


CM3110

Transport Processes and Unit Operations I

Fluid Mechanics
Non-Newtonian fluids –
An Introduction

The *Weissenberg effect* is when a viscoelastic, non-Newtonian fluid will climb a rotating shaft.

<https://www.youtube.com/watch?v=npZzlgKjs0I>




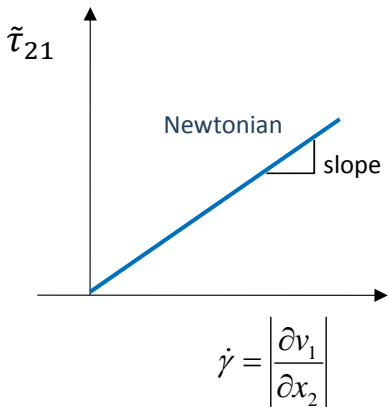


Photo by Carlos Arango Sabogal, U. Wisconsin, Madison

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Newtonian Fluids

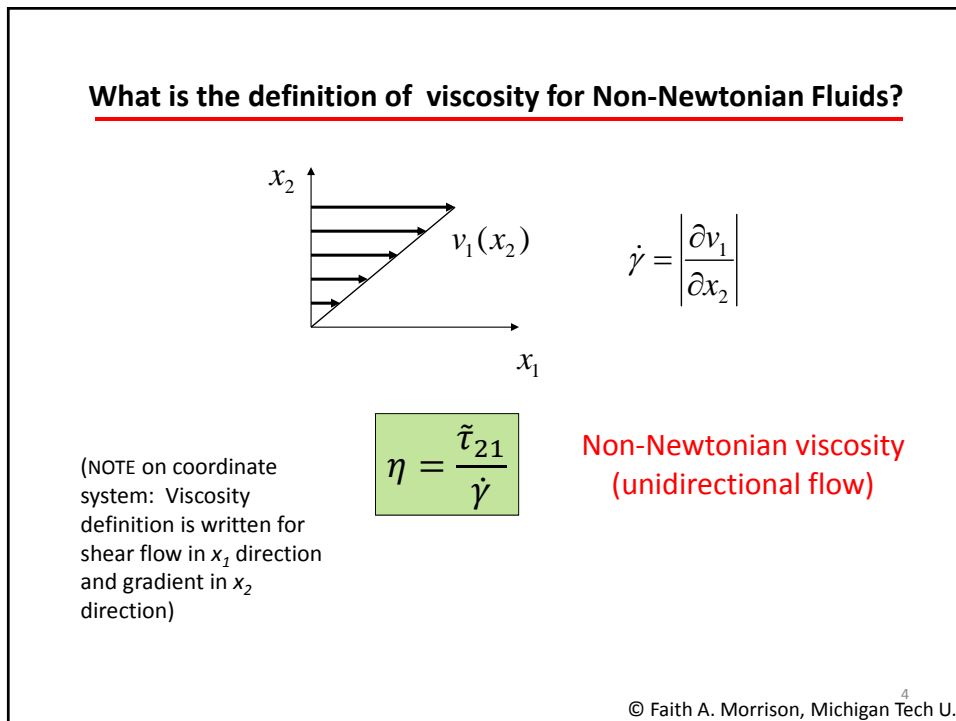
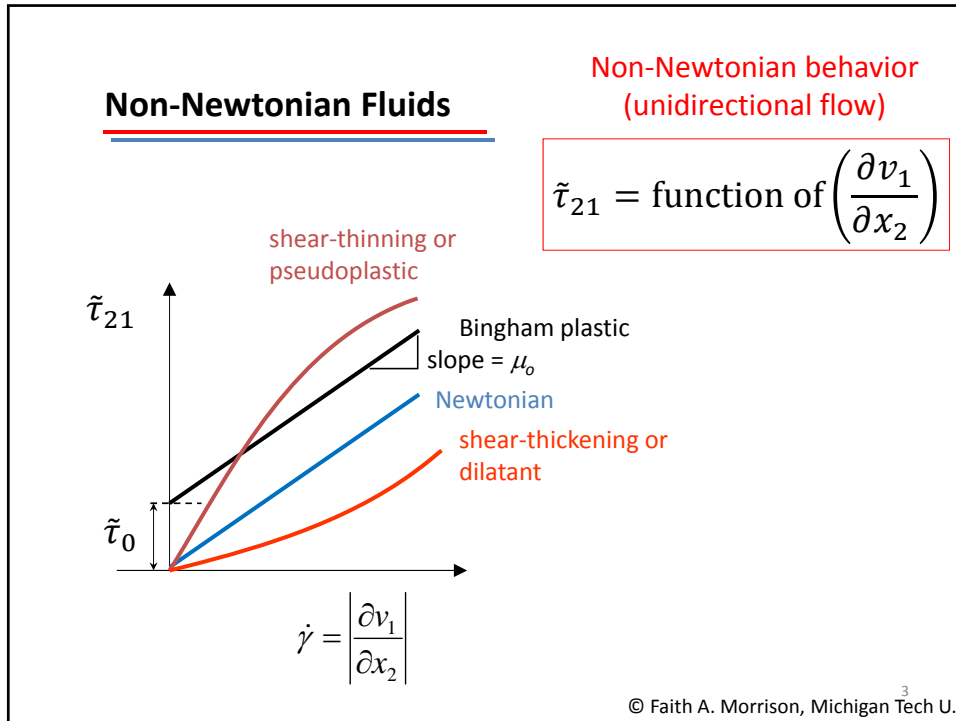


