

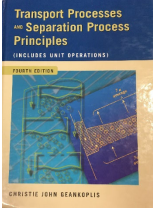


CM3110
Transport I
Part II: Heat Transfer



Michigan Tech





Professor Faith Morrison

Department of Chemical Engineering
 Michigan Technological University

These slides are incorporated into the slides from lectures 14-16, but are assembled here to tell the *heat-transfer resistance* story all together.

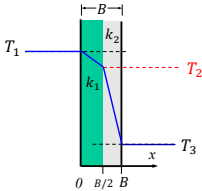
1

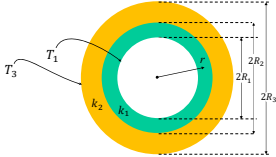
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Resistance Supplement

Thermal conductivity k and heat transfer coefficient h may be thought of as sources of resistance to heat transfer.

These resistances stack up in a logical way, allowing us to quickly and accurately determine the effect of adding insulating layers, encountering pipe fouling, and other applications.





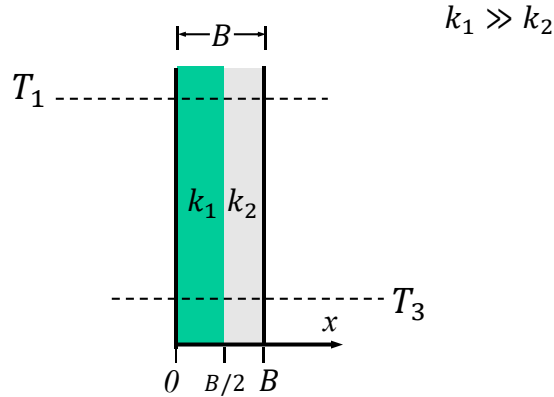
2

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Using the solution: Composite Door:

For an outside door, a metal is used (k_1) for strength, and a cork (k_2) is used for insulation. Both are the same thickness $B/2$. What is the temperature profile in the door at steady state? What is the flux? The inside temperature of the metal is T_1 and the outside temperature of the cork is T_3 .



Let's
try.

3

© Faith A. Morrison, Michigan Tech U.

Note: in the hand notes the temperatures from left to right are T_1, T_3, T_2 .

See handwritten notes.

https://pages.mtu.edu/~fmorriso/cm310/selected_lecture_slides.html

4

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Example 1b: Composite Door (two equal width layers)

SOLUTION:

$$\frac{q_x}{A} = \frac{(T_1 - T_3)}{\left(\frac{B}{2} \frac{(k_1 + k_2)}{k_1 k_2}\right)}$$

k_1 material: $(0 \leq x \leq B/2)$

$$T(x) = \frac{(T_2 - T_1)}{B/2} x + T_1$$

k_2 material: $(B/2 \leq x \leq B)$

$$T(x) = \frac{(T_3 - T_2)}{B/2} x + (2T_2 - T_3)$$

$$T_2 = \frac{k_1 T_1 + k_2 T_3}{k_1 + k_2}$$

5
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Example 1b: Composite Door (two equal width layers)

SOLUTION:

$$\frac{q_x}{A} = \frac{(T_1 - T_3)}{\frac{B/2}{k_1} + \frac{B/2}{k_2}}$$

Let: $\mathcal{R}_i \equiv \frac{\Delta x}{k_i}$

$$\frac{q_x}{A} = \frac{(T_1 - T_3)}{\mathcal{R}_1 + \mathcal{R}_2} = \frac{\text{driving force}}{\text{resistance}}$$

Each of the layers contributes a resistance, added in *series* (like in electricity).

6
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Example 2: Heat flux in a rectangular solid – Newton’s law of cooling BC

Assumptions:

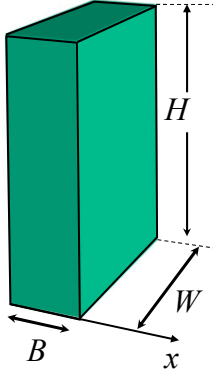
- wide, tall slab
- steady state
- h_1 and h_2 are the heat transfer coefficients of the left and right walls

What is the steady state temperature profile in a rectangular slab if the fluid on one side is held at T_{b1} and the fluid on the other side is held at T_{b2} ?

