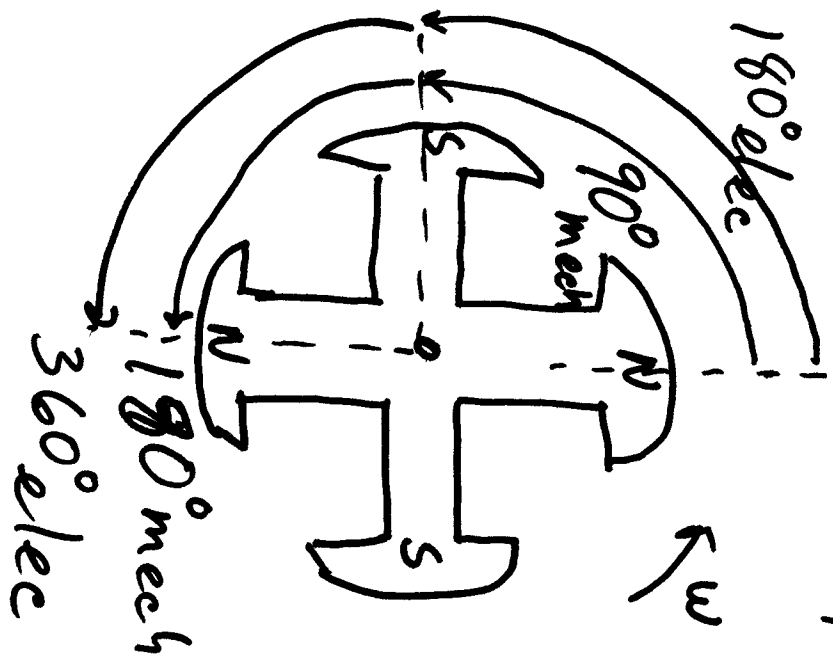


rotates at constant speed

$$N_{rpm} = \frac{120f}{\#P}$$



1 rotation of 360°

2 N poles

2 S poles

2 + peaks of V

2 - peaks of V

$$\Theta_{elec} = \frac{\#P}{2} \Theta_{mech}$$

of pole pairs

2 pole : fossil thermal plants

3600 rpm (60 Hz)

4 pole : nuclear thermal plants

1800 rpm (60 Hz)

