

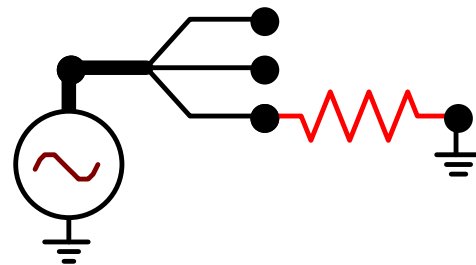
Topics for Today:

- Computer methods for time-domain transient simulation
 - ATP Simulation pointers 3-phase connections
 - Cap Bank Switching
 - ***ATP - how it works internally***
 - ***History of program development, versions available***
 - ***Rs, Ls, Cs***
 - ***Transmission lines***
 - ***System description as conductance matrix [G]***
 - ***Solution of [G] [V] = [I] when V's and I's are a mixture of knowns and unknowns.***

ATP Simulation Pointer for the day:

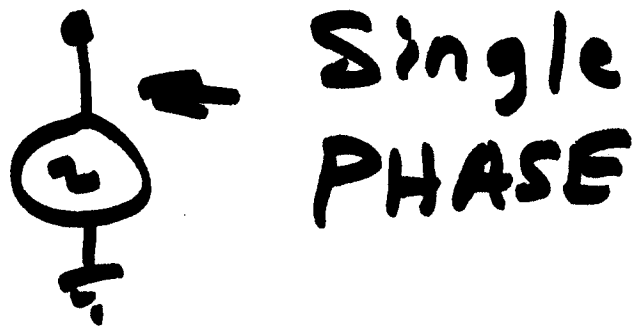
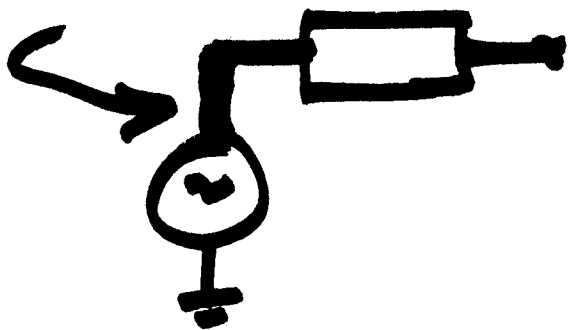
When building 3-phase circuits, you are actually drawing a one-line which represents the L-G per-phase equivalent of the system. Node names have a base name 5 characters long, with the 6th character A, B, C automatically added. Click on the 3-phase end of the splitter if you want to define the base node name.

If you need to make single-phase connection(s) to individual phases, use the splitter. When drawing a connecting line to a splitter, start at the node of the single-phase element and connect **to** the splitter. If you need to ground one phase, you can do that at the single phase element, but not at the splitter.

