

Reactor Switching and Current Chopping

EMTP Training
Nov. 16th, 2001
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The Short Story

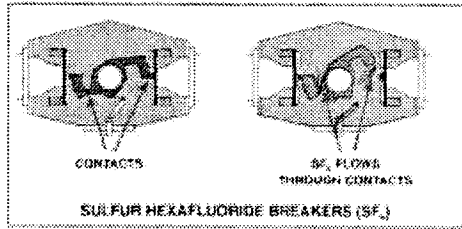
- CB can break currents ^{too} quickly

$$\bullet \mathbf{V} = L \frac{di}{dt}$$

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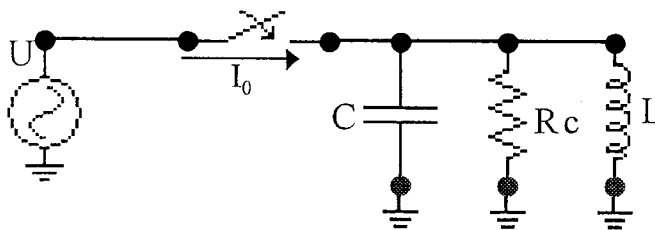
Circuit Breakers

- Most Often SF6 or Air-Blast
- Happens at low levels of inductive current



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Simplistic Equivalent Circuit



- L: inductance of coil
- C: capacitance of coil +bushing capacitance
- R_c : core loss resistance

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Overtoltage

- Assumptions:
No losses, Linear inductance

- Stored energy in inductor:

$$\text{Energy} = \frac{1}{2} L_M I_0^2$$

- Capacitor – Inductor Oscillation

$$\frac{1}{2} C V^2 = \frac{1}{2} L_M I_0^2 \Rightarrow V = I_0 \left(\frac{L_M}{C} \right)^{1/2} = I_0 Z_0$$

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Example

Transformer: : 1 MVA, 13.8 kV,

$I_{\text{exciting}} = 1.5$ A rms, $C = 5000$ pF, $I_0 = 2.5$ A

$$L_M = \frac{V}{\omega I_{\text{exciting}}} = \frac{13,800}{\sqrt{3} \times 377 \times 1.5} = 14H$$

$$Z_0 = \left(\frac{L_M}{C} \right)^{1/2} = \left(\frac{14}{5 \times 10^{-9}} \right)^{1/2} = 53,000\Omega$$

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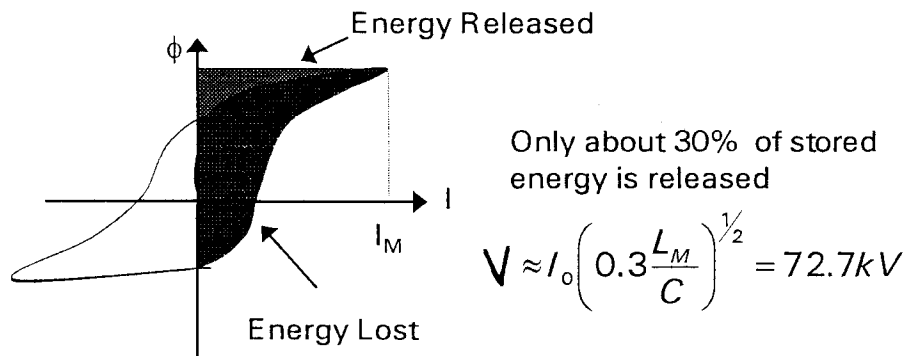
Example p.2

$$f = \frac{(1/L_M C)^{1/2}}{2\pi} = 602 \text{ Hz}$$

$$V = I_0 \left(\frac{L_M}{C} \right)^{1/2} = I_0 \times Z_0 = 2.5 \times 53,000 = 132 \text{ kV}$$