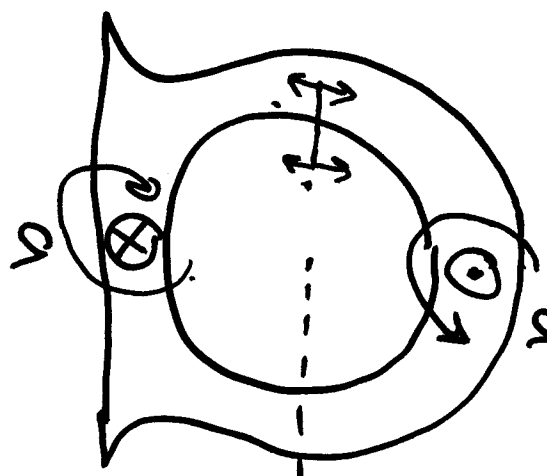
round rotor

less rotational losses

multi pole hydro plants

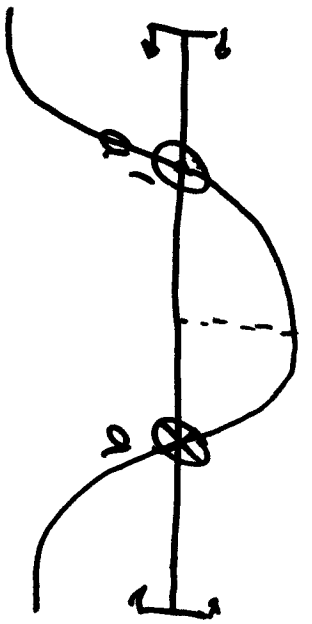
Space Vector a_1

or a axis

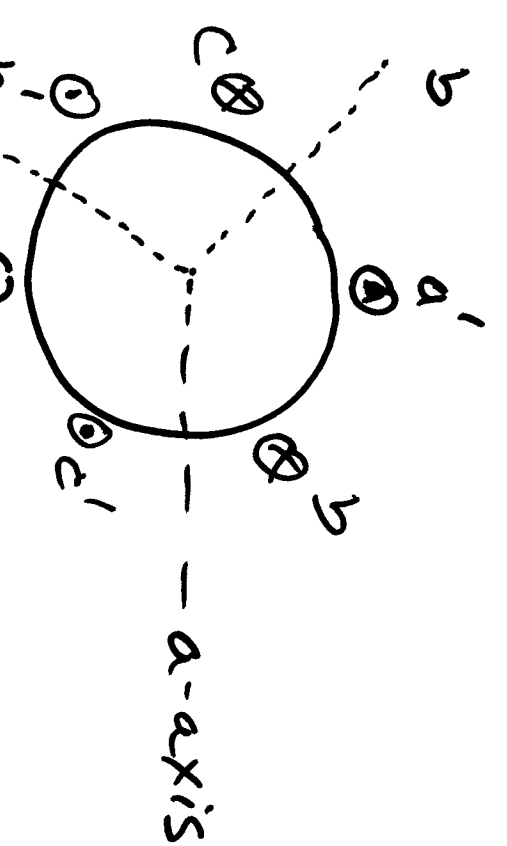


a -axis axis of the flux

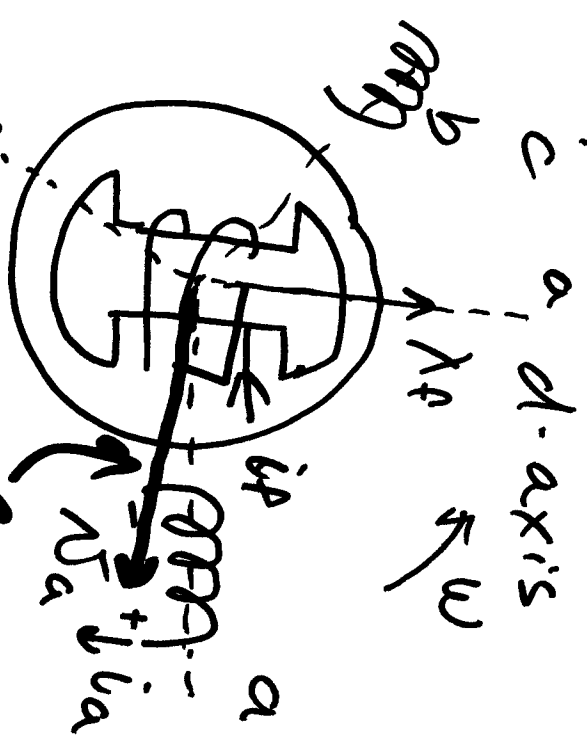
a - a' representation of a distributed winding



Sinusoidal flux distribution in space Peaks @ a -axis



field winding
magnetic field on
rotor



direct axis (d)
axis of positive
field flux
quadrature axis (q)
90° behind the
d axis

danger windings
One or more in d axis
One or more in q axis

g axis
c/w

~~Flux~~ $\rightarrow a$
 $N_a \psi_{ia}$

$$N_a = -\frac{d}{dt} \lambda_a - R_a i_a$$

$$N_b = -\frac{d}{dt} \lambda_b - R_b i_b$$

$$N_c = -\frac{d}{dt} \lambda_c - R_c i_c$$

Armature

$$\lambda_a = L_{aa} i_a + L_{ab} i_b + L_{ac} i_c + L_{af} i_f$$

$$\lambda_b = L_{ab} i_a + L_{bb} i_b + L_{bc} i_c + L_{bf} i_f$$

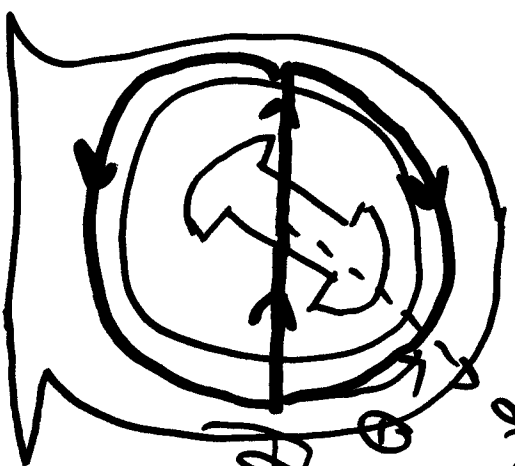
$$\lambda_c = L_{ac} i_a + L_{bc} i_b + L_{cc} i_c + L_{cf} i_f$$