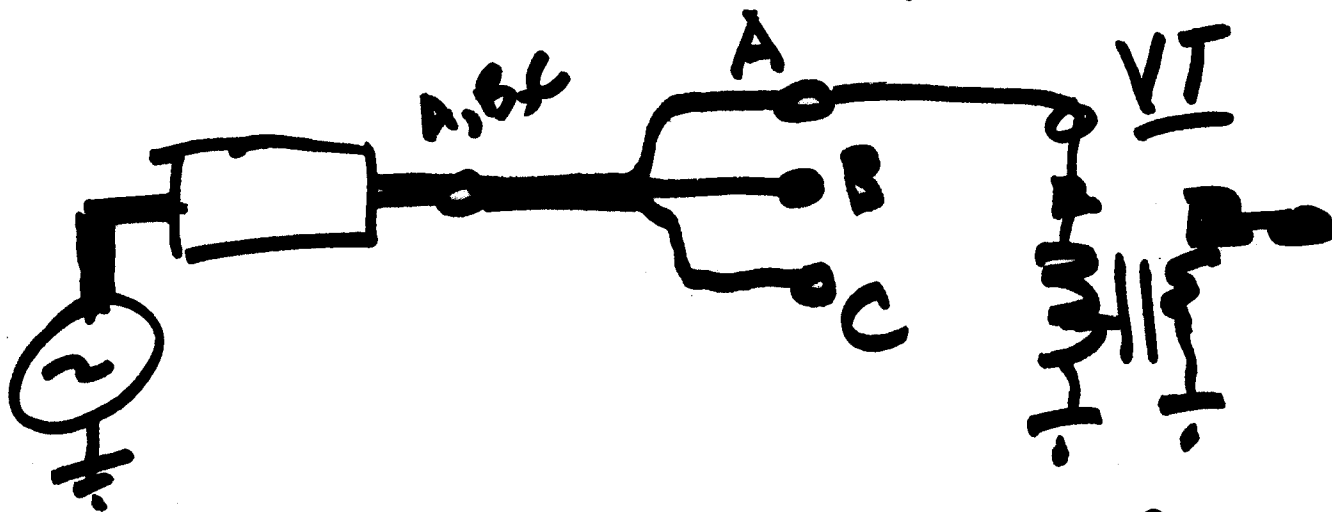


3-PHASE ELEMENTS

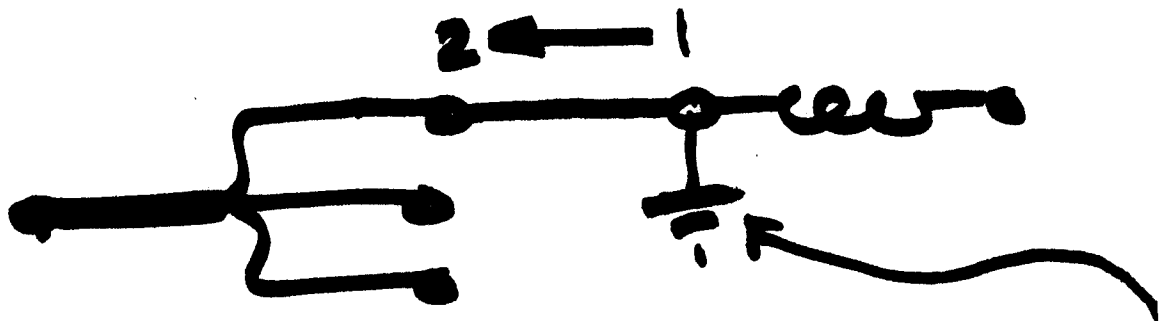
2



SPLITTER - 3ph \rightarrow 1ph



CONNECTING: Draw from 1 \rightarrow 2



Ground - Connect at 1 ϕ element

RS, L's & C's in EMTIP 3

Notes

EMTP - BPA, 1970 → '85

1985 EPRI ↓ DCG

EPRI EMTP
or DCG EMTP

- TACS ↓

EMTP/RV

F.O.I.

