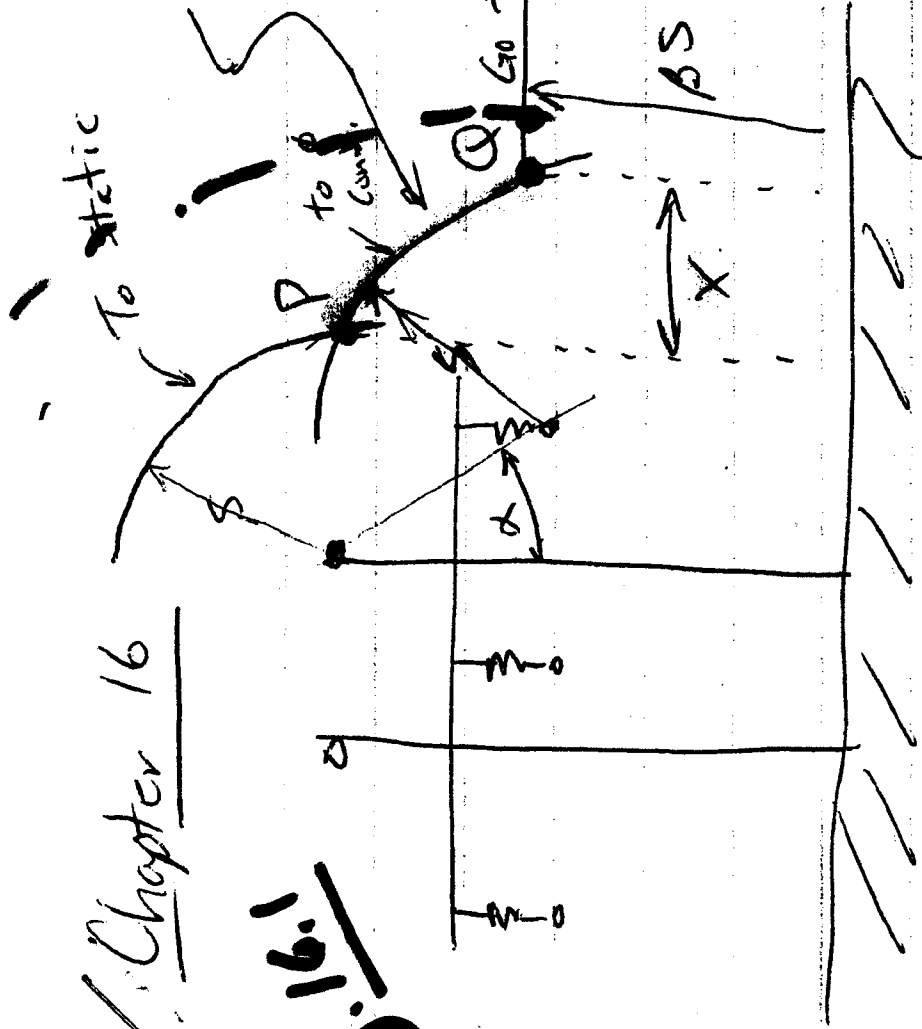


### Topics for Today:

- Course Info:
  - Web page: <https://pages.mtu.edu/~barnork/ee5220/>
  - Book, references, syllabus, more are on web page.
  - Software - Matlab. ATP/EMTP [ License - [www.emtp.org](http://www.emtp.org) ] ATP tutorials posted on our course web page
  - [EE5220-L@mtu.edu](mailto:EE5220-L@mtu.edu) (participation = min half letter grade)
- Hmwk 10 (Probs. 5.7 & 14.5) due Tues Apr 19<sup>th</sup> 9am.
- Term Project - Final Report - completed by Mon April 25<sup>th</sup> 9am
- Term Project - On-campus teams present on Monday Apr 25<sup>th</sup> 3pm
- Insulation design and coordination - Chapter 16
  - Shielding design for overhead lines
  - CB ratings in general
  - NESC tables for conductor separation, corona discharge
  - BIL and BSL levels vs. nominal voltage ratings
  - Comments on L-G vs. L-L overvoltages
  - Corona characteristic - nonlinear capacitance.

Fig. 16.1



Strike Distance  $S = 10I^{0.6}$

$$I = kA$$

$S = \text{meters}$

Quite likely to hit if it gets within  $S$  meters of conductor.

