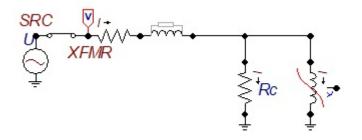
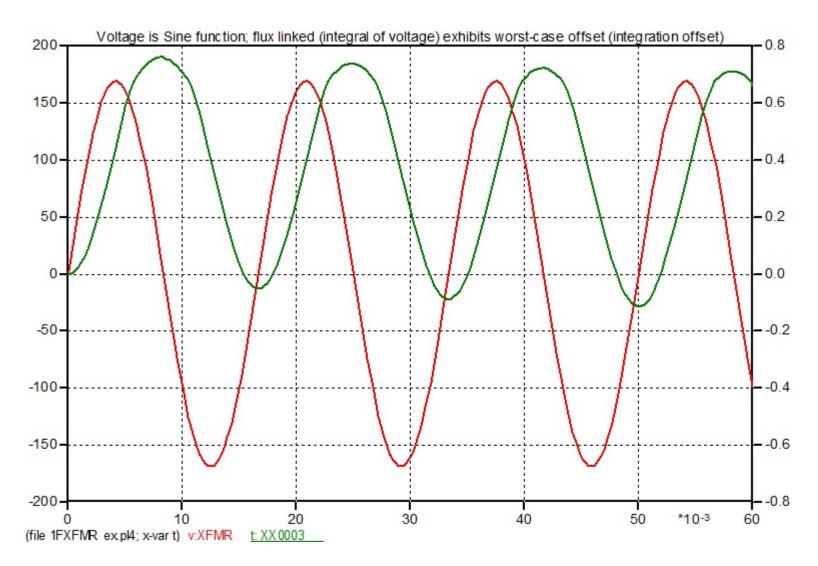
Topics for Today:

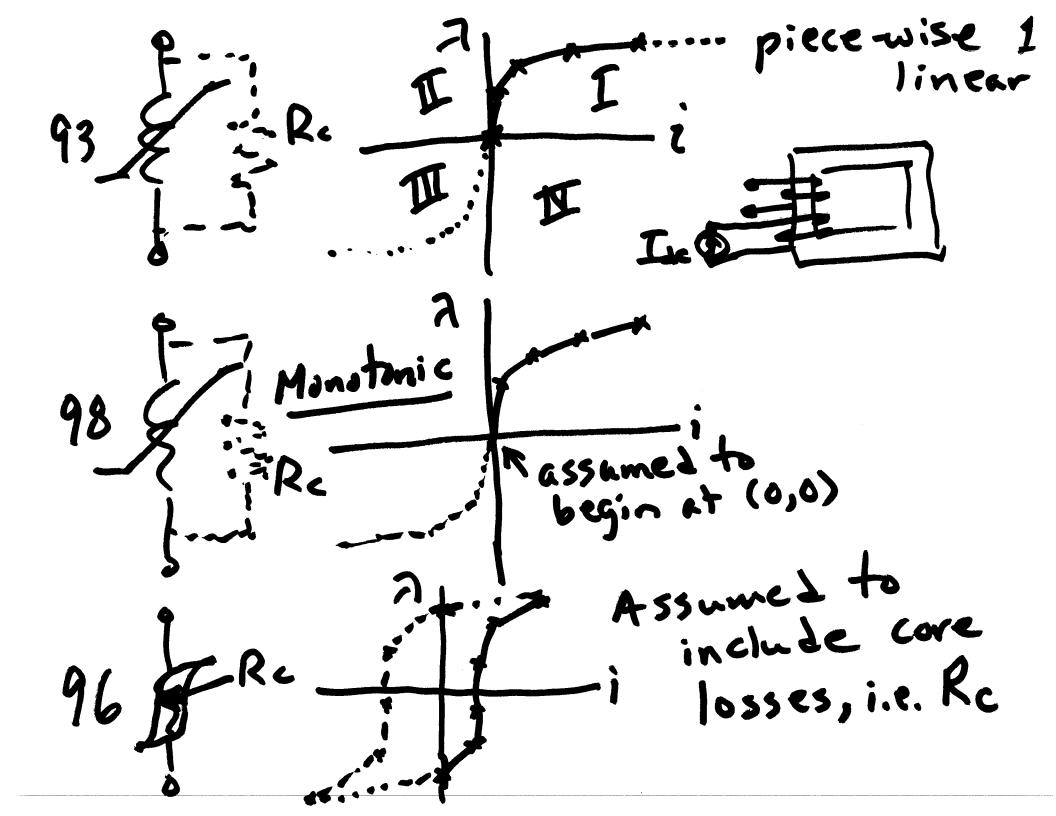
- Course Info:
 - Web page: https://pages.mtu.edu/~bamork/ee5220/
 - Book, references, syllabus, more are on web page.
 - Software Matlab. ATP/EMTP [License <u>www.emtp.org</u>] ATP tutorials posted on our course web page
 - <u>EE5220-L@mtu.edu</u> (participation = min half letter grade)
- HW#8 Probs. 9.6, 9.12 now due.
- HW#9 Probs. 9.2, 9.3, 9.4 due Tues Mar 26th, 9am.
- "Mid-term": tentatively scheduled for Week 12 or 13. Comments?
- Transformer modeling Section 11.1 of text, plus lecture notes
 - Nonlinear inductor models Types 93, 98, 96
 - Magnetic materials: B-H characteristics
 - Transformer Inrush initial conditions
 - Energization inrush
 - Recovery inrush
 - Sympathetic inrush
- Next take stock of available ATP transformer models