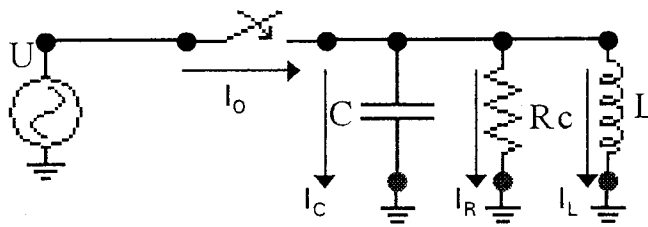
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With Saturation



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Formal Analysis



$$I_C + I_R + I_L = 0$$

$$I_C = C \frac{dV}{dt} \quad I_R = \frac{V}{R} \quad I_L = \frac{1}{L_M} \int V \cdot dt$$

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Formal Analysis 2

$$\frac{d^2V}{dt^2} + \frac{1}{RC} \frac{dV}{dt} + \frac{V}{L_M C} = 0$$

$$V(s) = \frac{sV_0}{s^2 + (s/RC) + (1/L_M C)} + \frac{V_0}{RC} \frac{1}{s^2 + (s/RC) + (1/L_M C)} - \frac{I_0}{C [s^2 + (s/RC) + (1/L_M C)]}$$

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Characteristics of Transients

- Frequency of oscillation is a few kHz for iron core reactors, hundreds of kHz for dry, air-core reactors
- Relatively little energy is trapped
Surge arrestors can usually deal with it

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Detailed Reactor Model

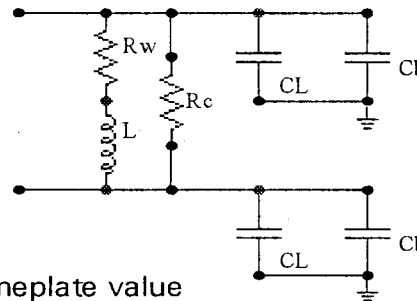
R_c: Core loss; ~1000 pu for iron core, infinite for air core

R_w: Winding resistance; same value as similar transformer winding, ~0.5%

L: Reactor inductance, nameplate value

CL: ½ Winding capacitance; iron core - same as similar transformer winding (See Ch 13, Greenwood); air core : 75 – 150 pF

C_b: Bushing capacitance; 150 – 600 pF



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Harner & Rodrigues

See also: C37.011

Appendix B

Tables B1 → B7

Restrikes

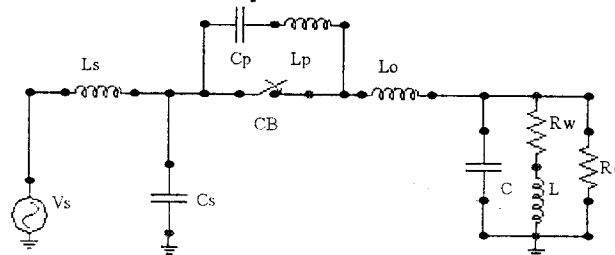
When breaking low level highly reactive currents:

- The arc is weak because the current is not large
- The contacts are not far apart when the arc extinguishes
- The system voltage is near its peak so the recovery voltage can be large

Dependent on how quickly the dielectric strength between the contacts recovers

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Restrike Equivalent Circuit



C_p, L_p : Parasitic capacitance and inductance of the CB;
value ?, use potential grading cap