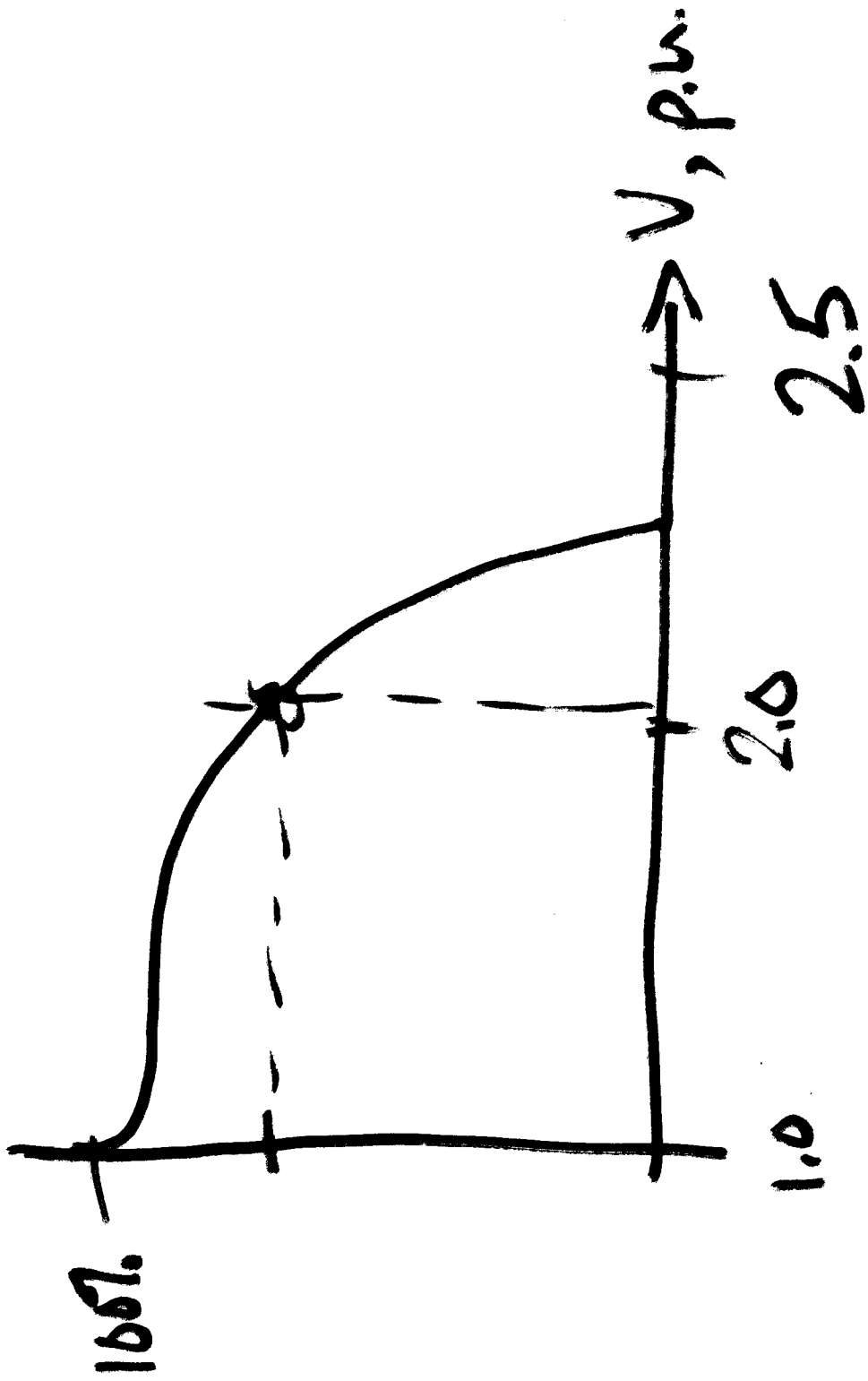
$$\beta \approx 0.8 - E_{HV}$$

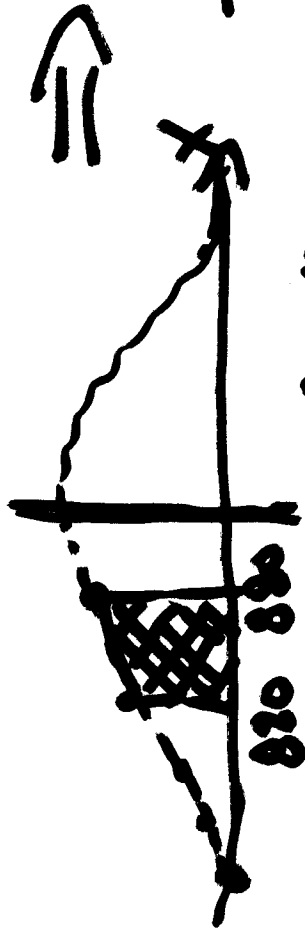
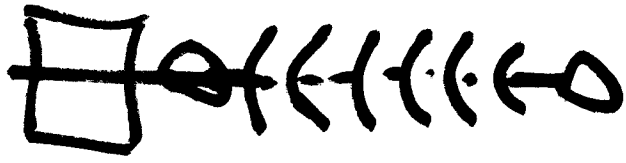
$$0.67 - U_{HV}$$

Shielding Failure Occurs over arc P-Q.

At same current value  $I_{max}$ , P & Q will coincide.

No shielding failure above  $I_{max}$ .

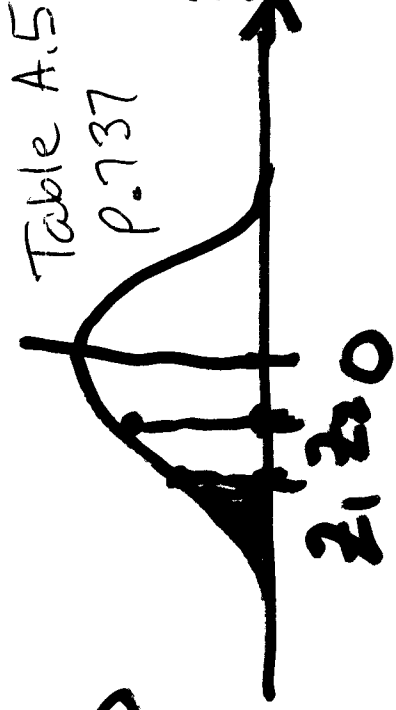




$$CFO = 920 \text{ kV}$$

( $\mu$ )

$$\sigma = 5\%$$



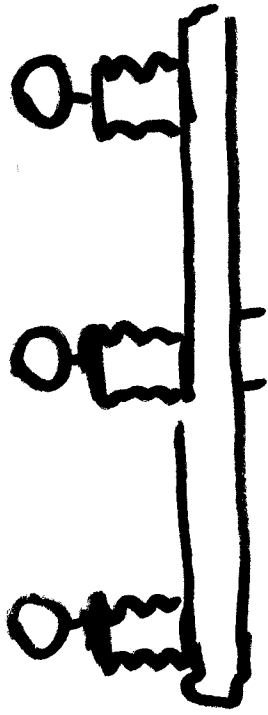
$$Z = \frac{x - \mu}{\sigma}$$

Often need to know P of  $V_T$  falling within a range of values.  $P(820 < V_T < 980) = P(Z < 2.17) - P(Z < -2.17)$

$$P(820 < V_T < 980 \text{ kV}) = \underline{\underline{?}} \Rightarrow \underline{\underline{.1922 - .0148}}$$

$$Z_1 = \frac{(820 - 920)}{46} = \underline{\underline{-2.174}} = \underline{\underline{17.7\%}}$$

$$Z_2 = \frac{(980 - 920)}{46} = \underline{\underline{12.609}} = \underline{\underline{0.8696}}$$