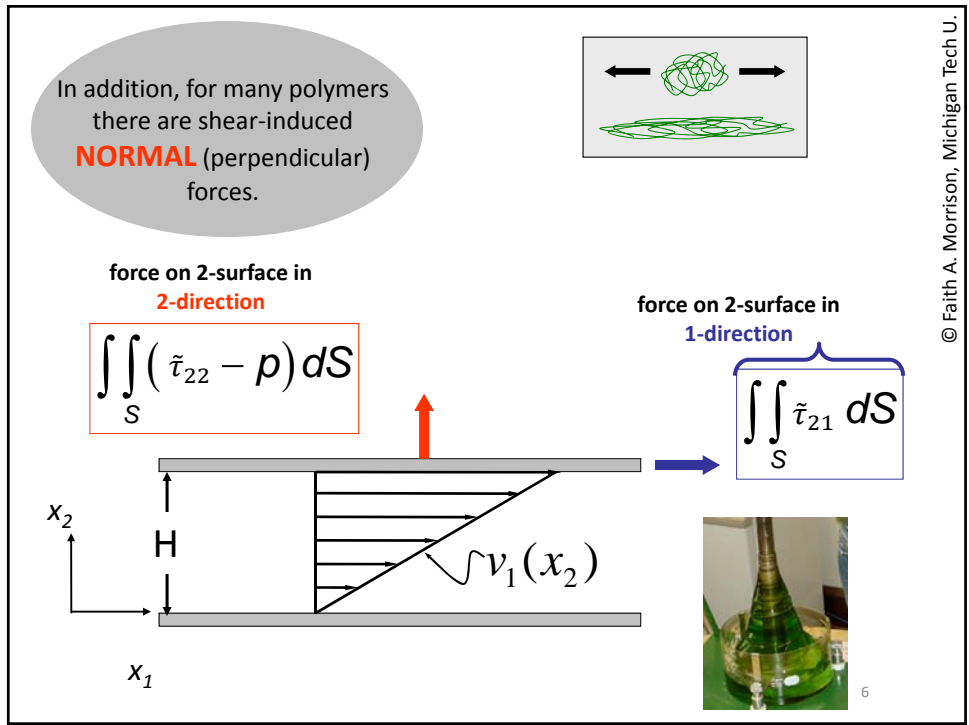
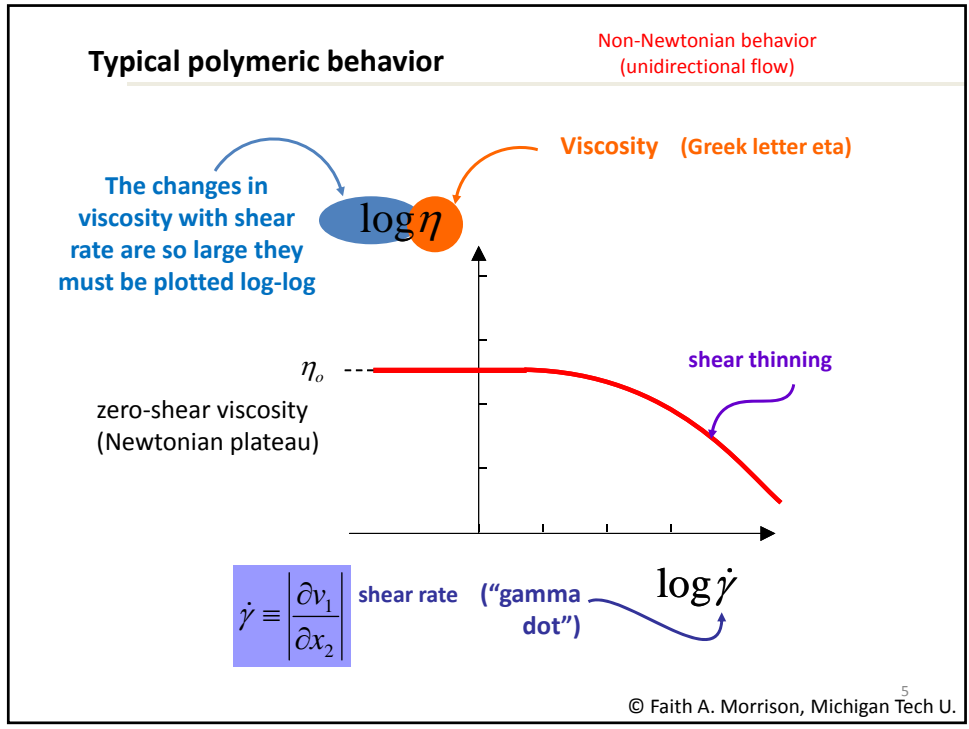
$\dot{\gamma} = \left| \frac{\partial v_1}{\partial x_2} \right|$