1987

ATP

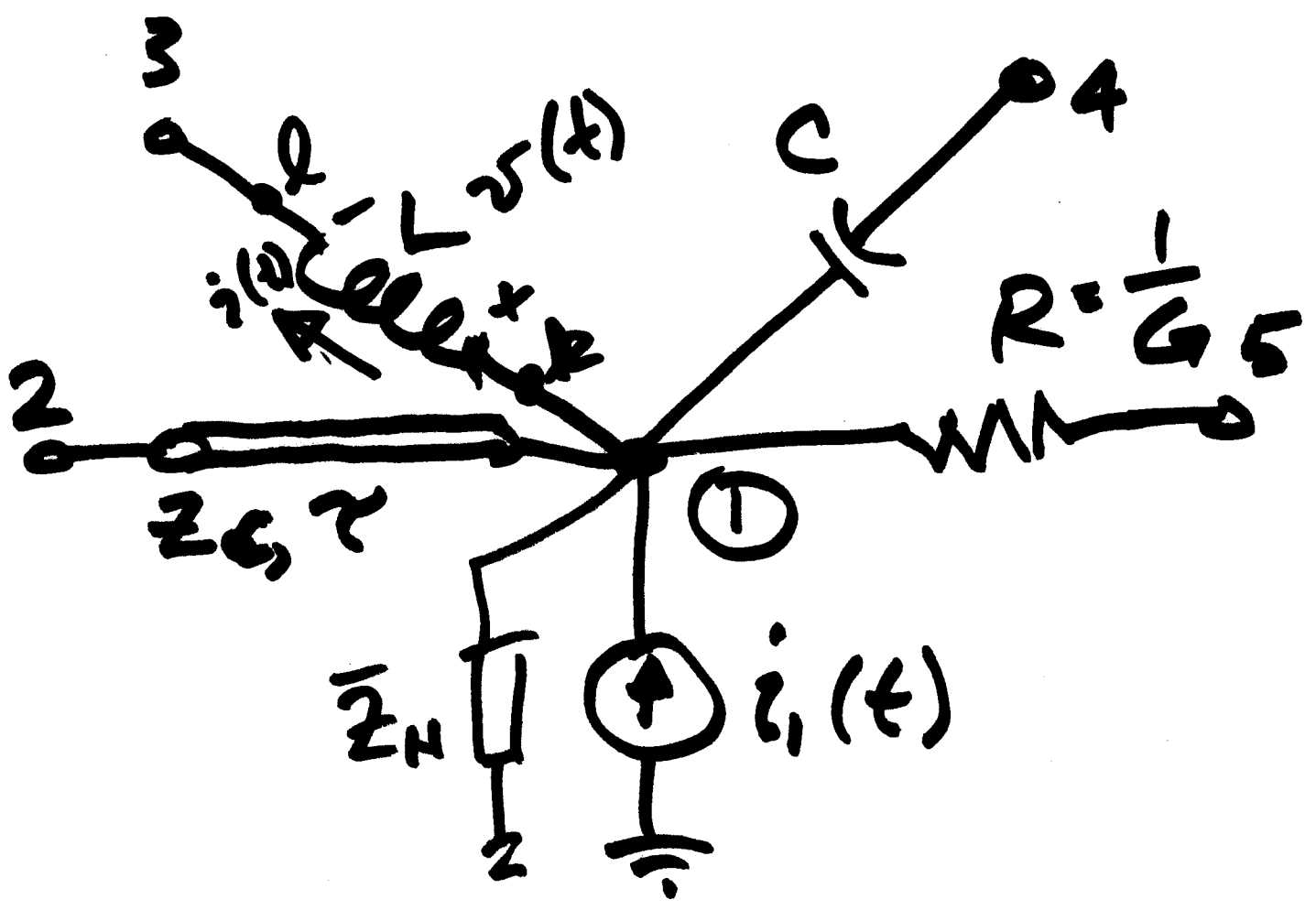
OTHERS:

- EMTDC/Pscad
- Micro-Tran ✓
- ABB/Siemens
- EDF - MORGAT

Different:

- TACS
- MODELS

Controls



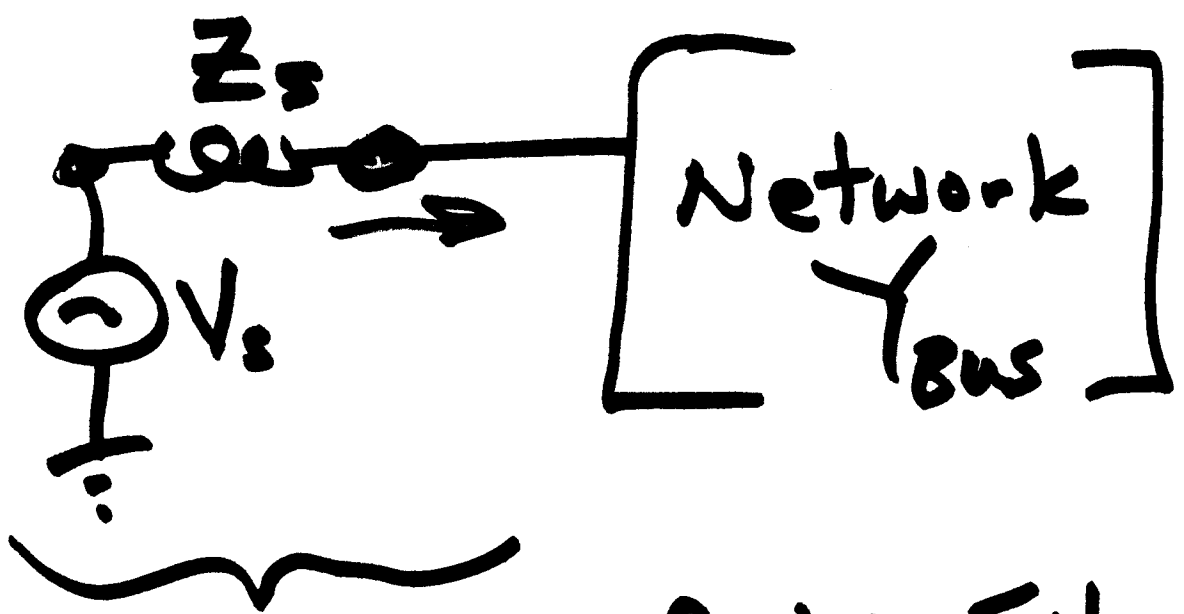
Side Note:

Mathematical Structure is

$$\text{Sparse} \rightarrow [Y][V] = [I]$$

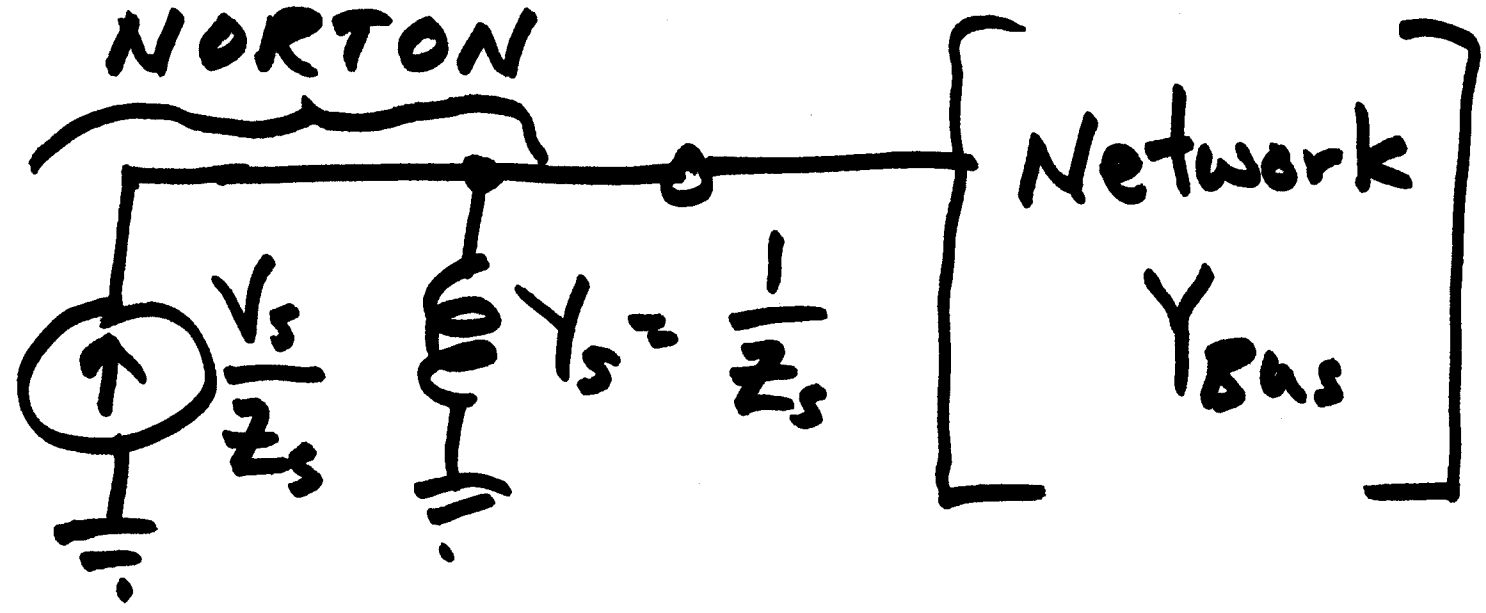