Field

$$\lambda_f = L_{af} i_a + L_{bf} i_b + L_{cf} i_c + L_{ff} i_f$$

$$L_{xy} = N_x N_y \frac{\mu_0 \mu_r A}{l} \leftarrow \text{Cross Sectional area}$$

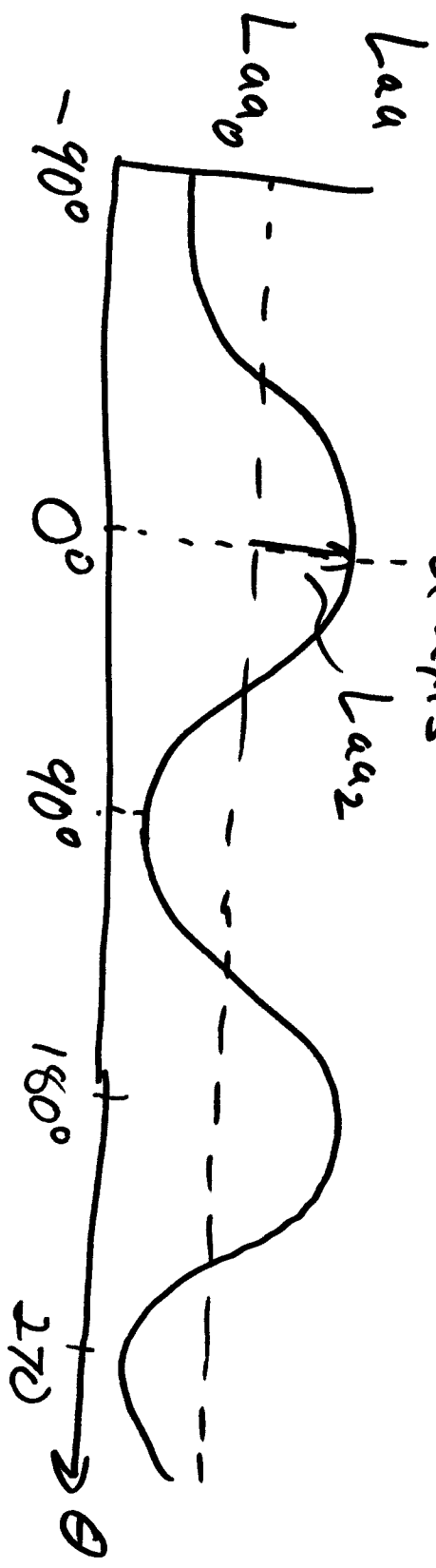
l ← length of magnetic circuit



$$\theta \gg 0^\circ$$

$$L_{a1} = L_{a0} + L_{a2} \cos(2\theta)$$

axis



$$L_{aa} = L_{a_0} + L_{a_2} \cos(2\theta) = L_s$$

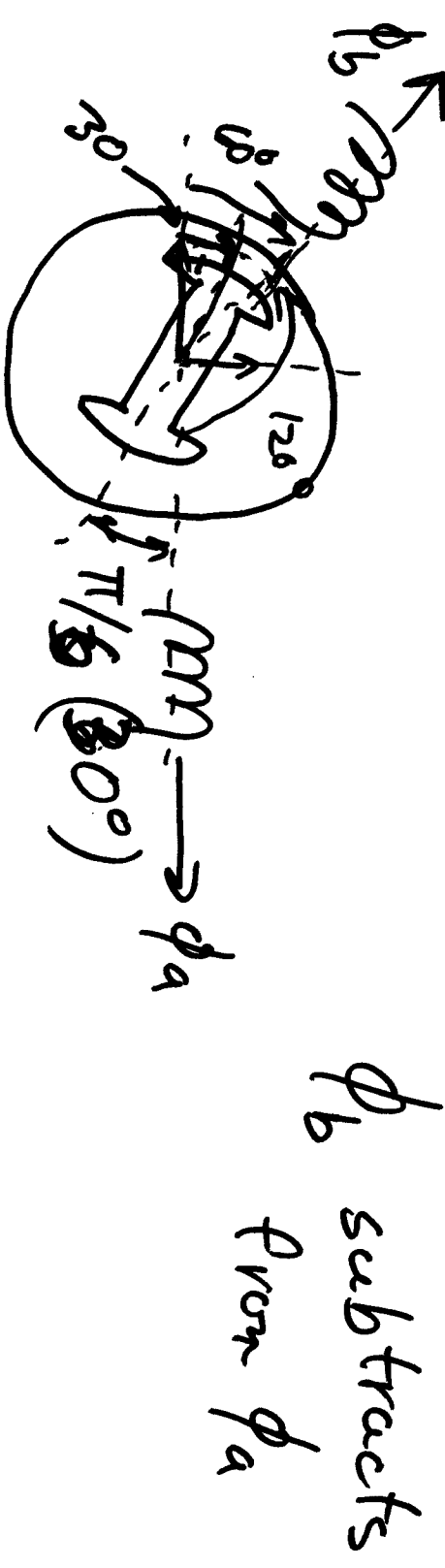
$$L_{bb} = L_{b_0} + L_{b_2} \cos\left(2\theta - \frac{2\pi}{3}\right) = L_s$$

$$L_{cc} = L_{c_0} + L_{c_2} \cos\left(2\theta + \frac{2\pi}{3}\right) = L_s$$

$$L_{a_0} = L_{b_0} = L_{c_0}$$

$$L_{a_2} = L_{b_2} = L_{c_2}$$

Stator mutual inductances



$$L_{ab} = -L_{ab0} - L_{ab2} \cos\left(2\theta + \frac{\pi}{3}\right) \quad \text{text} \quad L11-8$$