 $\lambda(0) = 0$; voltage source (red) is Sine wave which turns on at t=0. Note worst-case integration offset in flux linked (green).



で(4)



Type-96" - Hysteretic Weakness -Subleop trajectories. "Flux-Current Loop" Area & Losses 5- Hystesis - EJLy Current (- Anomalous - Stray Losses Rc = 00 if all losses in Type-96

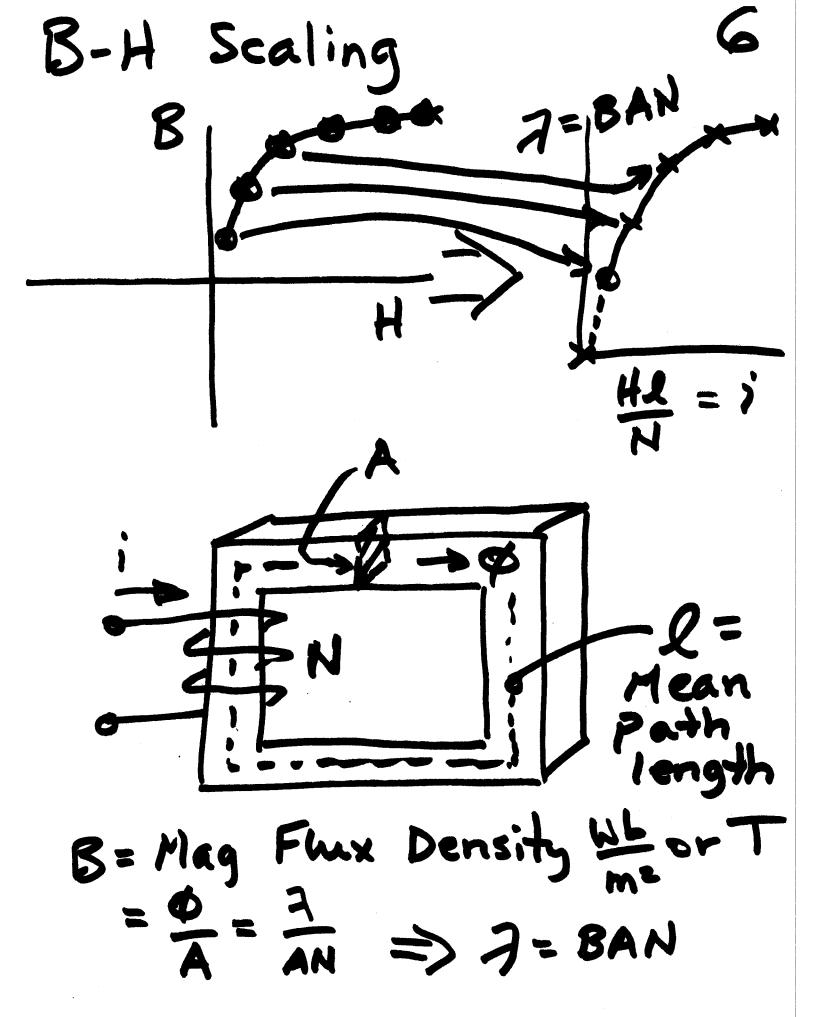
- Reversible - Single-Valued sation Method lewton Iter. - Approx with Local operating Refactorise if segment change. Lss well in contempte stimpte conts. - Size of network 5 - Big Network: Type-98 BAD