 ↑ node Vs ↑ injected currents

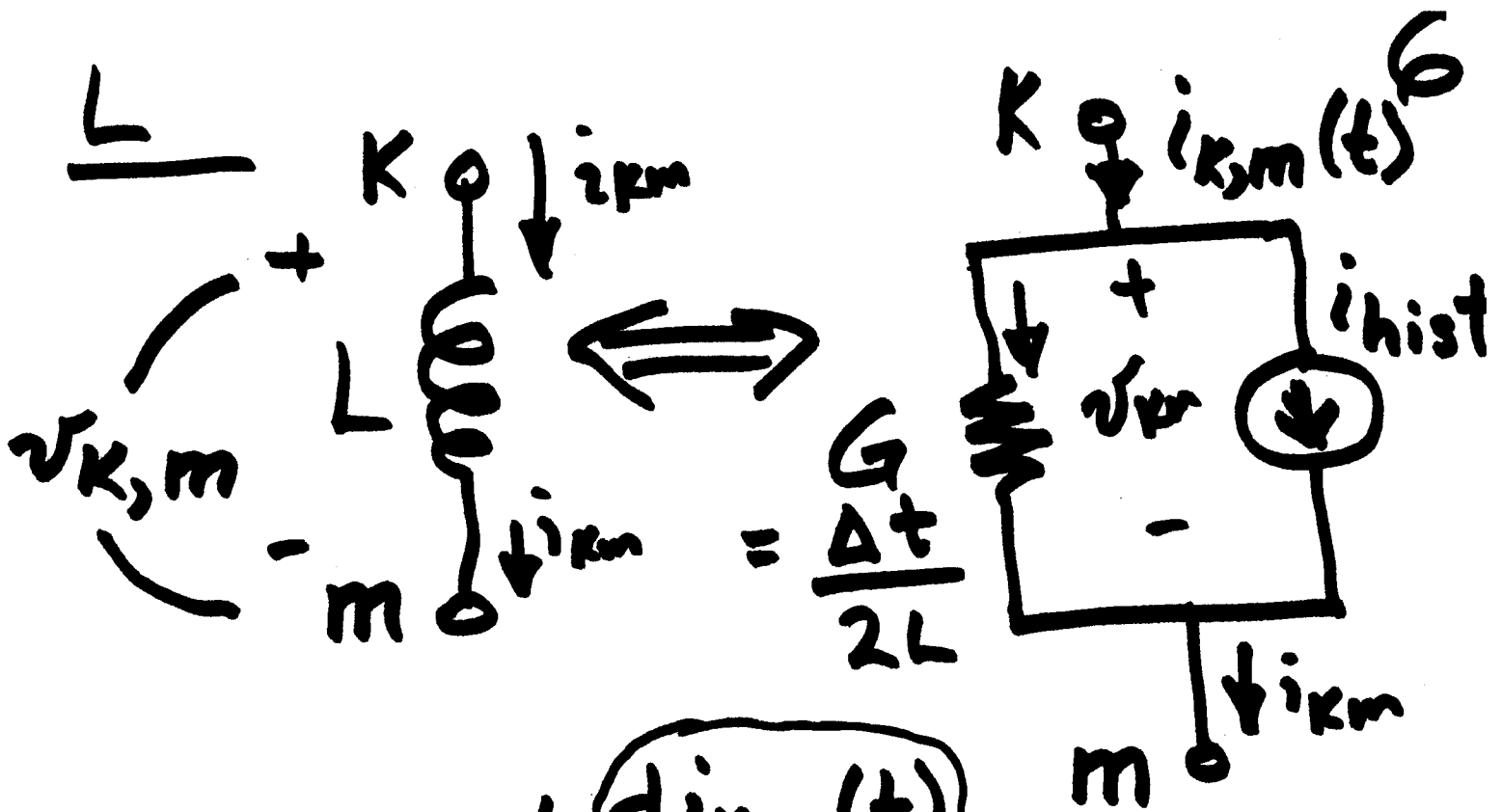
Injected Currents!



