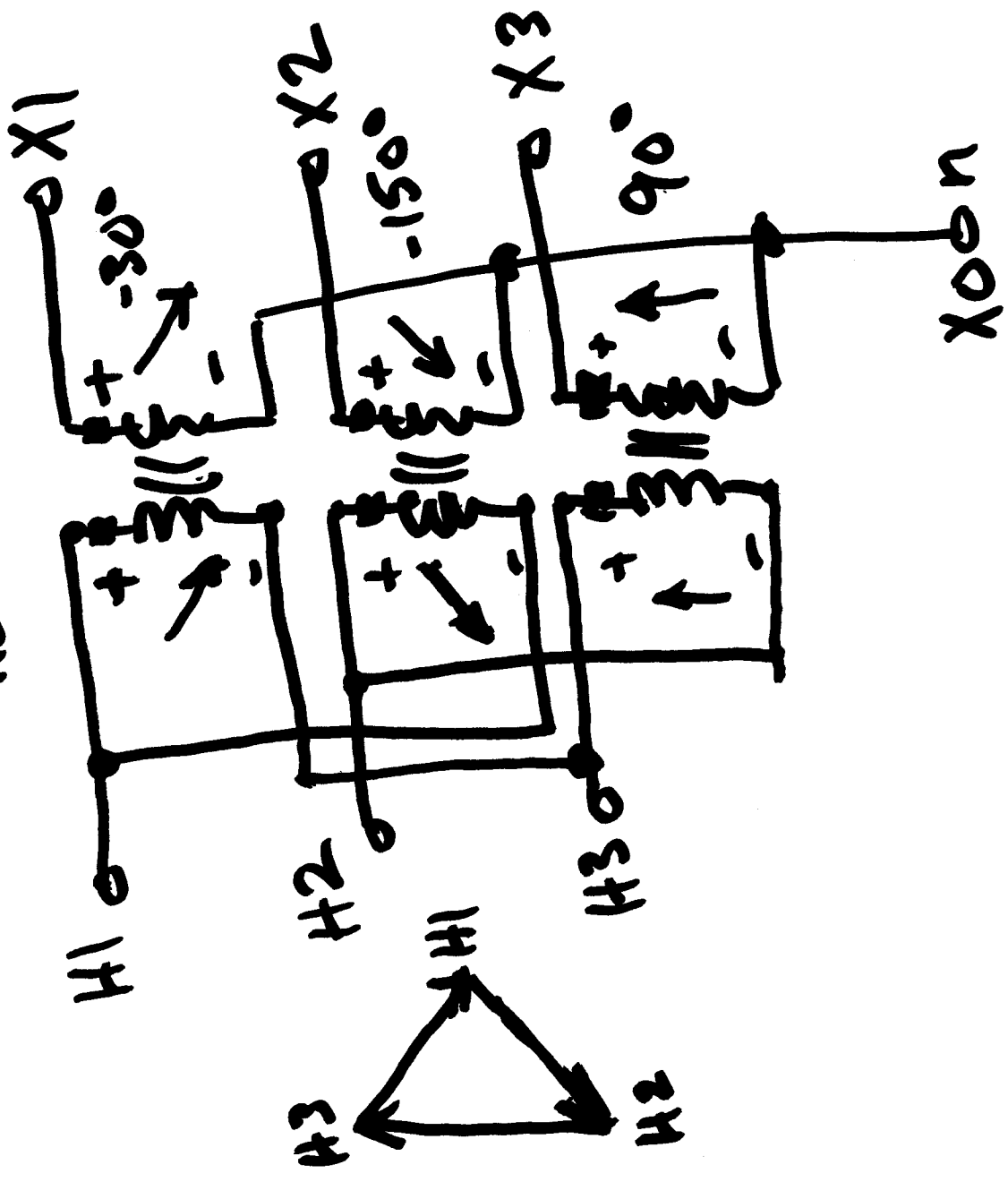


interval of interest

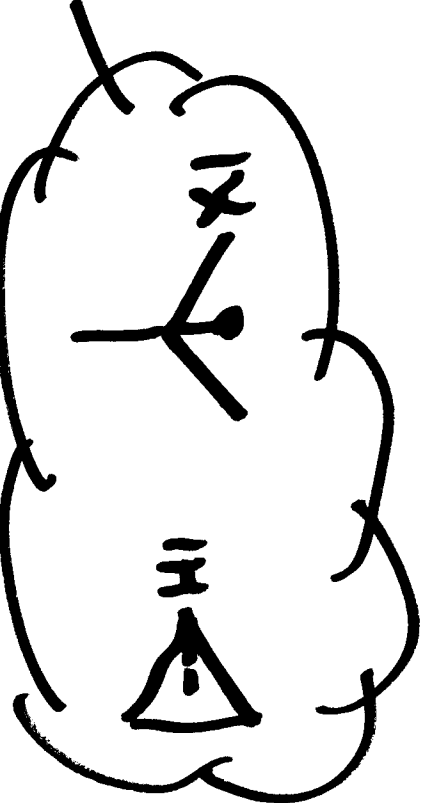
Then, based on required counter flux, we can find polarity of E_2 and direction of i_2 during that same interval, and properly define polarity marks

3-PHASE XFMR BANKS

Ex: Δ -Y (Dyn1)

