
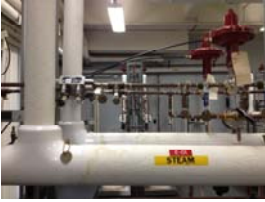
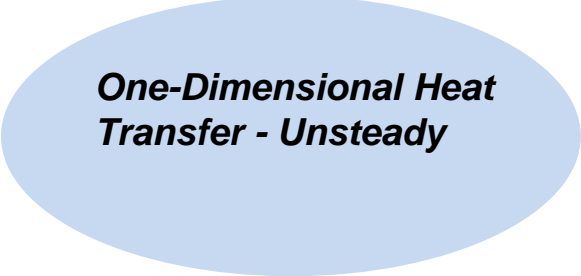


CM3110
Transport I
Part II: Heat Transfer



Michigan Tech






One-Dimensional Heat Transfer - Unsteady


Professor Faith Morrison


Department of Chemical Engineering
 Michigan Technological University

© Faith A. Morrison, Michigan Tech U. ¹

CM3110
 Transport I
 Part II: Heat Transfer







One-Dimensional Heat Transfer
(part 2: cylindrical shell)

Professor Faith Morrison
 Department of Chemical Engineering
 Michigan Technological University

SUMMARY

Steady State Heat Transfer

Example 1: Heat flux in a rectangular solid – Temperature BC

Example 2: Heat flux in a rectangular solid – Newton’s law of cooling

Example 3: Heat flux in a cylindrical shell – Temperature BC

Example 4: Heat flux in a cylindrical shell – Newton’s law of cooling



Example 5: Heat conduction with generation

Example 6: Wall heating of laminar flow

Conclusion: When we can simplify geometry, assume steady state, assume symmetry, the solutions are easily obtained

© Faith A. Morrison, Michigan Tech U. ²

CM3110
Transport I
Part II: Heat Transfer

One-Dimensional Heat Transfer
(part 2: cylindrical shell)

Professor Faith Morrison
Department of Chemical Engineering
Michigan Technological University

SUMMARY

Steady State Heat Transfer

Example 1: Heat flux in a rectangular solid – Temperature BC

Example 2: Heat flux in a rectangular solid – Newton’s law of cooling

Example 3: Heat flux in a cylindrical shell – Temperature BC

Example 4: Heat flux in a cylindrical shell – Newton’s law of cooling

Example 5: Heat conduction with generation

Example 6: Wall heating of laminar flow

Conclusion: When we can simplify geometry, assume steady state, assume symmetry, the solutions are easily obtained

What about non-steady-state problems (quite common in heat transfer)?

© Faith A. Morrison, Michigan Tech U. ³

1D Heat Transfer: Unsteady State

Example 1: Unsteady Heat Conduction in a Semi-infinite solid

A very long, very wide, very tall slab is initially at a temperature T_0 . At time $t = 0$, the left face of the slab is exposed to an environment at temperature T_1 . What is the time-dependent temperature profile in the slab? The slab is a homogeneous material of thermal conductivity, k , density, ρ , and heat capacity, C_p .

© Faith A. Morrison, Michigan Tech U. ⁴

1D Heat Transfer: Unsteady State

Example 1: Unsteady Heat Conduction in a Semi-infinite solid

A very long, very wide, very tall slab is initially at a temperature T_0 . At time $t = 0$, the left face of the slab is **exposed to an environment** at temperature T_1 . What is the time-dependent temperature profile in the slab? The slab is a homogeneous material of thermal conductivity, k , density, ρ , and heat capacity, C_p .

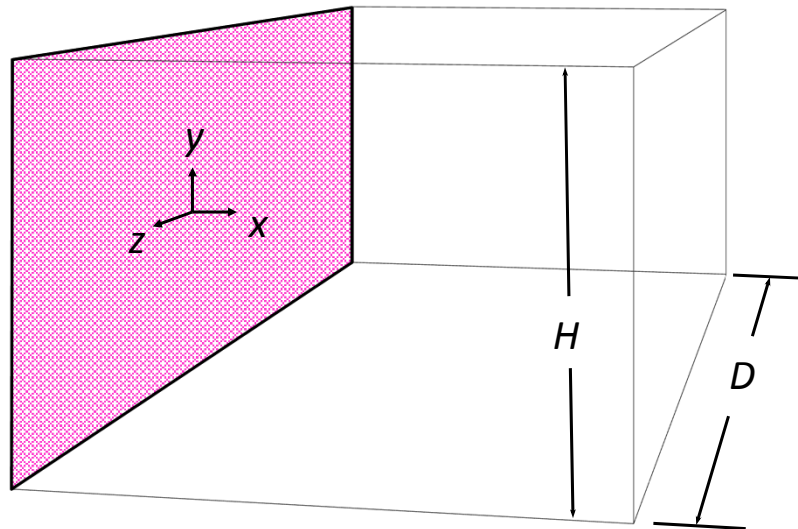
This is code for:

“Newton’s law of cooling boundary conditions:”
 $|\text{flux}| = h|T_{\text{bulk}} - T_{\text{wall}}|$

© Faith A. Morrison, Michigan Tech U.