Thevenin = Bad: Extra Node
 $V = \text{Fixed}$

Instead, convert to Norton:
NORTON



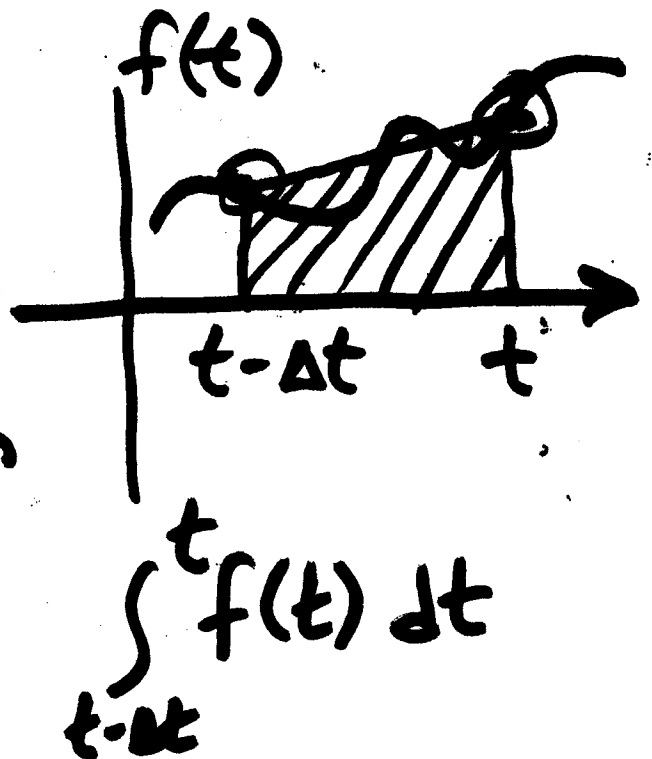


$$v_K - v_m = L \frac{di_{K,m}(t)}{dt}$$

$$di_{K,m}(t) \approx \left\{ i_{K,m}(t) - i_{K,m}(t - \Delta t) \right\} \Delta t$$

$$dt \approx \Delta t$$

Trapezoidal
Integration



$$i \downarrow \frac{d}{dt} v = L \frac{di}{dt}$$

$$v dt = L di$$

$$di = \frac{1}{L} v dt$$

$$i = \frac{1}{L} \int_0^t v dt$$

$$i = ?$$

Δt in EMTP

cannot be

as small as dt ,

Δt is finite.

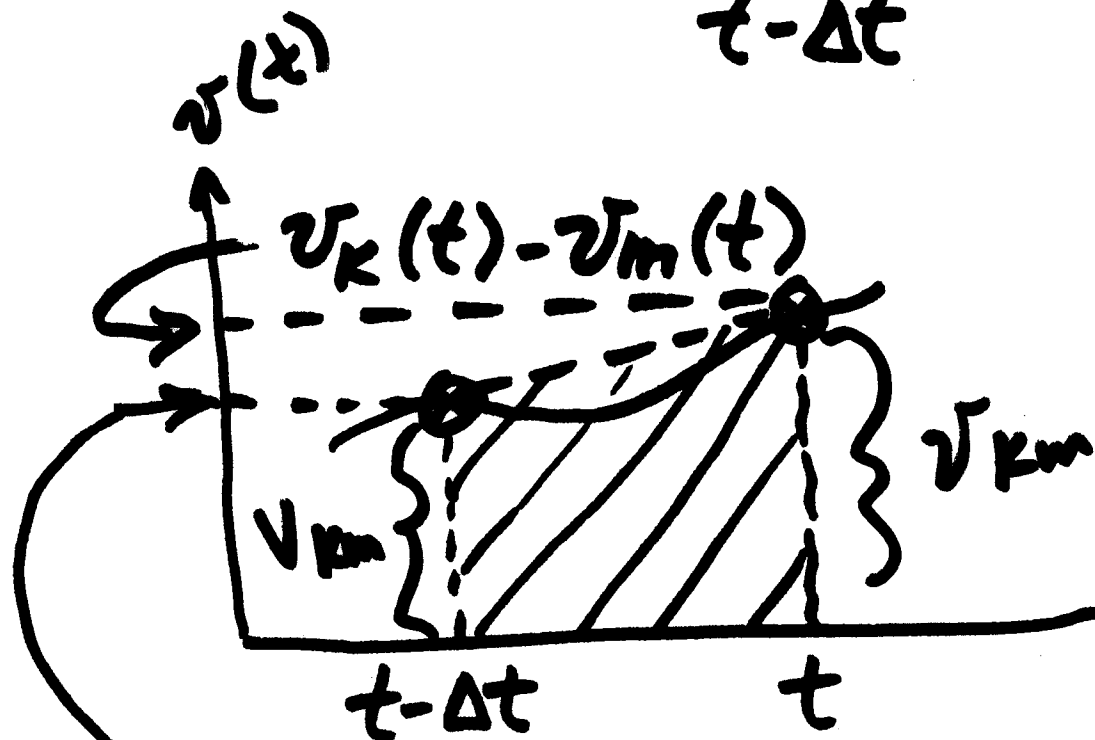
6A

Look at Trapezoidal
implementation of eqn:

