

Topics for Today:

- Questions from last lectures?
- Comments on Homework #2
- Augmentation for L-G Fault - signs !

Today - system data for computer studies

- Transformer Data
 - More on tap-changing transformers
- Coming up - keep studying Chapters 3 & 4.

- Nonlinear systems of equations
- Newton Iterative Method
- Newton-Raphson Load Flow Formulation
- Everybody have access to Aspen?

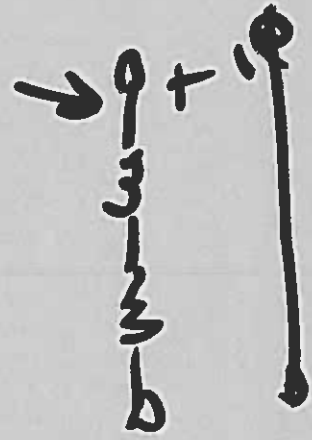
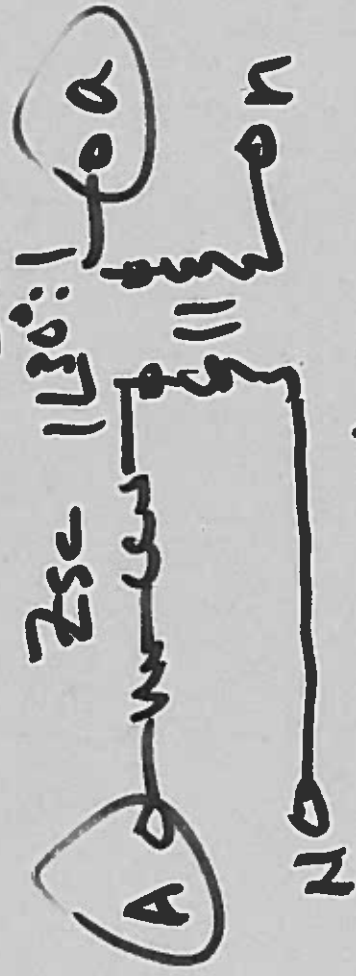
HMWK #2



$$[Y] \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ I_4 \end{bmatrix} + I_{sc}$$

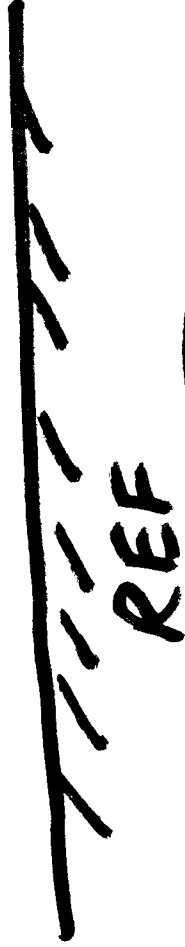
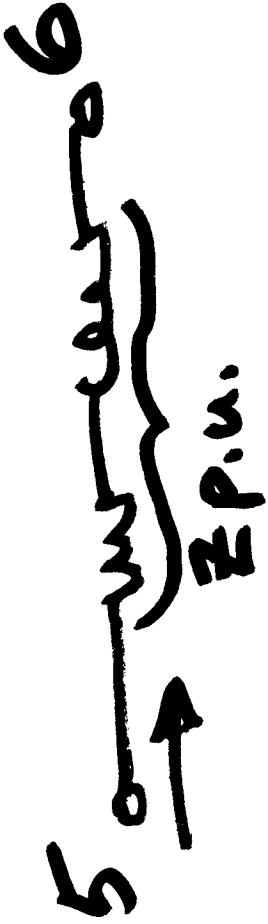
$$I_4 = y_{41}V_1 + y_{42}V_2 + y_{43}V_3 + y_{44}V_4 + I_{sc}$$

- * - Not matching P.u. Base Voltages
- * - LTC / TCUL (V, Q)
- Phase-shifting $x_{\text{far}} (P)$
- * - Per Phase Calcs - $\Delta-T$ phase shifts



$$\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix}$$

XFMRS - Use \bullet L-N
Per Phase Eguiv.