Newton's Law of Viscosity
 (unidirectional flow)

$$\tilde{\tau}_{21} = \mu \left(\frac{\partial v_1}{\partial x_2} \right)$$

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Non-Newtonian behavior
(unidirectional flow)

$\tilde{\tau}_{21} = \text{function of } \left(\frac{\partial v_1}{\partial x_2}\right)$

Power-Law Model

(does **not** model normal stresses)

$$\tilde{\tau}_{21} = m \left| \frac{dv_1}{dx_2} \right|^{n-1} \frac{dv_1}{dx_2}$$

m or K = consistency index ($m = \mu$ for Newtonian)
 n = power-law index ($n = 1$ for Newtonian)

$$\dot{\gamma} \equiv \left| \frac{\partial v_1}{\partial x_2} \right| = \text{shear rate}$$

7
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What does the power-law model predict for viscosity?

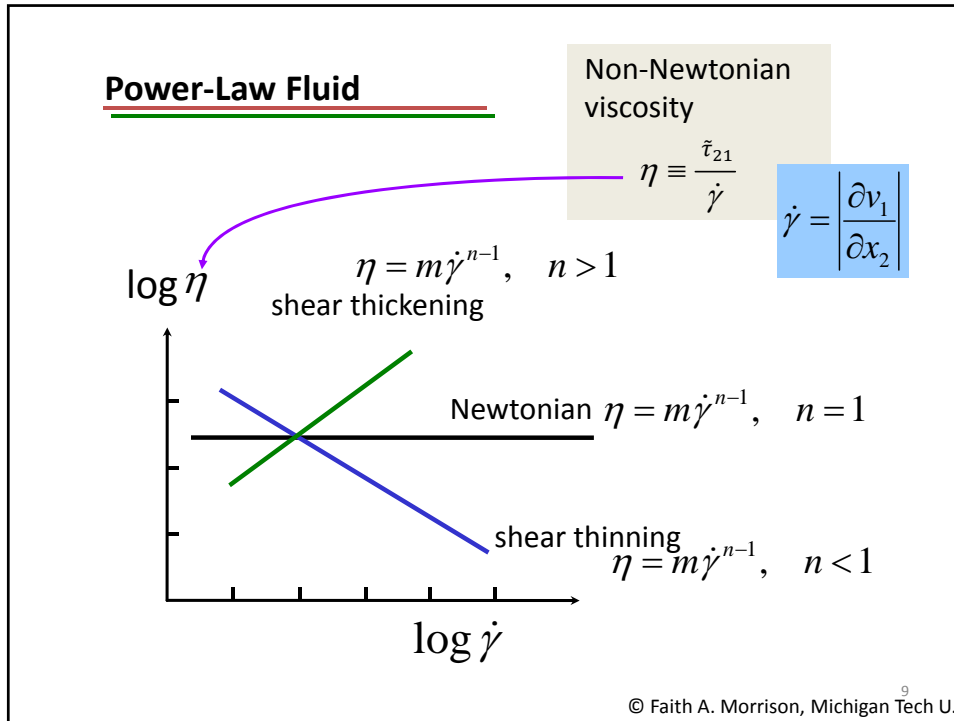
$$\tilde{\tau}_{21} = m \left| \frac{dv_1}{dx_2} \right|^{n-1} \frac{dv_1}{dx_2}$$