~~GB~~
GB

$$v_k(t) - v_m(t) = L \frac{di_{k,m}(t)}{dt}$$

$$di_{k,m}(t) = \frac{1}{L} \int_{t-\Delta t}^t [v_k(t) - v_m(t)] dt$$



$$v_k(t - \Delta t) - v_m(t - \Delta t)$$

The integral can then be approximated as the area of the trapezoid:

7

$$\frac{1}{L} \int_{t-\Delta t}^t [v_k(t) - v_m(t)] dt$$

$$\approx \frac{\Delta t}{L} \left[\frac{v_k(t) - v_m(t) + v_k(t-\Delta t) - v_m(t-\Delta t)}{2} \right]$$

(i.e. area of trapezoid = $\Delta t \times$ average height of sides)

$$di_{Km}(t) = \frac{1}{L} \int_{t-\Delta t}^t [\sigma_r(t) - \sigma_m(t)] dt$$



$$\underline{\underline{i_{Km}(t) - i_{Km}(t-\Delta t)}}$$

Integral is:

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$$\frac{1}{L} \left[\begin{aligned} &v_k(t) - v_m(t) + v_k(t - \Delta t) \\ &- v_m(t - \Delta t) \end{aligned} \right] \frac{\Delta t}{2}$$

Putting pieces together,

$$i_{k,m}(t) \equiv i_{k,m}(t - \Delta t) + \frac{\Delta t}{2L} \left[\begin{aligned} &v_k(t) - v_m(t) + v_k(t - \Delta t) \\ &- v_m(t - \Delta t) \end{aligned} \right]$$

~~ok~~ ok

Separating (t) & $(t - \Delta t)$ terms,

$$i_{m,k}(t) \approx \left(\frac{\Delta t}{2L} \right) \left[v_k(t) - v_m(t) \right]$$

9
Current
at time = t
for present
voltage drop

$$+ i_{k,m}(t-\Delta t) + \frac{\Delta t}{2L} \left[v_k(t-\Delta t) - v_m(t-\Delta t) \right]$$

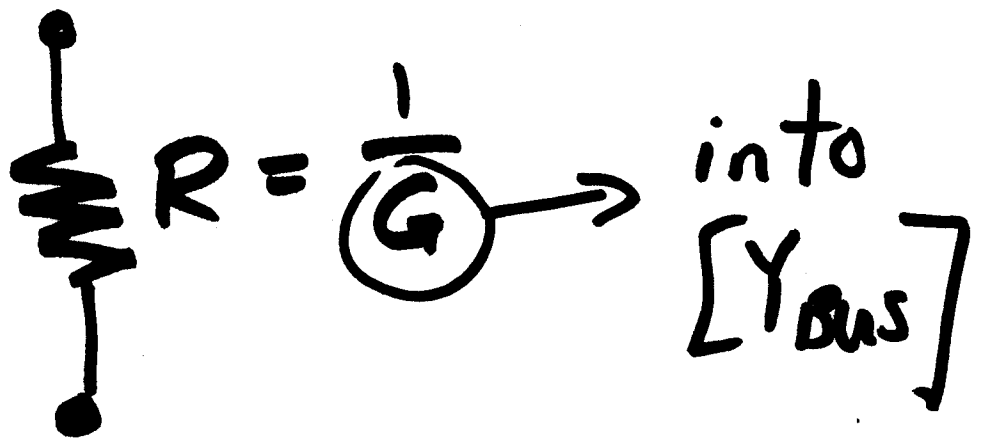
$I_{hist} = I_{k,m} =$ Summation of all currents
at past time steps. i.e.
 $t-\Delta t, t-2\Delta t, t-3\Delta t, \dots$