In [Ybus] $Y_{66} = -\frac{1}{Z_{66}}$

Basis 2-winding
XFMR is simple.

How about?

- LTC (or TCUL)
- Phase Shifter (PS)

Basic Approach: Develop π -Equiv and handle just like T-Line.

Note: a:1 represents nominal turns ratio, i.e. the ratio between the base voltages of the per unit system. Taken in the context of a per unit system, a=1 and the transformer can be represented as a simple series impedance.
 c:1 represents the off-nominal turns ratio, and so its effect must be included in [Ybus].

One-Line:



Per-unit per-phase

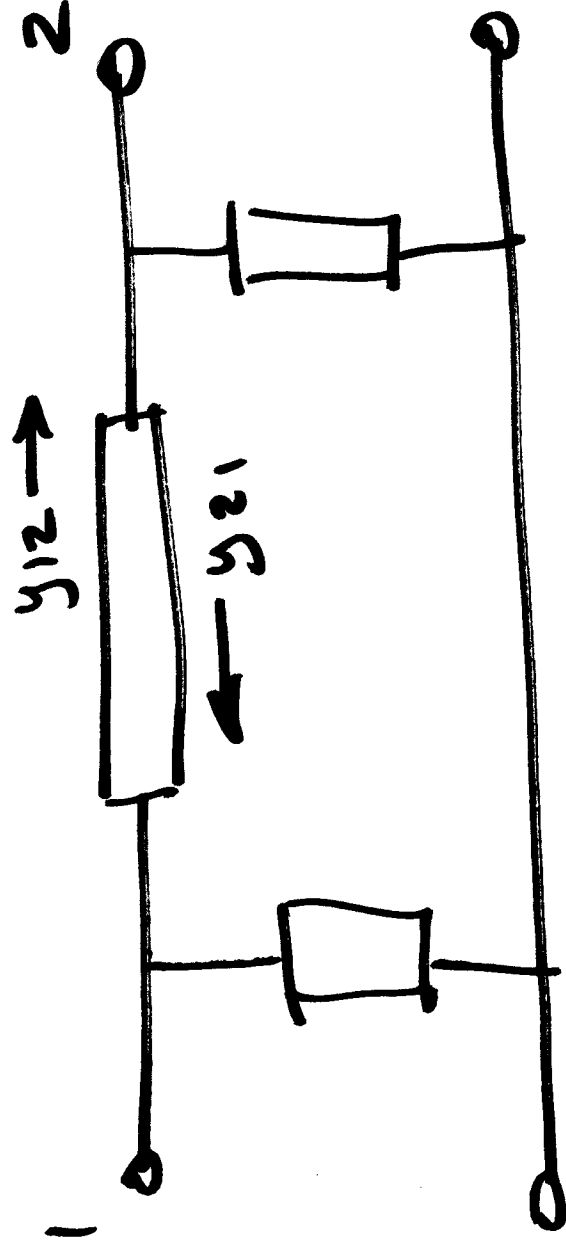
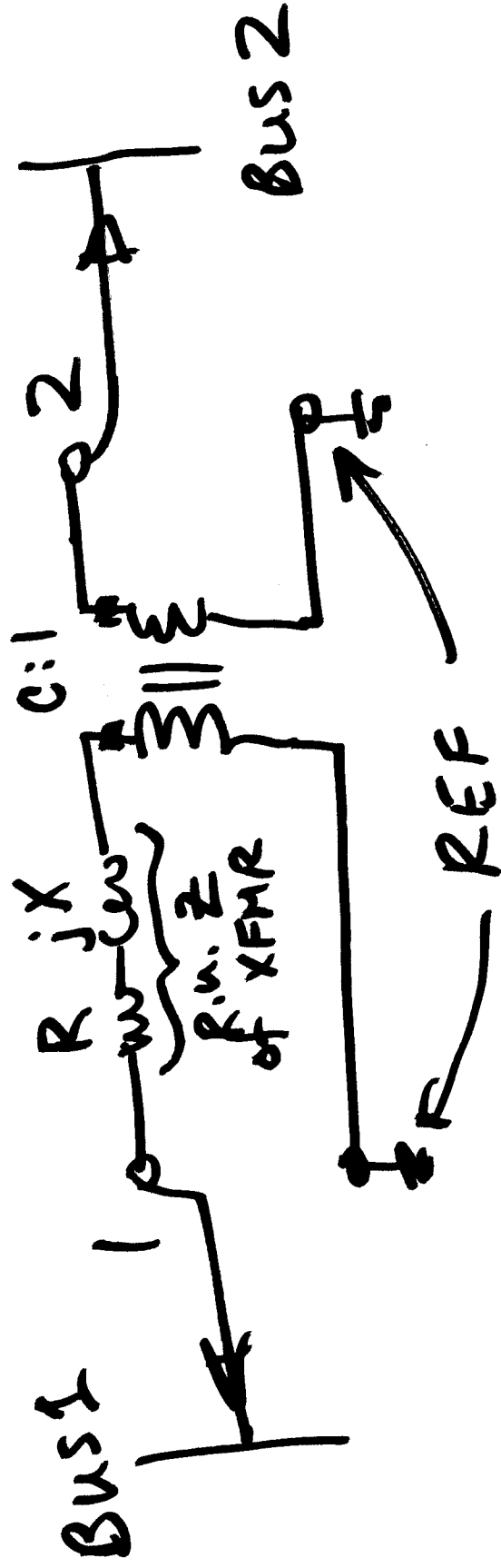