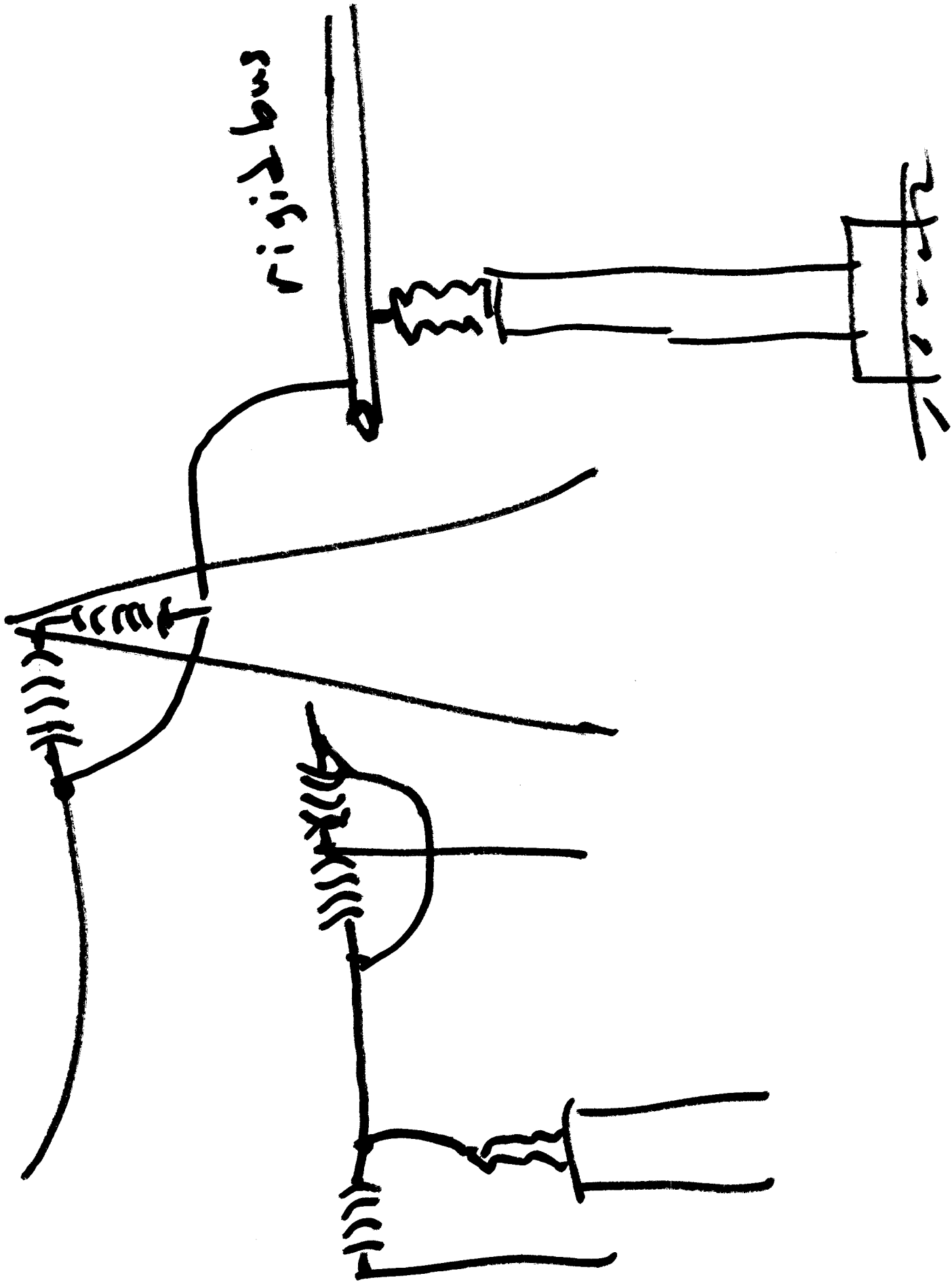


# Typical Spacings and Clearances in a Substation

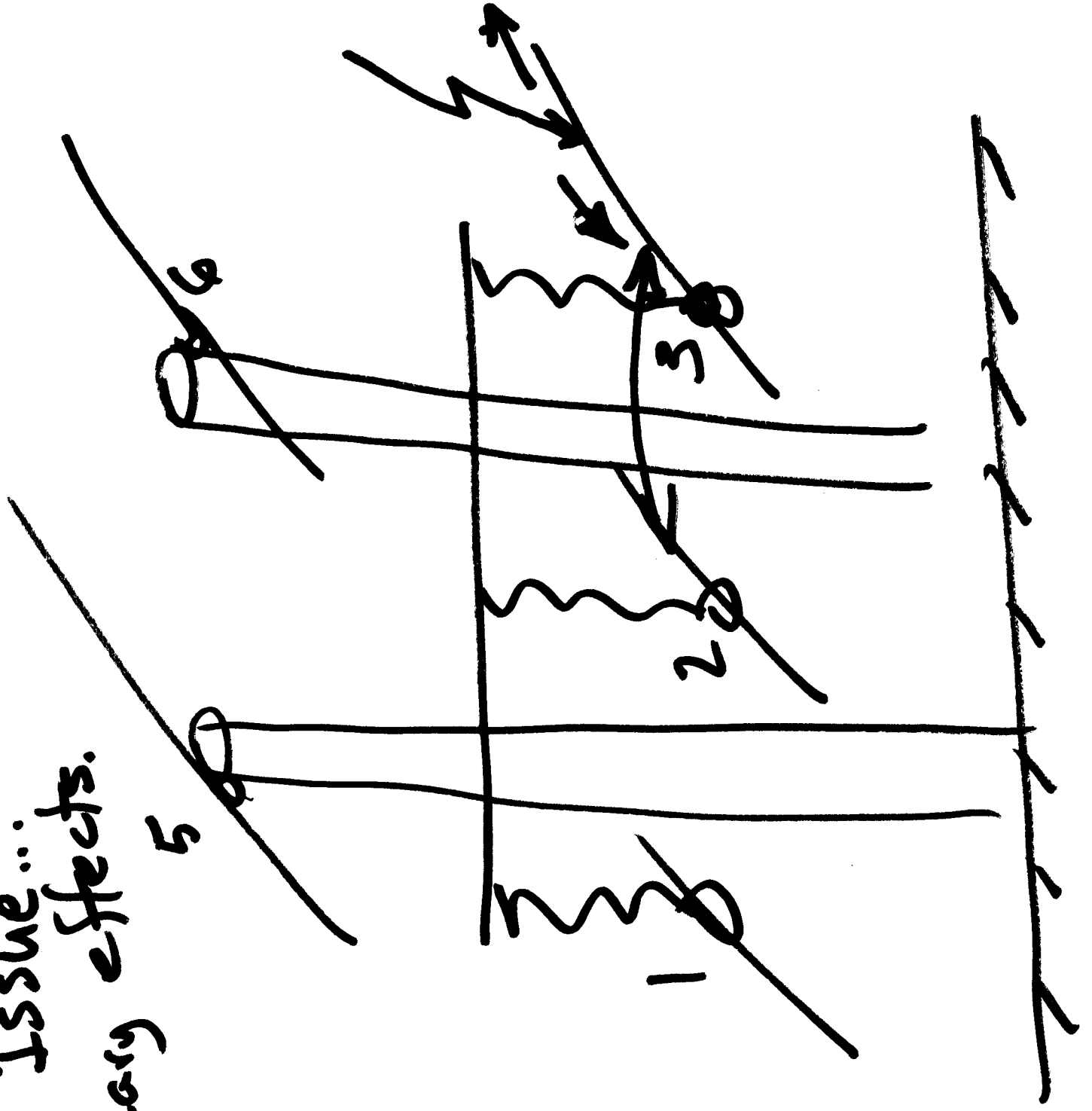
See up-to-date NESC to verify !

Voltage Level		Min Conductor Spacing			Min Switch Spacing Ph-Ph			Min L-L Phase Clearance	Min No. Bells at Deadend	Min Cable Size	Min Bus Size
KV (L-L)	BIL (kV)	Cent-Cent	Ph-Gnd	To Grade	Horngap	V Break	H Break				
7.5	95 <sup>2.0</sup>	1'-6"	7 1/2"	8'	3'	18"	2'-6"	7"	1	#2	1/2"
15	110	2'	10"	9'	3'	2'	2'-6"	12"	2	#2	1/2"
23	150	2'-6"	12"	10'	4'	2'-6"	3'	15"	3	#2	1/2"
34.5	200	3'	15"	10'	5'	3'	4'	18"	4	1/0	1/2"
46	250	4'	1'-6"	10'	6'	4'	5'	21"	4	1/0	1/2"
69	350	5'	2'-5"	11'	7'	5'	6'	31"	5	1/0	1/2"
115	550	7'	3'-7 1/2"	12'	10'	7'	9'	53"	8	4/0	1/2"
138	650	8'	4'-1"	13'	12'	8'	11'	63"	10	250	1/2"
161	750	9'	4'-10"	14'	14'	9'	13'	72"	12	350	1"
230	900	11'	6'-1/2"	15'	16'	11'	16'	89"	14	500	1"
230	1050	13'	7'-3"	16'	18'	13'	18'	105"	16	750	1 1/4"
345	1300	15'	8'-5 1/2"	18'	20'	15'	---	119"	19	---	2"
500	1800 <sup>3.0</sup>	25'	12'	---	---	25'	---	---	24	---	4"
765											