Initialization:

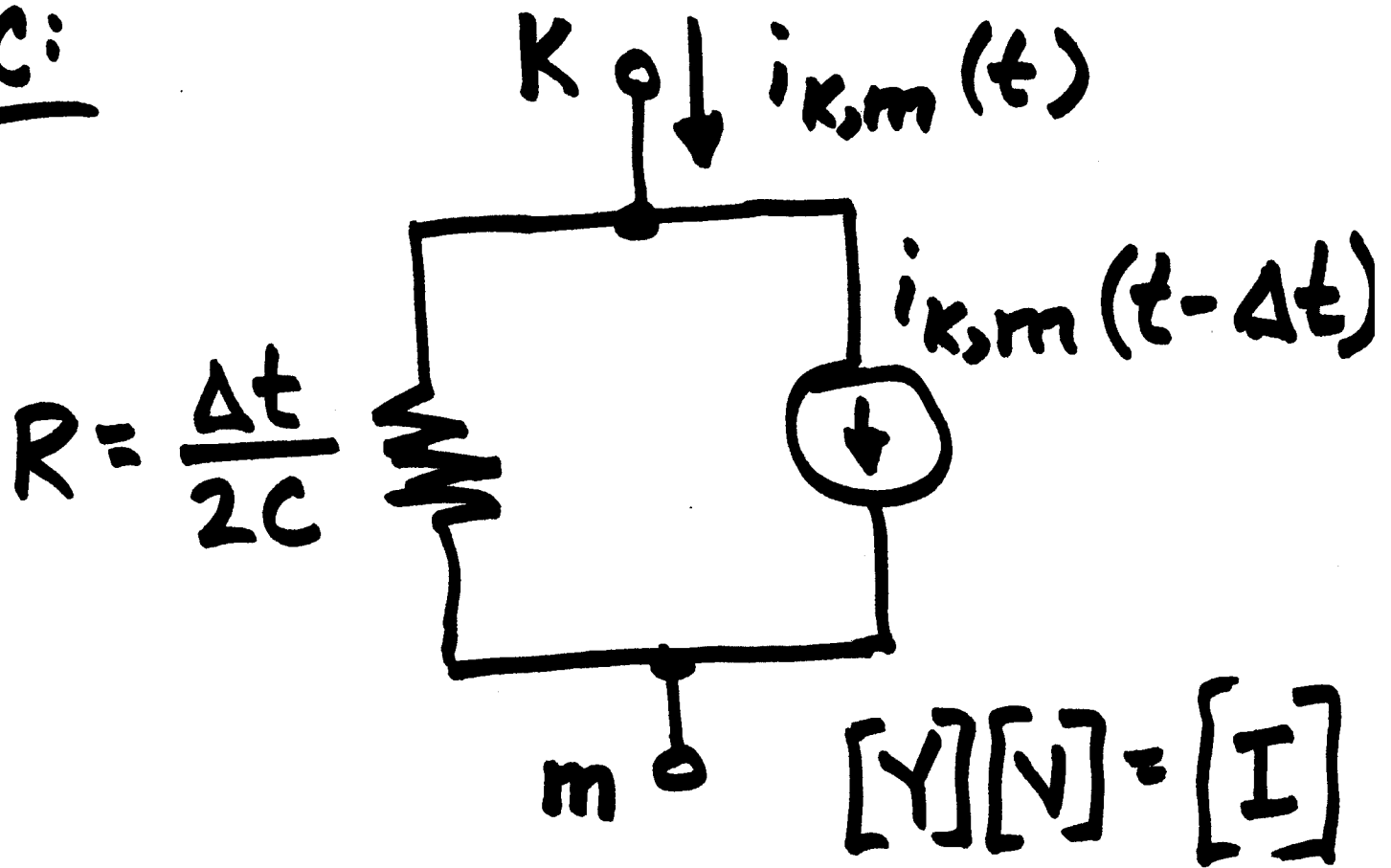
$$I_{hist}(0) = i(0).$$

$[Y_{bus}]$ is augmented ~~to~~ 10 according to system elements needed.

R:



C:



L_i

$K \circ b \ i_{k,m}(t)$

~~11~~
11