Bulk fluid temperature on left T_{b1}

Bulk fluid temperature on right T_{b2}

$T_{b1} > T_{b2}$



Newton's law of cooling boundary conditions

7

© Faith A. Morrison, Michigan Tech U.

**See handwritten notes
(in class, also on web).**

https://pages.mtu.edu/~fmorriso/cm310/selected_lecture_slides.html

https://pages.mtu.edu/~fmorriso/cm310/algebra_details_N_law_cooling.pdf

8

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Example 2: Heat flux in a rectangular solid – Newton’s law of cooling BC

Solution: (temp profile, flux)

Temperature profile:
(linear)

$$\frac{T_{b1} - T}{T_{b1} - T_{b2}} = \frac{\frac{x}{k} + \frac{1}{h_1}}{\left(\frac{1}{h_1} + \frac{B}{k} + \frac{1}{h_2}\right)}$$

Flux:
(constant)

$$\frac{q_x}{A} = \frac{T_{b1} - T_{b2}}{\frac{1}{h_1} + \frac{B}{k} + \frac{1}{h_2}}$$

Rectangular slab with Newton’s law of cooling BCs

9

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer

Example 2: Heat flux in a rectangular solid – Newton’s law of cooling BC

Solution: (temp profile, flux)

Temperature profile:
(linear)

$$\frac{T_{b1} - T}{T_{b1} - T_{b2}} = \frac{\frac{x}{k} + \frac{1}{h_1}}{\left(\frac{1}{h_1} + \frac{B}{k} + \frac{1}{h_2}\right)}$$

$$T = T_{b1} - \left(\frac{(T_{b1} - T_{b2})\frac{1}{k}}{\left(\frac{1}{h_1} + \frac{B}{k} + \frac{1}{h_2}\right)}\right)x + \left(\frac{(T_{b1} - T_{b2})\frac{1}{h_1}}{\left(\frac{1}{h_1} + \frac{B}{k} + \frac{1}{h_2}\right)}\right)$$

Resistance due to heat transfer at boundary

Resistance due to finite thermal conductivity

10

© Faith A. Morrison, Michigan Tech U.

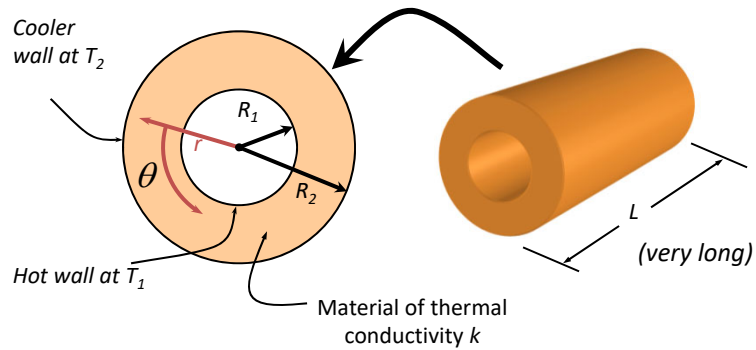
1D Heat Transfer – Radial

Example 3: Heat flux in a cylindrical shell – Temp BC

Assumptions:

- long pipe
- steady state
- k = thermal conductivity of wall

What is the steady state temperature profile in a cylindrical shell (pipe) if the **inner wall** is at T_1 and the **outer wall** is at T_2 ? ($T_1 > T_2$)



© Faith A. Morrison, Michigan Tech U. ¹¹

**See handwritten notes
in class.**

https://pages.mtu.edu/~fmorriso/cm310/selected_lecture_slides.html

© Faith A. Morrison, Michigan Tech U. ¹²

1D Heat Transfer – Radial

Example 3: Heat flux in a cylindrical shell – Temp BC

Solution for Cylindrical Shell:

NOT constant $\frac{q_r}{A} = \left(\frac{(T_1 - T_2)}{\frac{1}{k} \ln \frac{R_2}{R_1}} \right) \frac{1}{r}$

The heat flux $\frac{q_r}{A}$ **DOES** depend on k ;
also, $\frac{q_r}{A}$ decreases as $1/r$

NOT linear $\frac{T_2 - T}{T_2 - T_1} = \frac{\ln \frac{R_2}{r}}{\ln \frac{R_2}{R_1}}$

Note that $T(r)$ does not depend on the thermal conductivity, k (steady state)

Pipe with temperature BCs

© Faith A. Morrison, Michigan Tech U. ¹³

1D Heat Transfer – Radial

Example 3: Heat flux in a cylindrical shell – Temp BC

Solution for Cylindrical Shell:

NOT constant $\frac{q_r}{A} = \left(\frac{(T_1 - T_2)}{\frac{1}{k} \ln \frac{R_2}{R_1}} \right) \frac{1}{r}$

Let: $\mathcal{R}_i \equiv \frac{1}{k_i} \ln \frac{R_{i+1}}{R_i}$

$\frac{q_r}{A} = \left(\frac{(T_1 - T_2)}{\mathcal{R}_1} \right) \frac{1}{r} = \frac{\text{driving force}}{\text{resistance}}$

Resistance due to finite thermal conductivity, radial

© Faith A. Morrison, Michigan Tech U. ¹⁴

1D Radial Heat Transfer

Using the solution: Insulated Pipe (Composite, radial conduction)

For a metal pipe carrying a hot liquid (k_1) an insulation layer is added with thermal conductivity k_2 . What is the temperature profile in the composite pipe at steady state? What is the flux? The inside temperature of the metal pipe is T_1 and the outside temperature of the insulation is T_3 .

$k_1 \gg k_2$

15

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Radial

Example 3b: Insulated Pipe (Composite, radial conduction)

SOLUTION:

$$\frac{q_r}{A} = -k_i \left(\frac{dT}{dr} \right) = (\text{constant}) \frac{1}{r}$$

FLUX
NOT
constant

k_1 material: $(R_1 \leq r \leq R_2)$

$$T(r) = a_1 \ln r + b_1$$

$T(r)$
NOT
linear

k_2 material: $(R_2 \leq r \leq R_3)$

$$T(r) = a_2 \ln r + b_2$$

16

© Faith A. Morrison, Michigan Tech U.

See Lecture 16 Slides

https://pages.mtu.edu/~fmorriso/cm310/selected_lecture_slides.html

17

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Radial

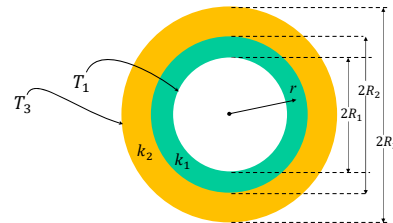
Example 3b: Insulated Pipe (Composite, radial conduction)

SOLUTION:

$$\frac{q_r}{A} = \left(\frac{(T_1 - T_3)}{\frac{1}{k_1} \ln \frac{R_2}{R_1} + \frac{1}{k_2} \ln \frac{R_3}{R_2}} \right) \frac{1}{r}$$

Let: $\mathcal{R}_i \equiv \frac{1}{k_i} \ln \frac{R_{i+1}}{R_i}$

$$\frac{q_r}{A} = \left(\frac{(T_1 - T_3)}{\mathcal{R}_1 + \mathcal{R}_2} \right) \frac{1}{r} = \frac{\text{driving force}}{\text{resistance}}$$



Note that we can continue to add layers in terms of resistance

Each of the layers contributes a resistance, added in series (like in electricity).