Tap-Changers

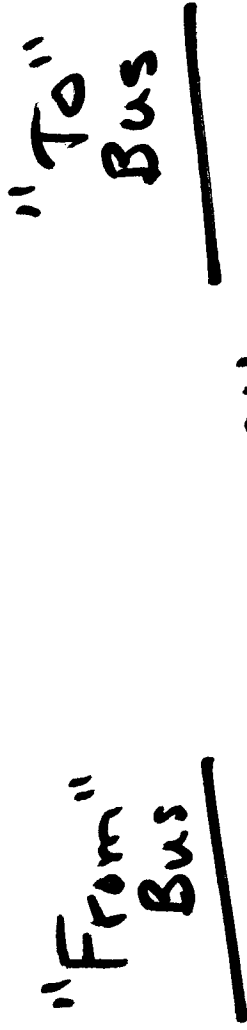


- LTC's
 - Phase-Shift

NOMINAL TURNS RATIO \uparrow \pm Adjustment in phase angle (ps) or Volt mag (LTC)



Tap Changing XFMRs - Variations (P.u. representations)



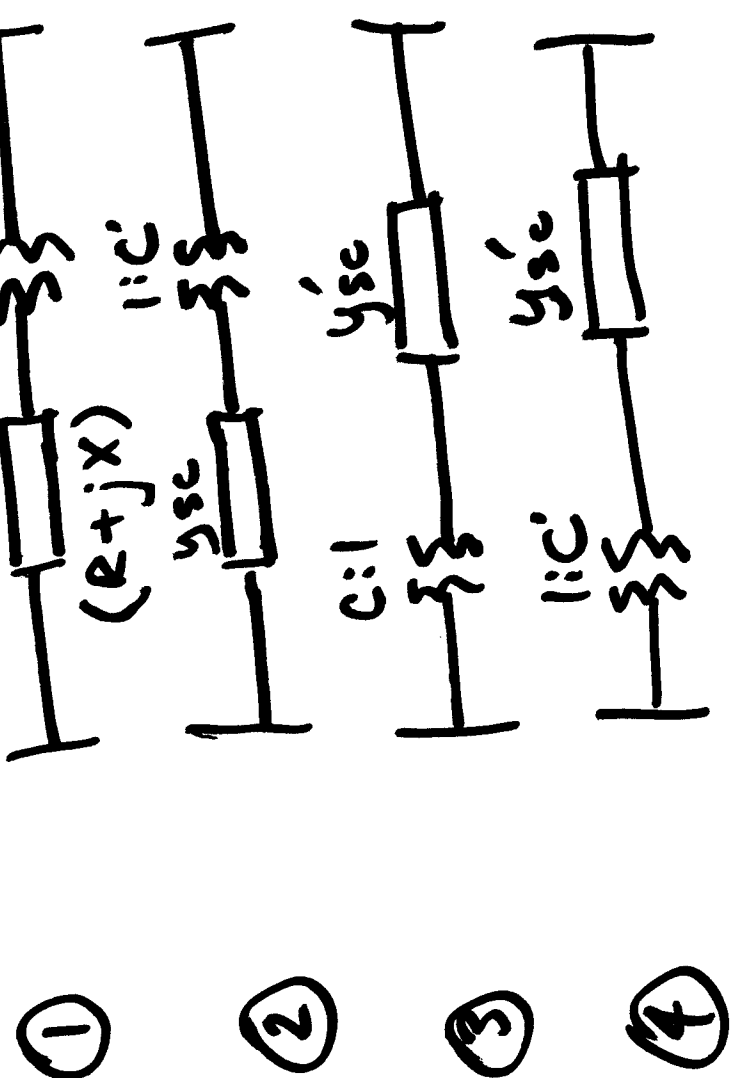
$$y_{sc} = \frac{1}{R+jX}$$

"C" is off-nominal turns ratio. In general C is complex.

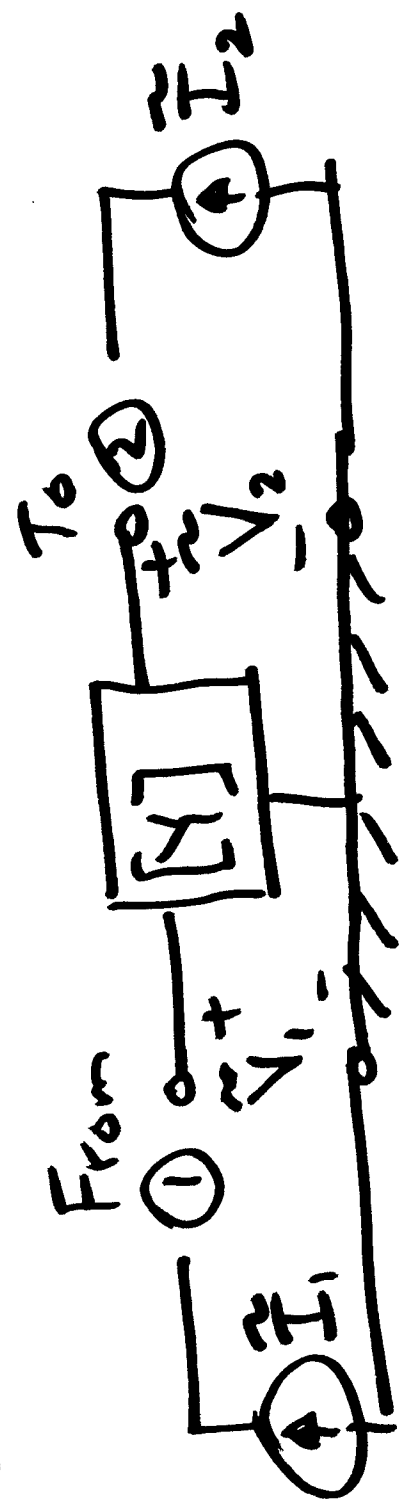
C is real for LTC.
C is complex for PS.

If $|C| \neq 1$ then magnitude change.