peak @ $-\frac{\pi}{6}$ or $\frac{5\pi}{6}$

$$= L_{ba}$$

$$L_{bc} = L_{cb} = -L_{ab0} - L_{ab2} \cos\left(2\theta - \pi\right) \quad -M_s$$

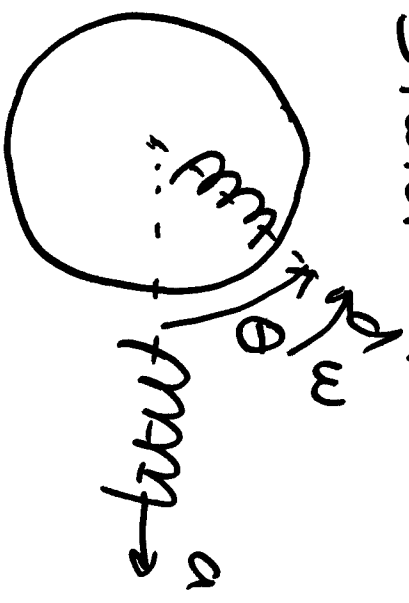
$$L_{ca} = L_{ac} = -L_{ab0} - L_{ab2} \cos\left(2\theta - \frac{\pi}{3}\right) \quad -M_s$$

Stator-rotor mutual inductance

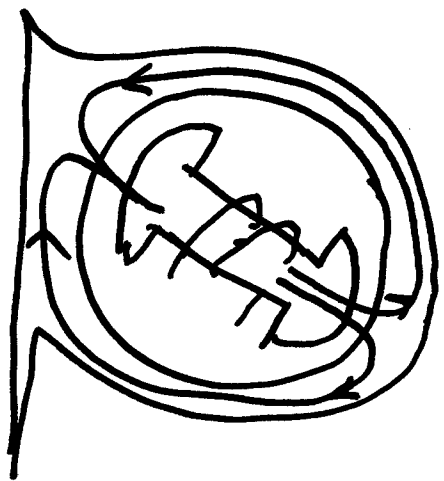
$$L_{af} = L_{af} \cos \theta \quad \text{text} \quad M_f$$

$$L_{bf} = L_{af} \cos\left(\theta - \frac{2\pi}{3}\right) \quad M_f$$

$$L_{cf} = L_{af} \cos\left(\theta + \frac{2\pi}{3}\right) \quad M_f$$



Rotor self inductance



$L_{FA} = \text{constant}$

Field winding always sees
the same magnetic circuit.