Corona

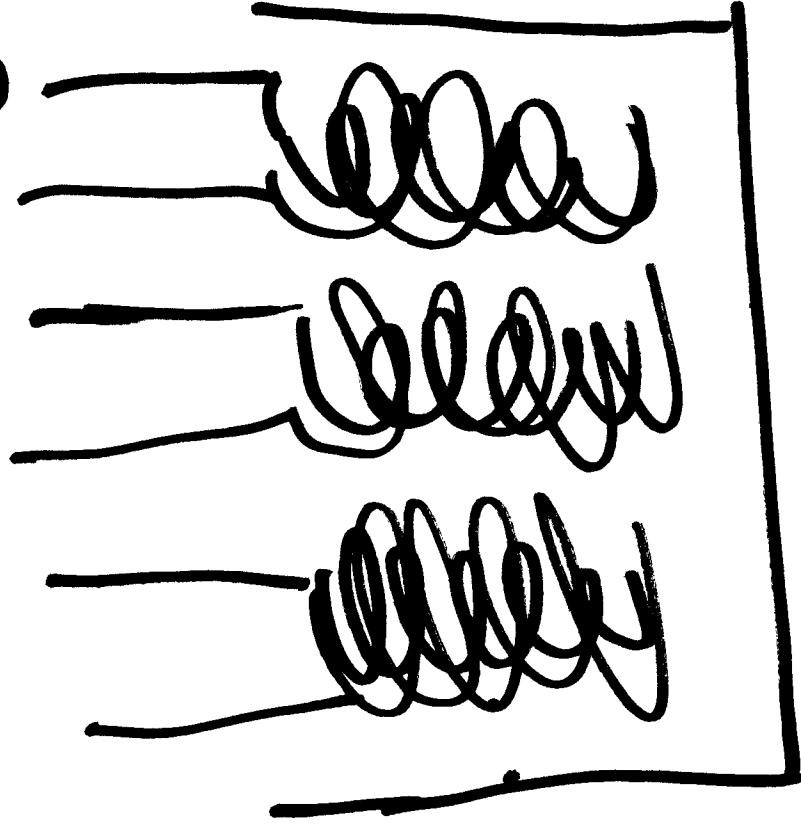


Another Issue...  
Secondary effects.