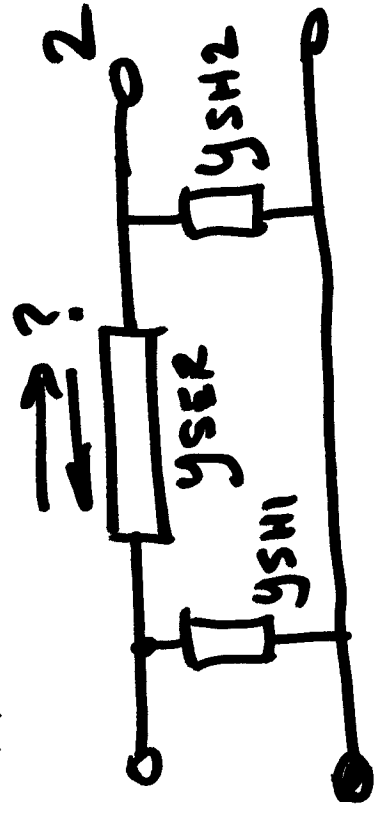
If C is complex, Phase Shift.



Standard Approach:



$$\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$



Goal:

$$y_{11} = y_{SER} + y_{SH1}$$

$$y_{12} = -y_{SER}$$

$$y_{21} = -y_{SER}$$

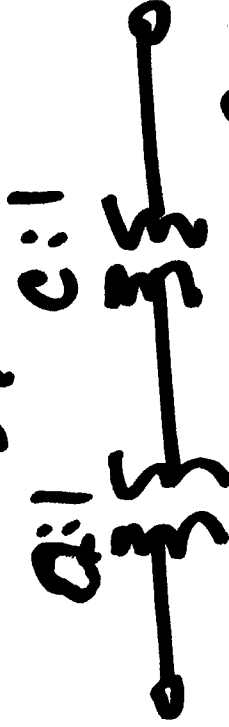
$$y_{22} = y_{SER} + y_{SH2}$$

TAP-CHANGERS

On One-Line Diags:



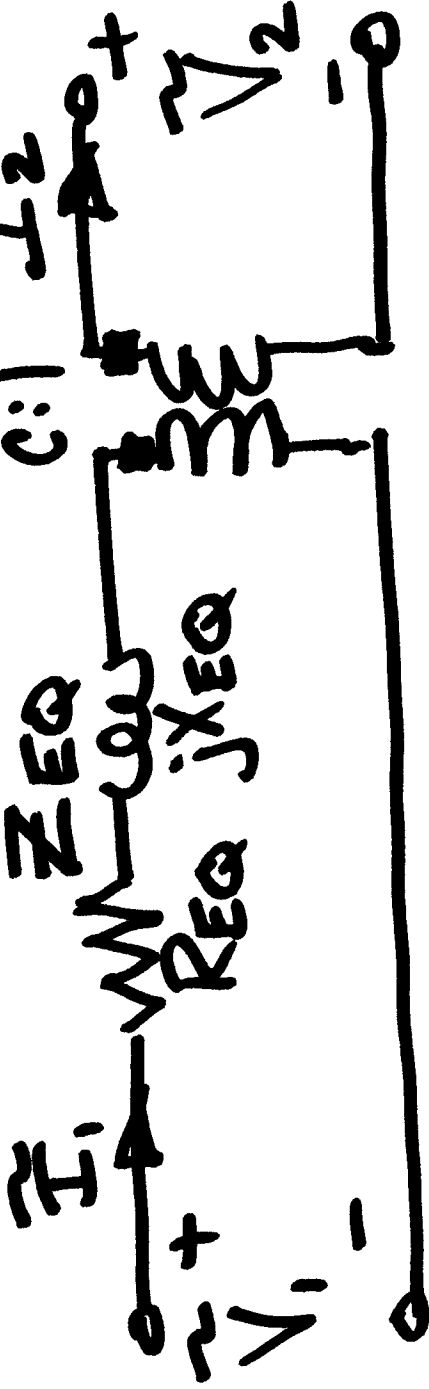
Conceptually:



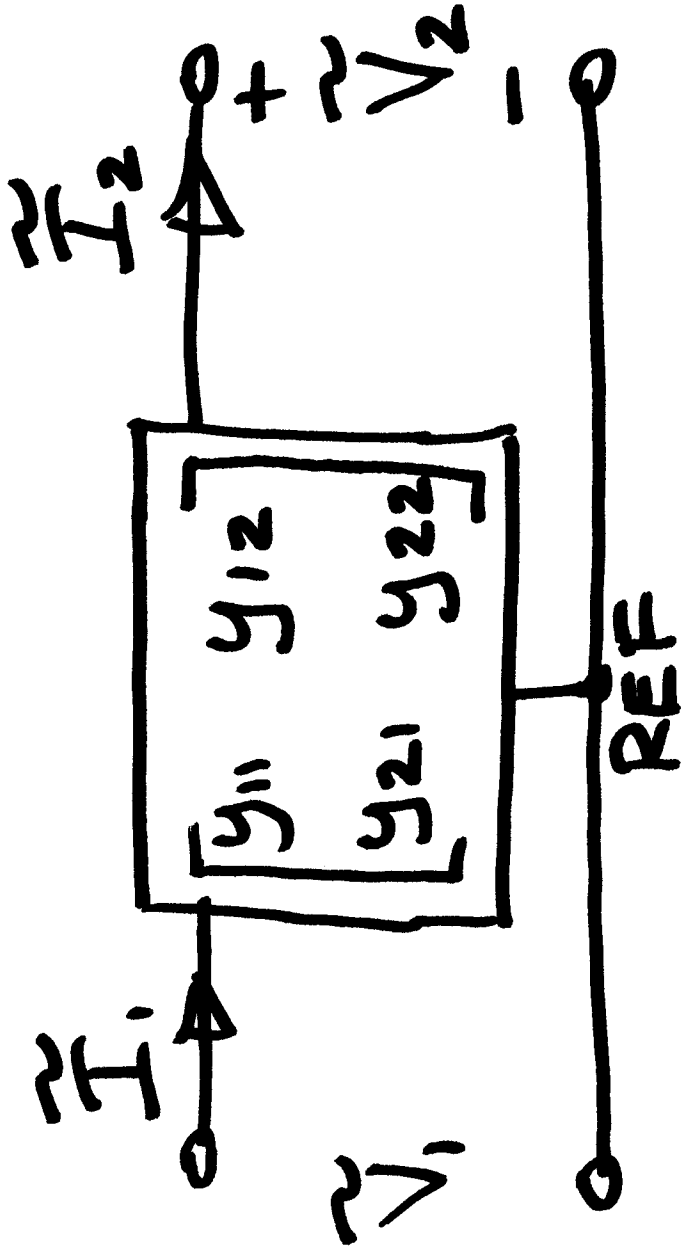
Nominal
Voltage
Ratio

↑ off-nominal
turns ratio
due to
Tap changer

In per unit, nominal
transformation "disappears"



Generally, we can describe this as a 2-node [Y]



where

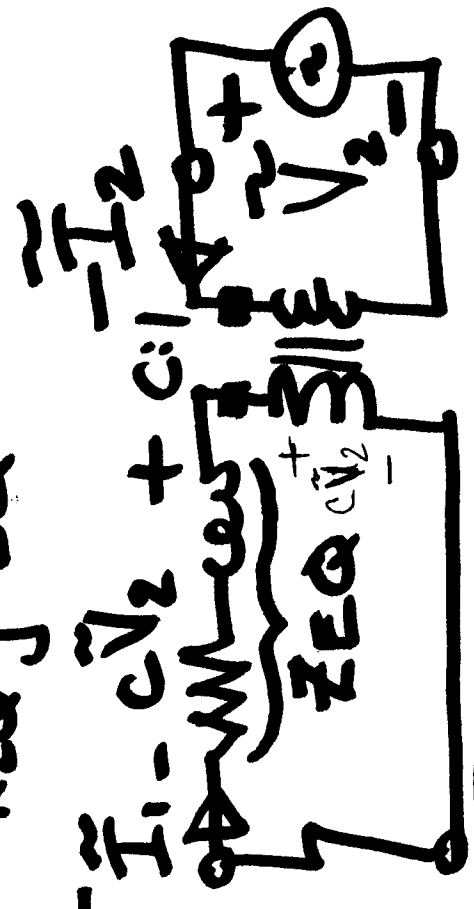
$$\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} I_1 \\ -I_2 \end{bmatrix}$$