In saltpoles

- change value depending on rotor position
- change dramatically for salient pole machine, less so for a round rotor machine

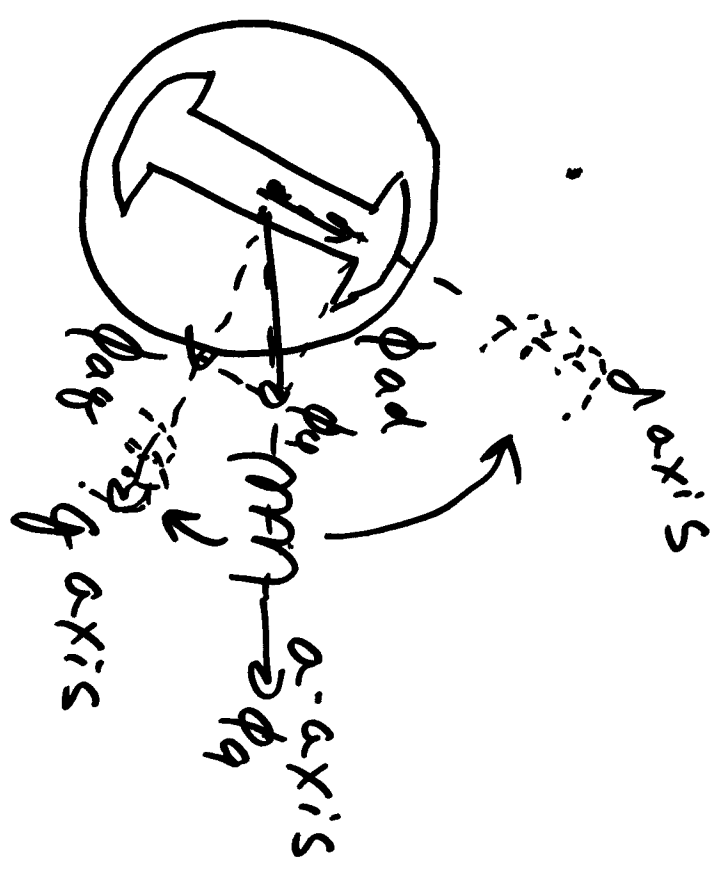
$$\begin{bmatrix} \dot{V}_a \\ \dot{V}_b \\ \dot{V}_c \\ \dot{V}_F \end{bmatrix} = - \frac{d}{dt} \left\{ \begin{array}{c|c|c|c} L_{aa}(\theta) & L_{ab}(\theta) & L_{ac}(\theta) & -L_{af}(\theta) \\ L_{ba}(\theta) & L_{bb}(\theta) & L_{bc}(\theta) & -L_{bf}(\theta) \\ L_{ca}(\theta) & L_{cb}(\theta) & L_{cc}(\theta) & -L_{cf}(\theta) \\ -L_{af}(\theta) & -L_{bf}(\theta) & -L_{cf}(\theta) & -L_{ff}(\theta) \end{array} \right\} \begin{bmatrix} i_a \\ i_b \\ i_c \\ i_f \end{bmatrix}$$

$$- \begin{bmatrix} R_a & 0 & 0 & 0 \\ 0 & R_b & 0 & 0 \\ 0 & 0 & R_c & 0 \\ 0 & 0 & 0 & -R_f \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \\ i_f \end{bmatrix}$$

Upper left
 $L_{SS}(\theta)$
 Upper right
 $L_{SR}(\theta)$

$$N_{dgo} = T N_{abc}$$

$$i_{dgo} = T i_{abc}$$



Transformation matrix is dependent
on rotor position

$$N_{abc} = -P [L_{ss}(\theta)] i_{abc} - P \{ [L_{sr}(\theta)] i_A \} - R_{abc} i_{abc}$$

P : derivative operator