# Voltage Levels vs. insulation ratings.

$\frac{V_{LN}}{V_{LL}} (L-G)$

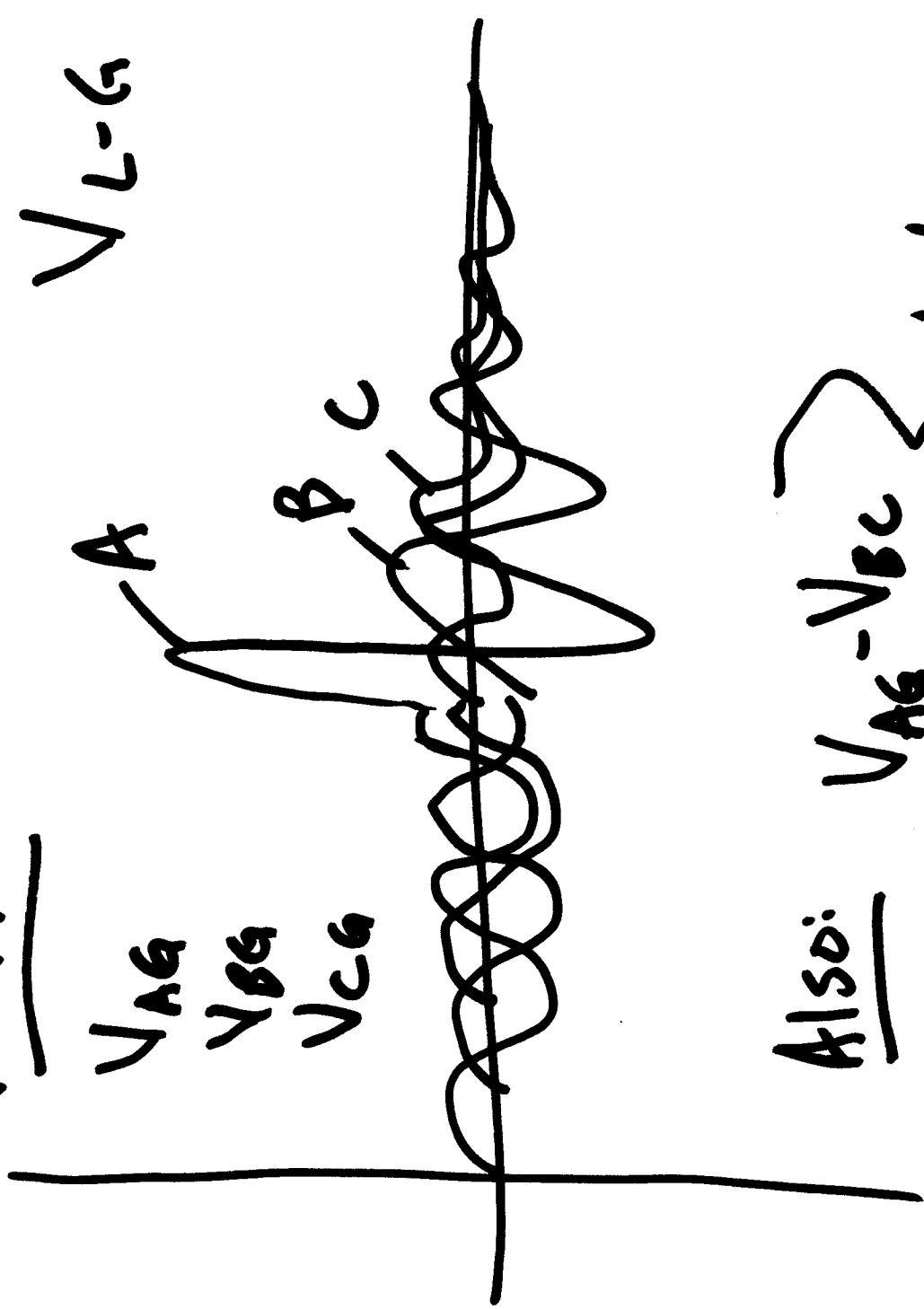


$\frac{V_{LL}}{V_{LN}}$



Plot XY

$V_{AG}$   
 $V_{BG}$   
 $V_{CG}$

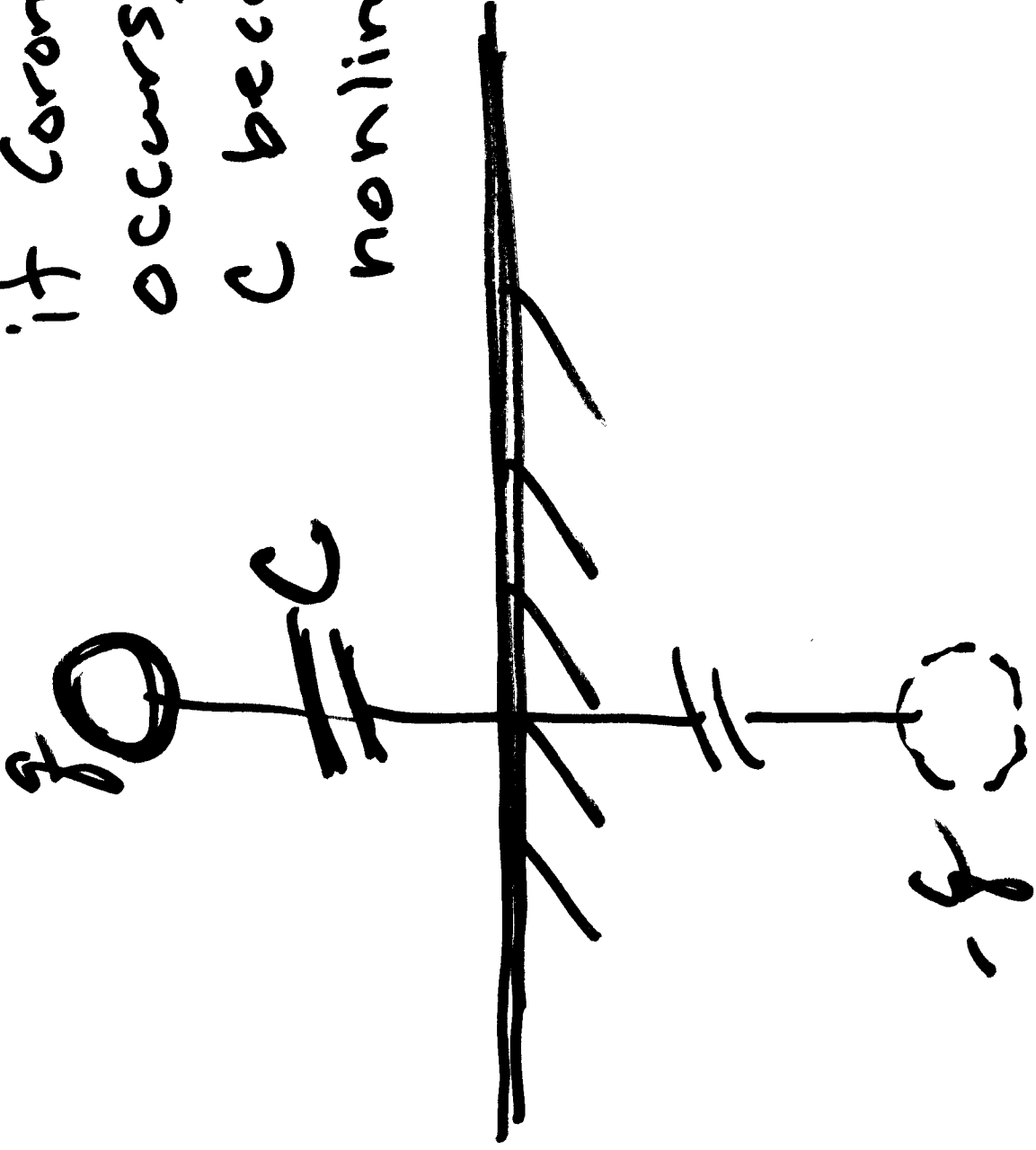


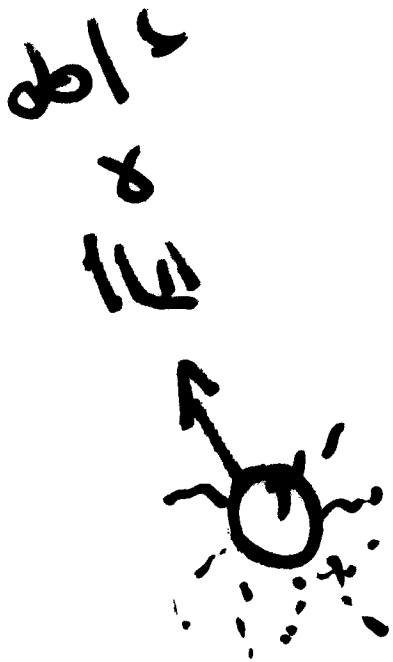
Also:

$V_{AG} - V_{BC}$   
 $V_{BG} - V_{CA}$   
 $V_{CG} - V_{AB}$

L-L

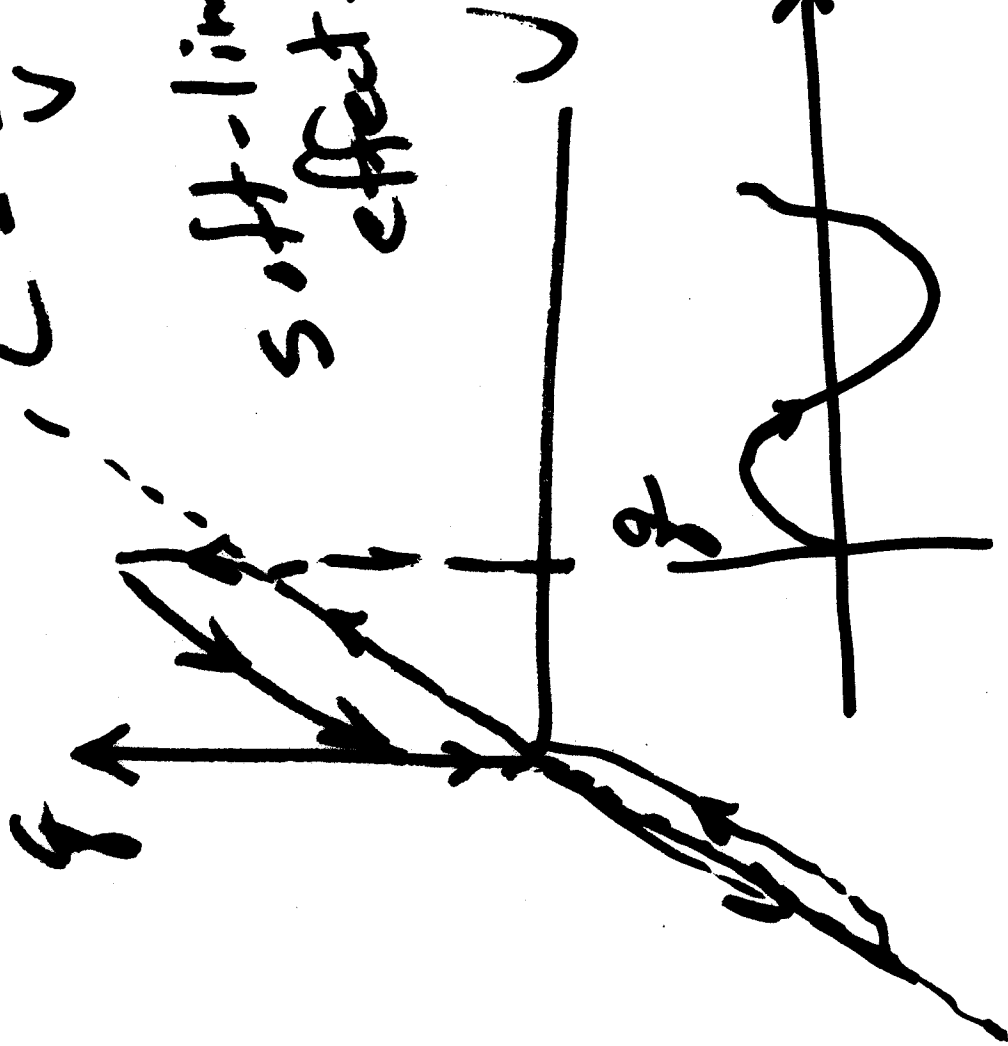
if corona  
occurs,  
C becomes  
nonlinear.



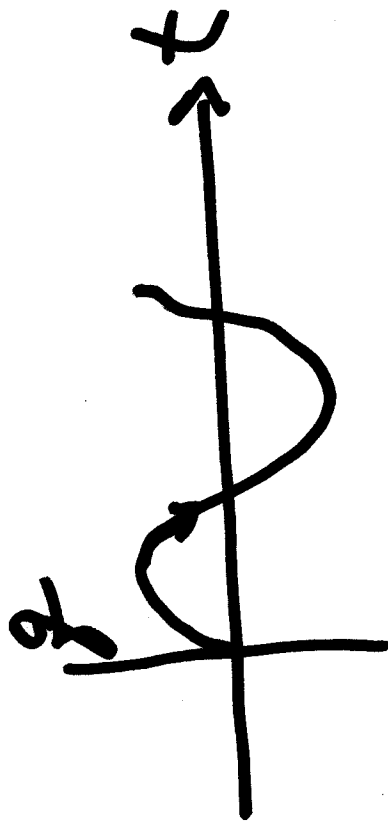


$$C = \frac{Q}{V}$$

soft-limiting  
effect.