L_s : Equivalent system inductance

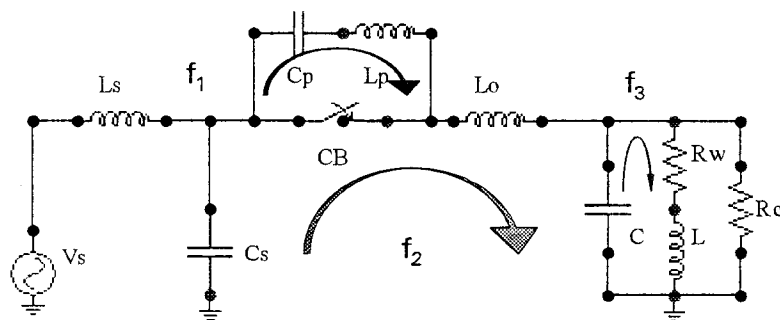
L_o : bus work inductance

C_s : System capacitance; CB bushing and buswork

C : Reactor equivalent capacitance; CB bushing, reactor bushing, winding cap

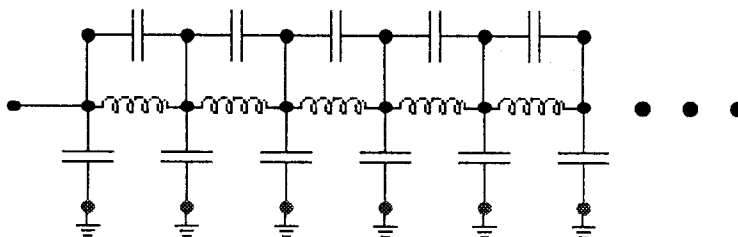
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Frequencies of Oscillation



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High f Equivalent Circuit



With high frequency waves, series capacitance forces uneven voltage distribution. Terminal end sees highest voltage.

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Example: Parkers Lake

2 dry type, air core reactors on 13.8 kV tertiary

Reactor 1: 7Ω -> 27.2 Mvar -> 18.57 mH

Very little capacitance; use 200 pF

Assume $R_{\text{winding}} = 0.1\%$, $R_{\text{core}} = \infty$

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Reactor 1 Predictions

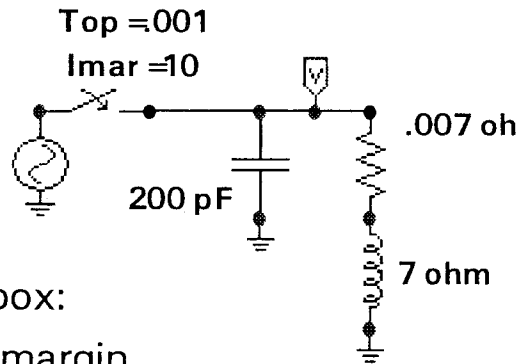
Surge Impedance: $Z_0 = \sqrt{L/C} = 9.64k\Omega$

Frequency: $f_0 = \frac{\sqrt{1/LC}}{2\pi} = 82.6kHz$

$$peak \approx I_{chop} \times Z_0$$

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Reactor Opening: Simulation



- Switch dialog box:
Imar – current margin
switch opens if $t > T\text{-op}$ AND $|i| < I\text{mar}$

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Reactor 2

Reactor 2: 12.7Ω -> 15 Mvar -> 33.69 mH

Has parallel capacitor to lower surge impedance and frequency.

What's the value?

My guess: $0.2 \mu\text{F}$

Assume $R_{\text{winding}} = 0.1\%$, $R_{\text{core}} = \infty$

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Reactor 2 Predictions

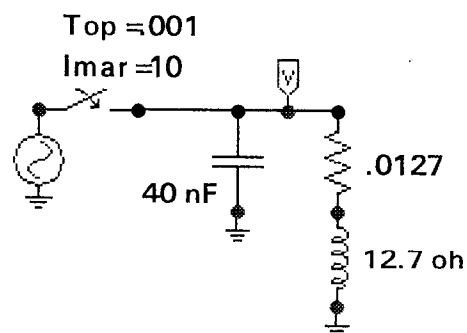
Surge Impedance: $Z_0 = \sqrt{L/C} = 410.4\Omega$

Frequency: $f_0 = \frac{\sqrt{1/LC}}{2\pi} = 1.94\text{kHz}$

$$peak \approx I_{chop} \times Z_0$$

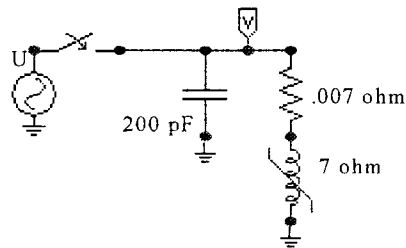
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Reactor Opening: Simulation