Unsteady State Heat Transfer

Example: Unsteady Heat Conduction in a Semi-infinite solid



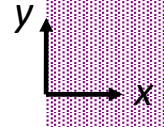
H, D, very large

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

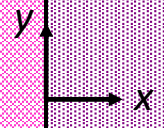
Initial Condition:

$t < 0$
 $T = T_o$



$t < 0$
 $T = T_o$

$t \geq 0$
 $T = T_1$



$t > 0$
 $T = T(x, t)$

© Faith A. Morrison, Michigan Tech U. ⁷

1D Heat Transfer: Unsteady State

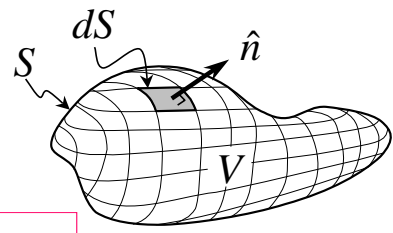
General Energy Transport Equation

(microscopic energy balance)

As for the derivation of the microscopic momentum balance, the microscopic energy balance is derived on an arbitrary volume, V , enclosed by a surface, S .

Gibbs notation:

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S$$



see handout for component notation

© Faith A. Morrison, Michigan Tech U. ⁸

1D Heat Transfer: Unsteady State

General Energy Transport Equation

(microscopic energy balance)

$$\rho \hat{C}_p \left(\underbrace{\frac{\partial T}{\partial t}}_{\text{rate of change}} + \underbrace{v \cdot \nabla T}_{\text{convection}} \right) = \underbrace{k \nabla^2 T}_{\text{conduction (all directions)}} + \underbrace{S}_{\text{source (energy generated per unit volume per time)}}$$

velocity must satisfy equation of motion, equation of continuity

see handout for component notation

© Faith A. Morrison, Michigan Tech U.

Equation of energy

for Newtonian fluids of constant density, ρ , and thermal conductivity, k , with source term (source could be viscous dissipation, electrical energy, chemical energy, etc., with units of energy/(volume time)).

CM310 Fall 1999 Faith Morrison

Source: R. B. Bird, W. E. Stewart, and E. N. Lightfoot, *Transport Processes*, Wiley, NY, 1960, page 319.

Gibbs notation (vector notation)

$$\left(\frac{\partial T}{\partial t} + v \cdot \nabla T \right) = \frac{k}{\rho \hat{C}_p} \nabla^2 T + \frac{S}{\rho \hat{C}_p}$$

Cartesian (xyz) coordinates:

$$\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

Cylindrical (r θ z) coordinates:

$$\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

Spherical (r θ ϕ) coordinates:

$$\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi} = \frac{k}{\rho \hat{C}_p} \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + \frac{S}{\rho \hat{C}_p}$$

© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

Example 1: Unsteady Heat Conduction in a Semi-infinite solid

A very long, very wide, very tall slab is initially at a temperature T_0 . At time $t = 0$, the left face of the slab is exposed to an environment at temperature T_1 . What is the time-dependent temperature profile in the slab? The slab is a homogeneous material of thermal conductivity, k , density, ρ , and heat capacity, C_p .

Newton's law of cooling BC's:

$$|q_x| = hA |T_{bulk} - T_{surface}|$$

© Faith A. Morrison, Michigan Tech U. ¹¹

1D Heat Transfer: Unsteady State

Microscopic Energy Equation in Cartesian Coordinates

$$\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

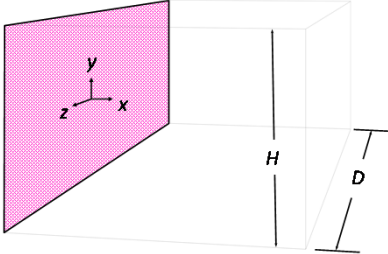
$$\alpha \equiv \frac{k}{\rho \hat{C}_p} = \text{thermal diffusivity}$$

what are the boundary conditions? initial conditions?