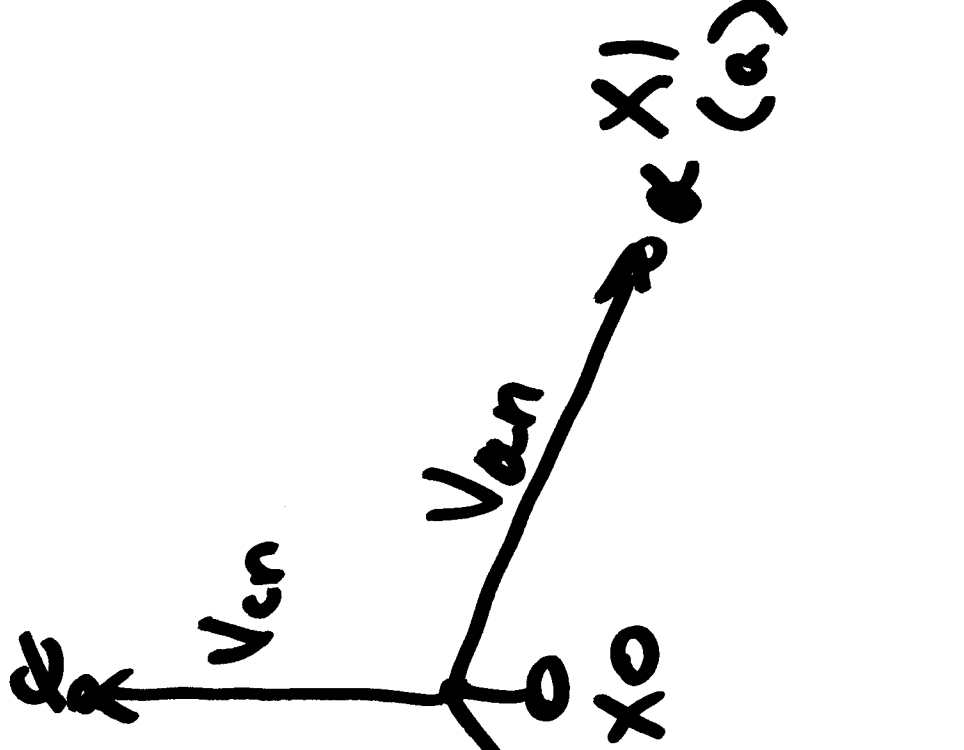


"ANSI"
or IEEE
STDS

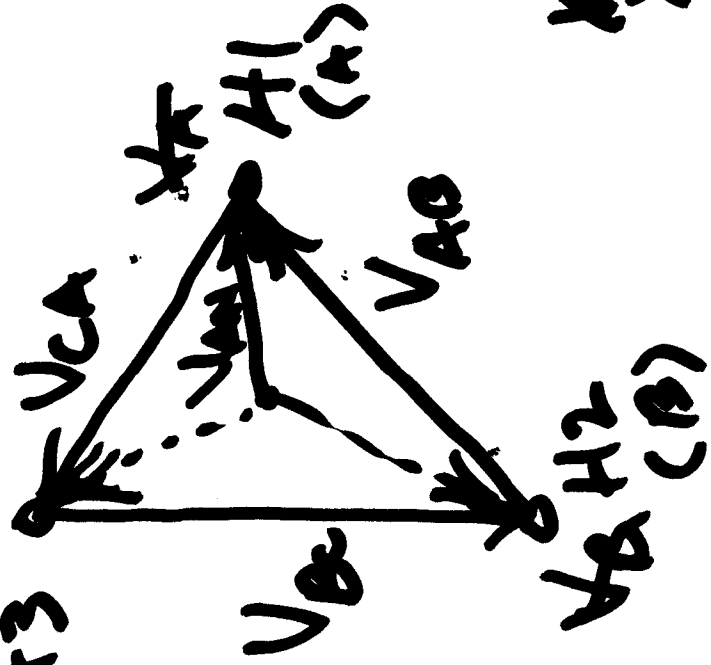


POS SEQ
PHASE SHIFT
7a

X3 (c)



(c) H3



(a)

(b) H2

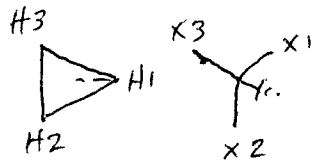
(c)

- Three-Phase Transformers

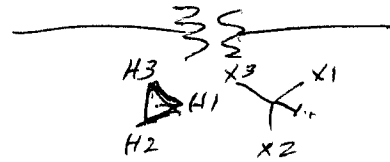
Mork

All of these can and are used to indicate the same winding connections:

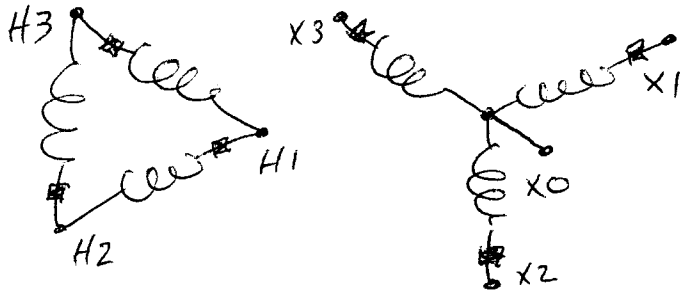
IEEE Stds:



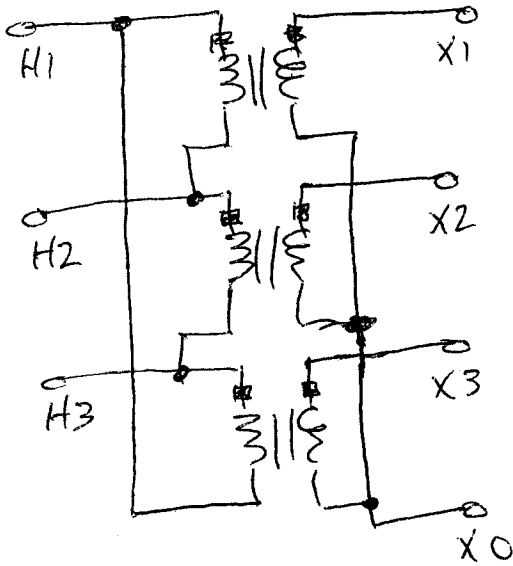
One-Line:



schematic



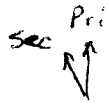
circuit 3-line diagram



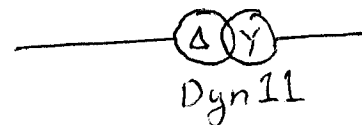
In Europe and much of the world:

IEC Stds:

Dyn11



One-Line:



'old-down' diagram