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Try using a saturable inductor



Use: L(i) Type 98 – Dialog Box

CURR: peak current in A

FLUX: flux in Volt-sec

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Current/Flux Data

Need I_{peak} and magnitude ($\int V dt$)

13.8 kV \rightarrow 7967V I-n

$I = V/Z \rightarrow I = 1138 \text{ A rms} \rightarrow 1610 \text{ A peak}$

$$\text{Volt-sec} = \frac{7967 \times 2^{1/2}}{2 \pi 60} = 29.888 \text{ V-sec}$$

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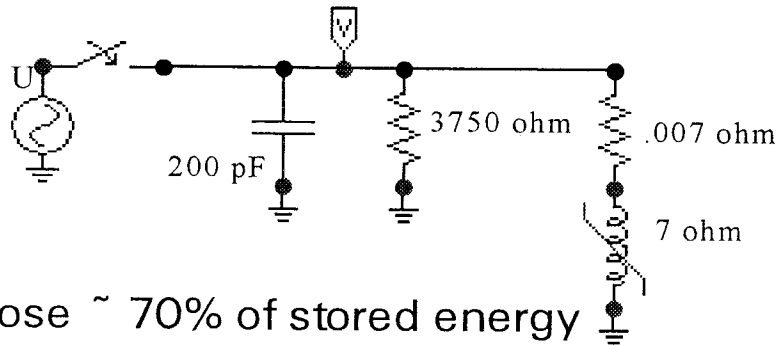
Saturation Data

V (pu)	Peak Current (A)	Flux (Volt-sec)
1.0	1610	29.888
1.1	5506	32.877

"Characteristic" tab in "Component" dialog box

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Add excitation losses

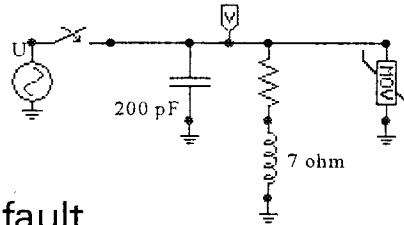


Lose ~ 70% of stored energy

Gives $R = 3750 \Omega$

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Add a surge arrester



Use "MOV Type 92"

Attributes: change default

$V_{ref} = 2 \times \text{system } V$

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Surge Arrester Data

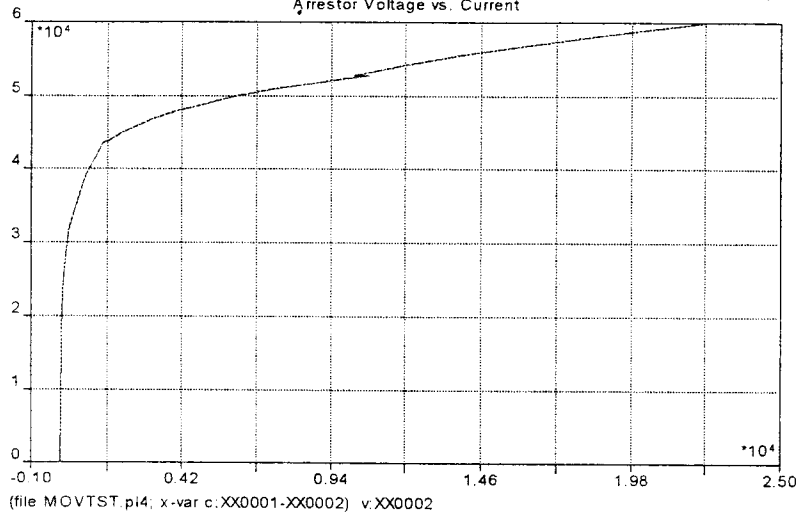
Current (A)	Voltage (V)
5*	13800*
1500	43700
3000	46400
5000	48500
10000	52900
20000	58500
40000	65900

Need to know low current characteristic
Difficult to find (I made it up)

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Surge Arrestor Characteristic

Arrestor Voltage vs. Current



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