© Faith A. Morrison, Michigan Tech U. ¹²

1D Heat Transfer: Unsteady State

Example 7: Unsteady Heat Conduction in a Semi-infinite solid





Initial Condition:

$t < 0$ $T = T_o$		$t < 0$ $T = T_o$
$t \geq 0$ $T = T_1$		$t > 0$ $T = T(x, t)$

You try.

© Faith A. Morrison, Michigan Tech U. ¹³

1D Heat Transfer: Unsteady State

$t < 0$ $T = T_o$		$t < 0$ $T = T_o$
$t \geq 0$ $T = T_1$		$t > 0$ $T = T(x, t)$

Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} \right) = \alpha \left(\frac{\partial^2 T}{\partial x^2} \right)$$

Initial condition: $t = 0, T = T_o \quad \forall x$

Boundary conditions:

$$x = 0, \quad q_x = hA(T - T_1) \quad \forall t > 0$$

$$x = \infty, \quad T = T_o \quad \forall t$$

© Faith A. Morrison, Michigan Tech U. ¹⁴

1D Heat Transfer: Unsteady State

Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} \right) = \alpha \left(\frac{\partial^2 T}{\partial x^2} \right)$$

Initial condition: $t = 0, T = T_o \forall x$

Boundary conditions:

$$x = 0, q_x = hA(T - T_1) \quad \forall t > 0$$

$$x = \infty, T = T_o \quad \forall t \text{ "for all t"}$$

15
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} \right) = \alpha \left(\frac{\partial^2 T}{\partial x^2} \right)$$

Initial condition: $t = 0, T = T_o \forall x$

Boundary conditions:

$$x = 0, q_x = hA(T - T_1) \quad \forall t > 0$$

$$x = \infty, T = T_o \quad \forall t$$

The solution is obtained by combination of variables.

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k} \quad \zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

16
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

Unsteady State Heat Conduction in a Semi-Infinite Slab

Solution:

$$\frac{T - T_0}{T_1 - T_0} = \text{erfc } \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k} \quad \zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

Geankoplis 4th ed., eqn 5.3-7, page 363

complementary error function of y $\text{erfc}(y) \equiv 1 - \text{erf}(y)$

error function of y $\text{erf}(y) \equiv \frac{2}{\sqrt{\pi}} \int_0^y e^{-(y')^2} dy'$

17
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

Solution:

$$\frac{T - T_0}{T_1 - T_0} = \text{erfc } \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k} \quad \zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

Geankoplis 4th ed., eqn 5.3-7, page 363

complementary error function of y $\text{erfc}(y) \equiv 1 - \text{erf}(y)$

error function of y $\text{erf}(y) \equiv \frac{2}{\sqrt{\pi}} \int_0^y e^{-(y')^2} dy'$

To make this solution easier to use, we can plot it.

18
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

This:

$$\frac{T - T_0}{T_1 - T_0} = \operatorname{erfc} \zeta - e^{\beta(2\zeta + \beta)} \operatorname{erfc}(\zeta + \beta)$$

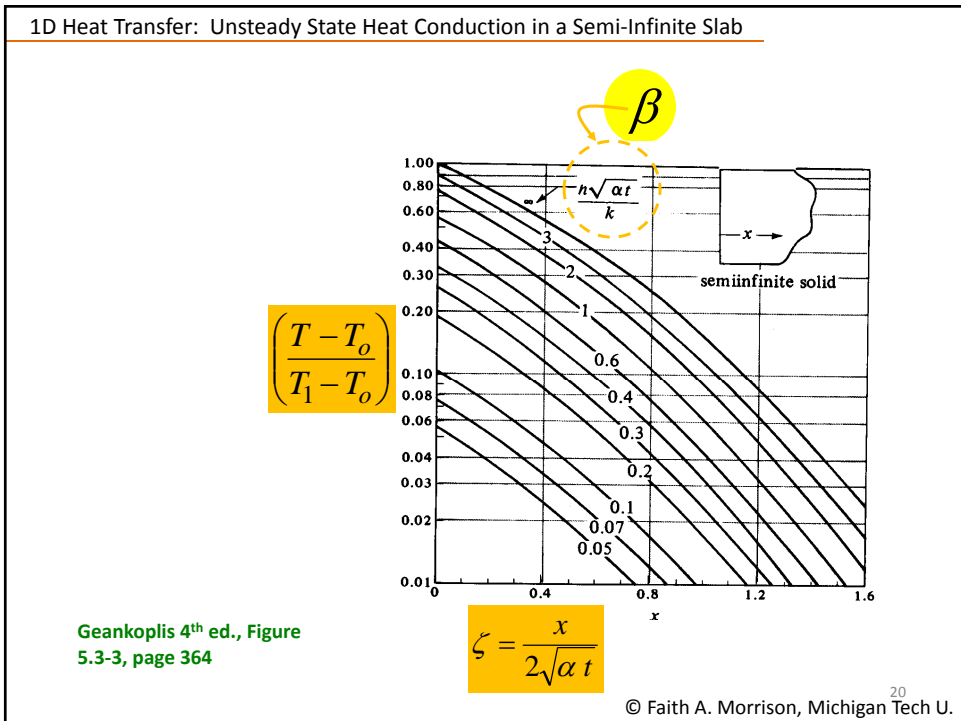
Versus this: $\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$