Strategically using shorts ~~on~~
~~the~~ values of $[Y]$, we can isolate on



$$y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0}$$

$$= \frac{1}{Z_{EQ}} = Y_{EQ} = \frac{1}{R + j\omega C}$$



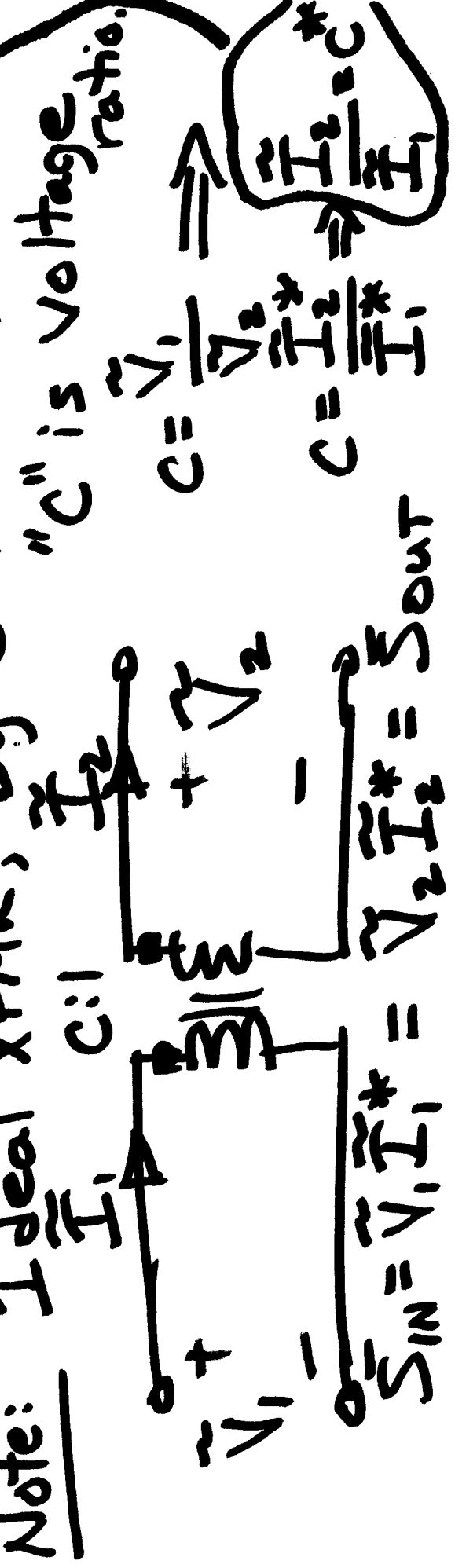
$$y_{22} = -\frac{I_1}{V_2} \Big|_{V_1=0}$$

$$= \frac{1}{Z_{EQ}/|C|^2} = |C|^2 Y_{EQ}$$

$$y_{12} = \frac{\tilde{I}_1}{\tilde{V}_2} \Big|_{\tilde{V}_1=0} = \frac{-C \tilde{V}_2 / Z_{EQ}}{\tilde{V}_2} = -C Y_{EQ}^d$$

$$y_{21} = \frac{-\tilde{I}_2}{\tilde{V}_1} \Big|_{\tilde{V}_2=0} = \frac{-C^* \tilde{I}_1}{\tilde{V}_1} = -C^* Y_{EQ}$$