$$\eta \equiv \frac{\tilde{\tau}_{21}}{\dot{\gamma}} = \frac{\tilde{\tau}_{21}}{\left| \frac{dv_1}{dx_2} \right|} = m \left| \frac{dv_1}{dx_2} \right|^{n-1}$$

On a log-log plot, this would give a straight line:

$$\underbrace{\log \eta}_{Y} = \underbrace{\log m}_{B} + \underbrace{(n-1)}_{M} \underbrace{\log \left| \frac{dv_1}{dx_2} \right|}_{X}$$

8
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Where do we use the power-law expression?

The Equation of Continuity and the Equation of Motion in Cartesian, cylindrical, and spherical coordinates

Continuity Equation, Cartesian coordinates

$$\frac{\partial \rho}{\partial t} + \left(v_x \frac{\partial \rho}{\partial x} + v_y \frac{\partial \rho}{\partial y} + v_z \frac{\partial \rho}{\partial z} \right) + \rho \left(\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \right) = 0$$

Continuity Equation, cylindrical coordinates

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial(\rho r v_r)}{\partial r} + \frac{1}{r} \frac{\partial(\rho v_\theta)}{\partial \theta} + \frac{\partial(\rho v_z)}{\partial z} = 0$$

$$\frac{\partial \rho}{\partial t} + \underline{v} \cdot \nabla \rho = -\rho(\nabla \cdot \underline{v})$$

Continuity Equation, spherical coordinates

$$\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial(\rho r^2 v_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial(\rho v_\theta \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial(\rho v_\phi)}{\partial \phi} = 0$$

Equation of Motion for an incompressible fluid, 3 components in Cartesian coordinates

$$\begin{aligned} \rho \left(\frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_z \frac{\partial v_x}{\partial z} \right) &= -\frac{\partial P}{\partial x} + \left(\frac{\partial \tilde{\tau}_{xx}}{\partial x} + \frac{\partial \tilde{\tau}_{yx}}{\partial y} + \frac{\partial \tilde{\tau}_{zx}}{\partial z} \right) + \rho g_x \\ \rho \left(\frac{\partial v_y}{\partial t} + v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_z \frac{\partial v_y}{\partial z} \right) &= -\frac{\partial P}{\partial y} + \left(\frac{\partial \tilde{\tau}_{xy}}{\partial x} + \frac{\partial \tilde{\tau}_{yy}}{\partial y} + \frac{\partial \tilde{\tau}_{zy}}{\partial z} \right) + \rho g_y \\ \rho \left(\frac{\partial v_z}{\partial t} + v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \right) &= -\frac{\partial P}{\partial z} + \left(\frac{\partial \tilde{\tau}_{xz}}{\partial x} + \frac{\partial \tilde{\tau}_{yz}}{\partial y} + \frac{\partial \tilde{\tau}_{zz}}{\partial z} \right) + \rho g_z \end{aligned}$$

The one with "τ" is for non-Newtonian fluids

Where do we use the power-law expression?

e.g., Poiseuille flow in a tube:

Newtonian $\tilde{\tau}_{rz} = \mu \left(\frac{dv_z}{dr} \right)$

non-Newtonian, power-law $\tilde{\tau}_{rz} = m \left| \frac{dv_z}{dr} \right|^{n-1} \frac{dv_z}{dr}$