18

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Radial

Example 4: Heat flux in a cylindrical shell – Newton’s law of cooling

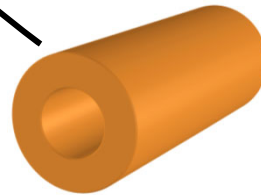
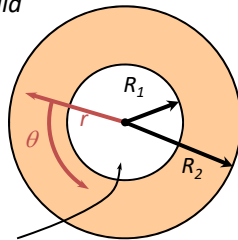
Assumptions:

- long pipe
- steady state
- k = thermal conductivity of wall
- h_1, h_2 = heat transfer coefficients

*What is the steady state temperature profile in a cylindrical shell (pipe) if the **fluid on the inside** is at T_{b1} and the **fluid on the outside** is at T_{b2} ? ($T_{b1} > T_{b2}$)*

Cooler fluid
at T_{b2}

Hot fluid at
 T_{b1}



© Faith A. Morrison, Michigan Tech U.

See handwritten notes.

https://pages.mtu.edu/~fmorriso/cm310/selected_lecture_slides.html

1D Heat Transfer – Radial

Example 4: Heat flux in a cylindrical shell

Newton's law of cooling boundary conditions

Solution: Radial Heat Flux in an Annulus

$T(r)$

$$T - T_{b2} = \frac{(T_{b1} - T_{b2}) \left(\ln \left(\frac{R_2}{r} \right) + \frac{k}{h_2 R_2} \right)}{\frac{k}{h_2 R_2} + \ln \left(\frac{R_2}{R_1} \right) + \frac{k}{h_1 R_1}}$$

$q_r(r)$

$$\frac{q_r}{A} = \frac{(T_{b1} - T_{b2})}{\frac{1}{h_2 R_2} + \frac{1}{k} \ln \left(\frac{R_2}{R_1} \right) + \frac{1}{h_1 R_1}} \left(\frac{1}{r} \right)$$

Resistance \mathcal{R} due to heat transfer coefficients, radial
Resistance \mathcal{R} due to finite thermal conductivity, radial

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Radial

Solution: Radial Heat Flux in an Annulus

$$\frac{q_r}{A} = \frac{(T_{b1} - T_{b2})}{\frac{1}{h_2 R_2} + \frac{1}{k} \ln \left(\frac{R_2}{R_1} \right) + \frac{1}{h_1 R_1}} \left(\frac{1}{r} \right)$$

Note that we can continue to add layers in terms of resistance

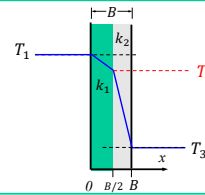
Resistance \mathcal{R} due to heat transfer coefficients, radial
Resistance \mathcal{R} due to finite thermal conductivity, radial

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer – Composite Structures

Let: $\mathcal{R}_i \equiv \frac{\Delta x}{k_i}$

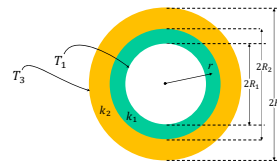
$$\frac{q_x}{A} = \frac{(T_1 - T_3)}{\mathcal{R}_1 + \mathcal{R}_2} = \frac{\text{driving force}}{\text{resistance}}$$



Note: Geankoplis uses a different resistance. For rectangular heat flux:
 $R_{\text{Geankoplis}} = \mathcal{R}/LW$

Let: $\mathcal{R}_i \equiv \frac{1}{k_i} \ln \frac{R_{i+1}}{R_i}$

$$\frac{q_r}{A} = \frac{(T_1 - T_3)}{\mathcal{R}_1 + \mathcal{R}_2} = \frac{\text{driving force}}{\text{resistance}}$$



Note: Geankoplis uses a different resistance. For radial heat flux:
 $R_{\text{Geankoplis}} = \mathcal{R}/2\pi L$

© Faith A. Morrison, Michigan Tech U. ²³

CM3110
Transport I
Part II: Heat Transfer

Michigan Tech

Heat Transfer Resistances
(Supplement)



Professor Faith Morrison
Department of Chemical Engineering
Michigan Technological University

These slides are incorporated into the slides from lectures 14-16, but are assembled here to tell the *heat-transfer resistance* story all together.

Back to regular thread



© Faith A. Morrison, Michigan Tech U. ²⁴