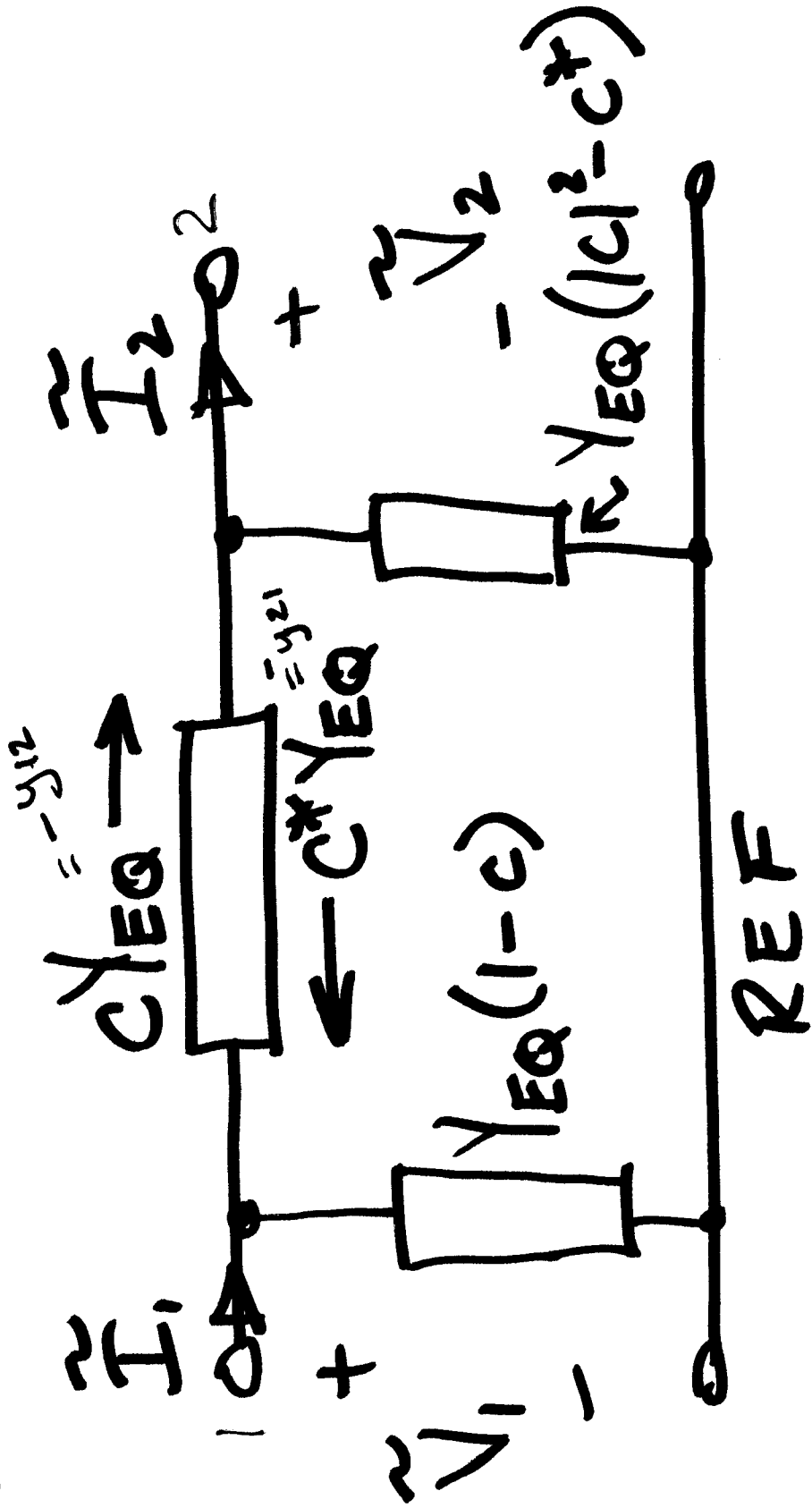
Note: Ideal XFMR, by definition, has



If we "reverse engineer" our e)

$[Y]$ into an equivalent 2-bus

network, then



Observations:

- LTC (TCL) has a c that is Real.

\therefore Transfer Admittances

$$C_{YEQ} = C^* Y_{EQ} \\ \Rightarrow \text{Bilateral. } (y_{12} = y_{21})$$

- Phase-Shifter (PS) has complex c .

\therefore Transfer admittances

$$C_{YEQ} \neq C^* Y_{EQ}$$

$$y_{12} \neq y_{21}$$

Not Bilateral.

$[Y]$ not symm.
(about main diag.)