$\tilde{\tau}_{rz} = \left(\frac{L\rho g + (P_o - P_L)}{2L} \right) r$

\Rightarrow solve for $v_z(r)$

1-direction = r
2-direction = z

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EXAMPLE III: Pressure-driven flow of a Power-law fluid in a tube

- steady state
- incompressible
- well developed
- long tube

Calculate velocity and stress profiles

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Calculate the velocity field for
Pressure-driven flow of a power-
law (PL) fluid:

Non-Newtonian behavior
(unidirectional flow)

$$\tilde{\tau}_{21} = \text{PL function of } \left(\frac{\partial v_1}{\partial x_2} \right)$$

$$\begin{aligned} \tilde{\tau}_{rz} &= m \underbrace{\left| \frac{dv_z}{dr} \right|^{n-1}}_{\text{red bracket}} \underbrace{\frac{dv_z}{dr}}_{\text{purple bracket}} = \left(\frac{L\rho g + (P_o - P_L)}{2L} \right) r \\ &= - \frac{\partial v_z}{\partial r} \quad \forall r \quad \equiv \alpha \end{aligned}$$

$$m \left(- \frac{dv_z}{dr} \right)^{n-1} \frac{dv_z}{dr} = - m \left(- \frac{dv_z}{dr} \right)^n = \alpha r$$

Solve for $v_z(r)$

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Boundary Conditions:

?

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Non-Newtonian behavior
(unidirectional flow)

$\tilde{\tau}_{21} = \text{PL function of } \left(\frac{\partial v_1}{\partial x_2}\right)$

Velocity field
Poiseuille flow of a power-law fluid:

$$v_z(r) = \left(\frac{R(L\rho g + P_o - P_L)}{2Lm}\right)^{\frac{1}{n}} \left(\frac{R}{\frac{1}{n} + 1}\right) \left(1 - \left(\frac{r}{R}\right)^{\frac{1}{n} + 1}\right)$$

$$\langle v \rangle = \frac{1}{\pi R^2} \int_0^{2\pi} \int_0^R v_z(r) r dr d\theta = R \left(\frac{n}{1 + 3n}\right) \left[\frac{R(P_o - P_L)}{2mL}\right]^{\frac{1}{n}}$$

15
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Non-Newtonian behavior
(unidirectional flow)

$\tilde{\tau}_{21} = \text{PL function of } \left(\frac{\partial v_1}{\partial x_2}\right)$

Solution to Poiseuille flow in a tube
incompressible, power-law fluid

16
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Non-Newtonian behavior (all flows)

$$\tilde{\tau}_{21} = \text{nonlinear function of } \nabla v$$

Rheology (Non-Newtonian Fluid Mechanics)

Rheology affects:



•End use (food texture, product pour, motor-oil function)

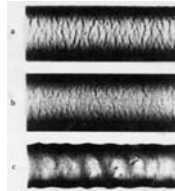
•Processing (design, costs, production rates)



www.corrugatorman.com/pic/akron%20extruder.JPG



www.math.utwente.nl/mpcm/aamp/examples.html



•Product quality (surface distortions, anisotropy, strength, structure development)

Pomar et al. JNNFM
54 143 1994

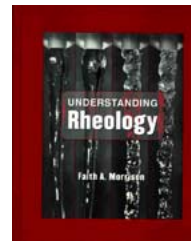
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Rheology (Non-Newtonian Fluid Mechanics)

At Michigan Tech:

CM4650 Polymer Rheology (Even years spring, MW 4-5:20pm)
www.chem.mtu.edu/~fmorriso/cm4650/cm4650.html

CM4655 Polymer Rheology Lab (Fall, when possible)
www.chem.mtu.edu/~fmorriso/cm4655/cm4655.html



18
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Next:

A thumbnail of a presentation slide. At the top left, it reads 'CM3110 Transport I Part I: Fluid Mechanics'. At the top right is the Michigan Tech logo. In the center, a yellow oval contains the text 'More Complicated Flows' followed by '(Dimensional Analysis, rough pipes, hydraulic diameter, porous media)'. To the right of the oval is a photograph of a person in a white protective suit and mask working in a pool of water. Below the oval, it says 'Professor Faith Morrison, Department of Chemical Engineering, Michigan Technological University'. At the bottom right, there is a small number '1' and the text '© Faith A. Morrison, Michigan Tech U.'.



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