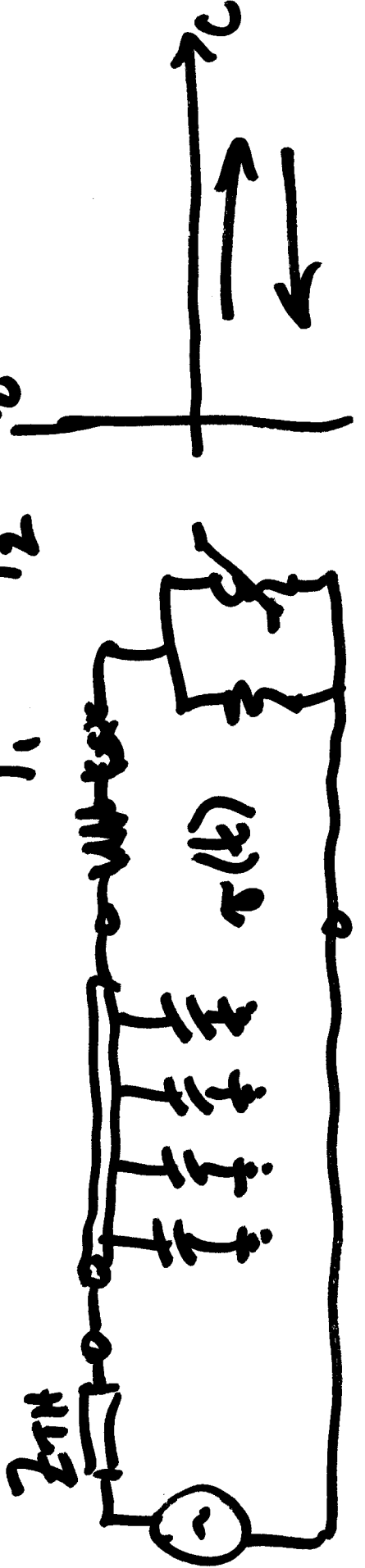
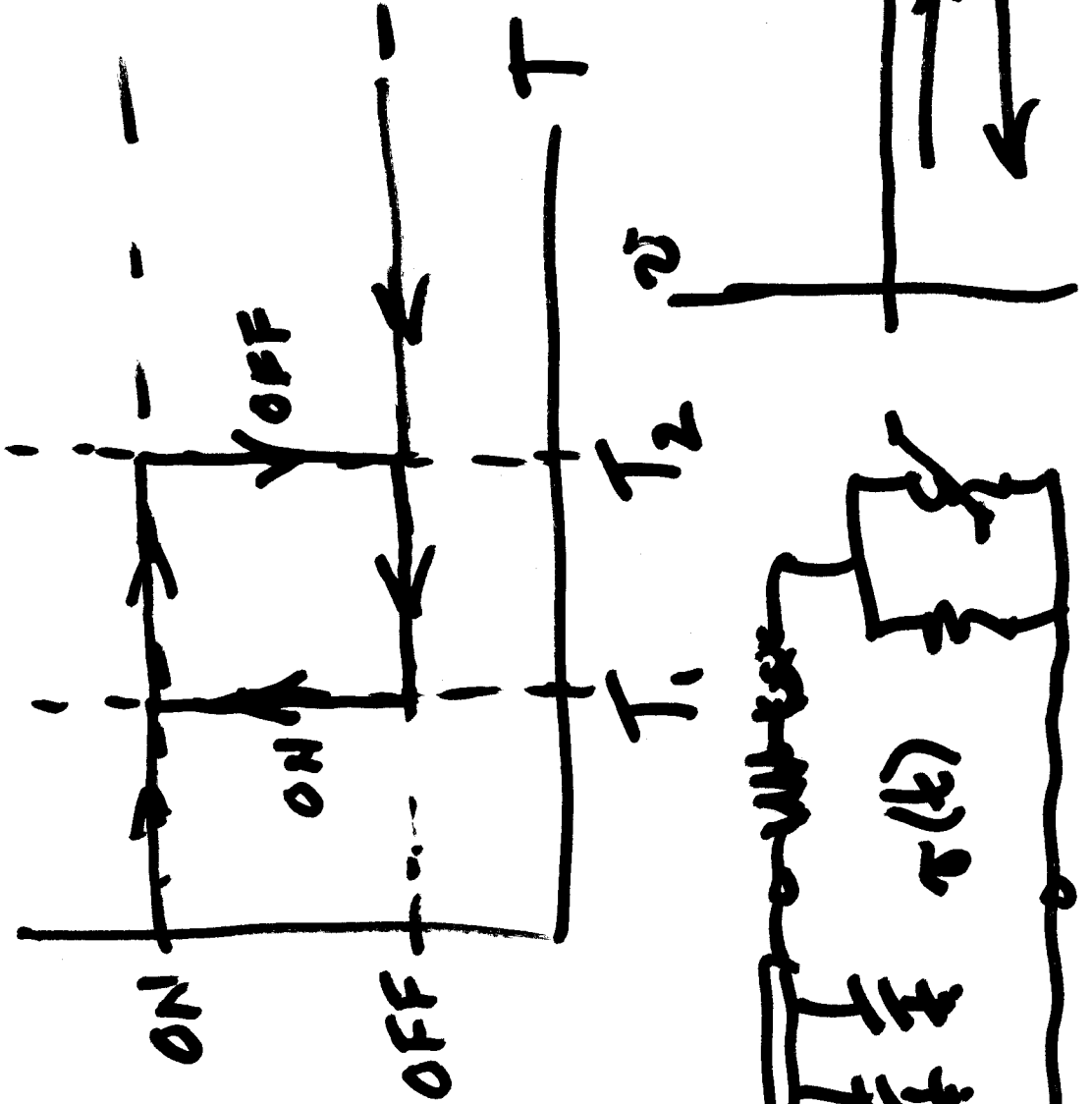
$Q$

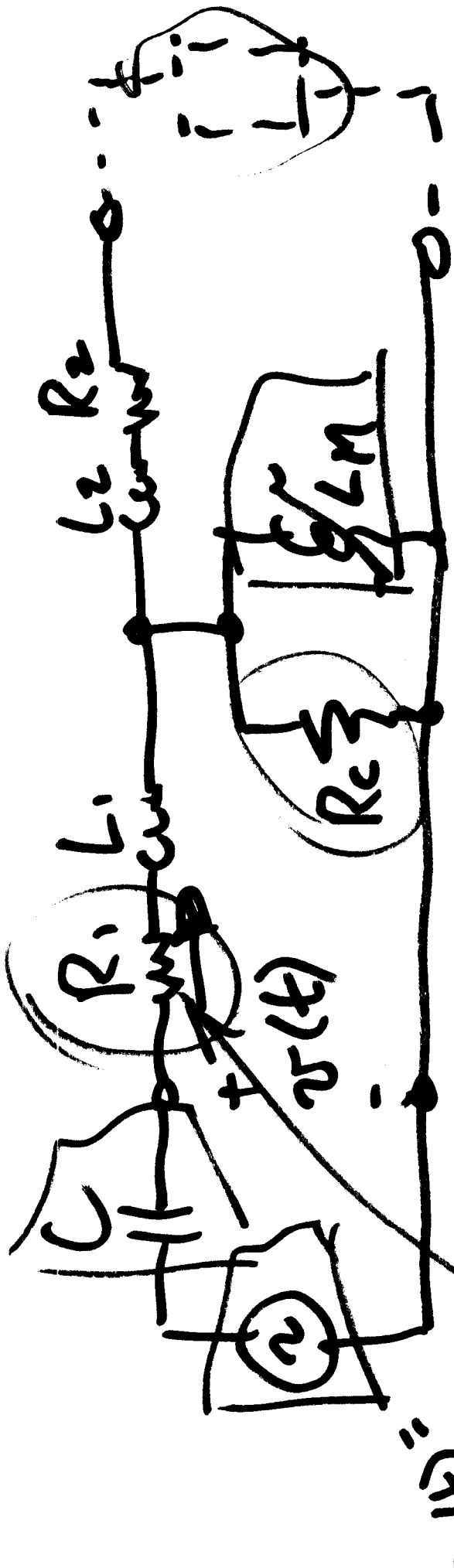


# - Bifurcation

\*

$T_{ues} / \mu m$





$P(t) = i_2(t) v_2(t)$

$P(t) = \frac{v^2(t)}{R_c}$