- No. of inductors
98-Bad if Lets
93-Better

- No. of Segments Large: 98-Bad 93-6000

Type-13- More Stable.

Type-98 - Operates one timestep outside of proper segment.

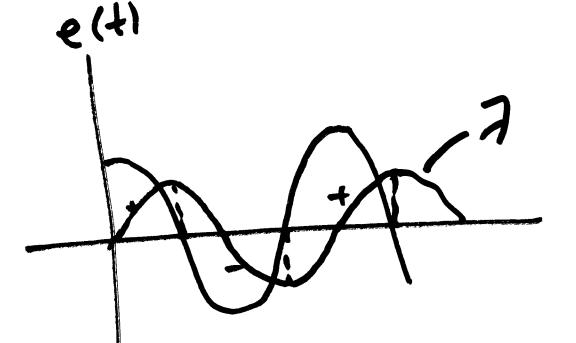


H = Magnetic Field Intensity = MMF drop per unit length along mean path MMF=3= Ni Ampere-turn (Amperes) H= MMF = Ni A-t or Am

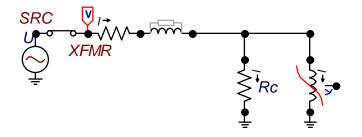
Initialitation Initial Aux = (I(0), FL(0) (0,-.45)

 $e(t) = V_M \sin \omega t + \Phi$ $\lambda(t) = \lambda_m \sin(\omega t + \phi) + \lambda(0) = \lambda_m \phi$ See next page for details of offsets!

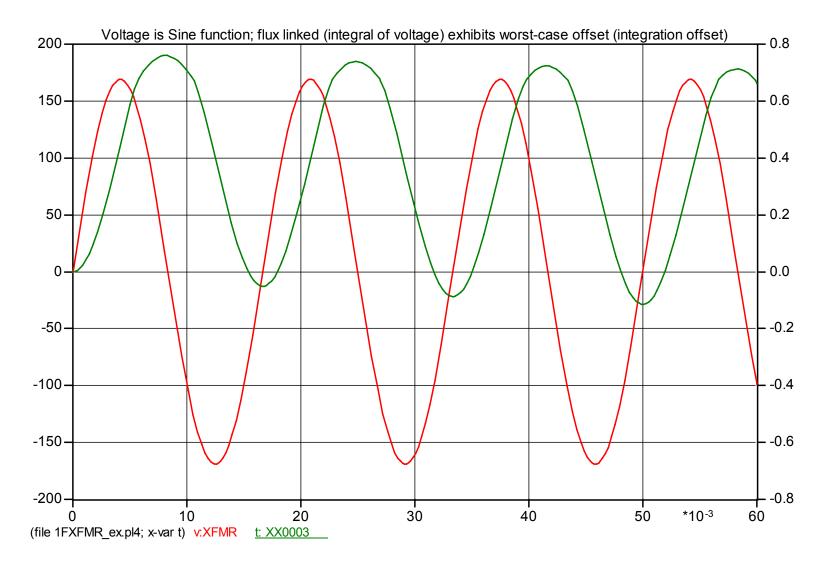
if: $e(t) = V_m \cos(\omega t + \Phi) \leftarrow \Phi = -90^{\circ}$ Bc for sin wave! then: A(t) = (Vmcos (wt+4)+A(0) = Ym sin (wt+4) - Ym sin 4 + 7(0) $|\lambda(t) = \lambda_m \sin(\omega t + \Delta) - \lambda_m \sin(\omega t + \lambda(a))$

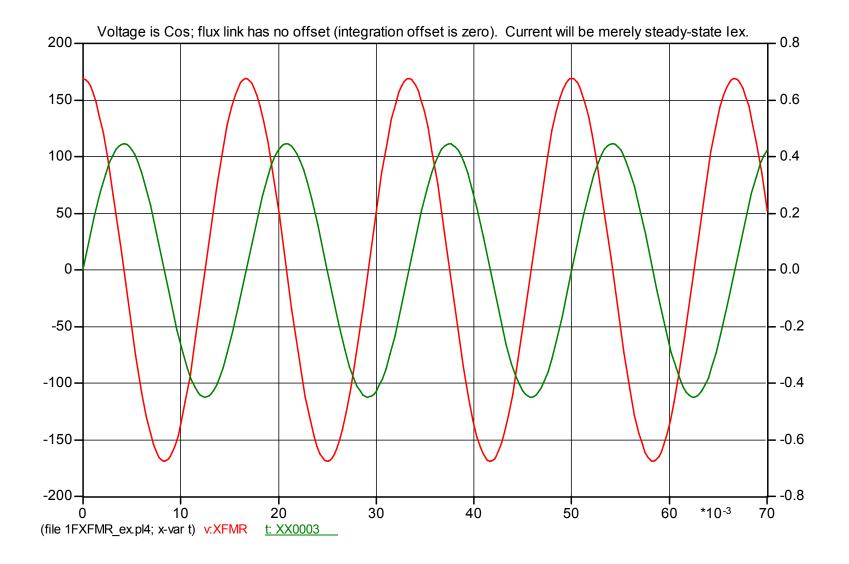


To minimize inrush, Switch on at Vp or - Vp! (assumes 7(6)=0).



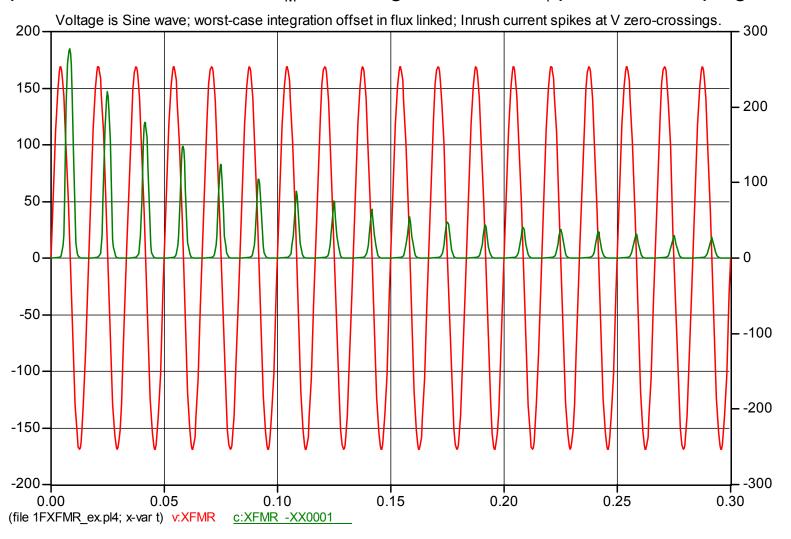
 $\lambda(0) = 0$; voltage source (red) is Sine wave which turns on at t=0. Note worst-case integration offset in flux linked (green).





Special case to illustrate how to get rid of integration offset. Energize transformer at plus or minus peak voltage (Cos voltage function) and then the flux linked will have zero offset. (Again, this assumes that residual flux linked $\lambda(0)$ in transformer core is zero. Unfortunately, $\lambda(0)$ cannot be known or exactly

predicted). Cases below go back to worst-case integration offset to illustrate the characteristics of inrush current. Inrush current spikes lag voltage by 90° as would be expected of an inductance $L_{\rm M}$. Winding resistance $R_{\rm 1}$ provides damping.



Same case as above, inrush current is overplotted with flux linked. See how flux linked begins with full offset, but the offset decays due to the damping effect of R_1 . Rate of decay is not exactly exponential like in a linear R-L circuit, due to nonlinear (saturable) L_M characteristic. Decay is initially quite rapid while L_M is in full saturation, but rate of decay is slower as it progresses (less saturation => smaller current spikes => less damping).