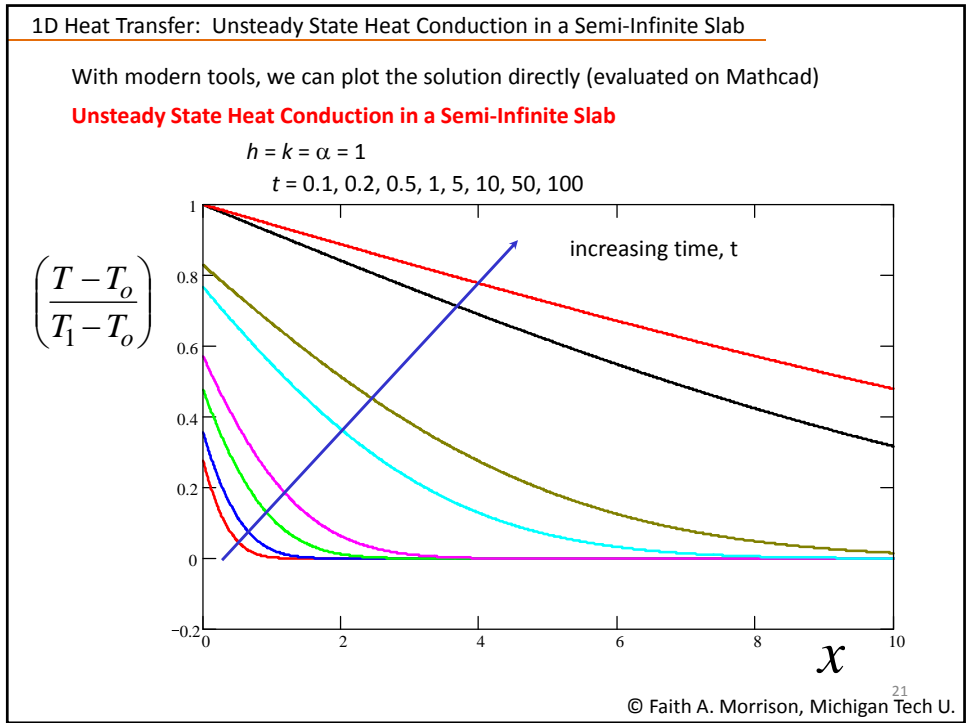
At various values of this:

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

To make this solution easier to use, we can plot it.

© Faith A. Morrison, Michigan Tech U. ¹⁹





1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

How could we use this solution?

Example: Will my pipes freeze?

The temperature has been 35°F for a while now, sufficient to chill the ground to this temperature for many tens of feet below the surface. Suddenly the temperature drops to -20°F. How long will it take for freezing temperatures (32°F) to reach my pipes, which are 8 ft underground? Use the following physical properties:

$$h = 2.0 \frac{BTU}{h \text{ ft}^2 \text{ } ^\circ F}$$

$$\alpha_{soil} = 0.018 \frac{ft^2}{h}$$

$$k_{soil} = 0.5 \frac{BTU}{h \text{ ft } ^\circ F}$$

© Faith A. Morrison, Michigan Tech U. ²²

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{T - T_0}{T_1 - T_0} = \operatorname{erfc} \zeta - e^{\beta(2\zeta + \beta)} \operatorname{erfc}(\zeta + \beta)$$

$$\zeta \equiv \frac{x}{2\sqrt{\alpha t}}$$

$$\beta \equiv \frac{h\sqrt{\alpha t}}{k}$$

Both ζ
and β
depend
on time

$$T_0 = ?$$

$$T_1 = ?$$

$$T = ?$$

$$\frac{T - T_0}{T_1 - T_0} = ?$$

23
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\left(\frac{T - T_0}{T_1 - T_0} \right)$$

(Iterative solution)

Geankoplis 4th ed., Figure 5.3-3, page 364

$$\zeta = \frac{x}{2\sqrt{\alpha t}}$$

24
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State Heat Conduction in a Semi-Infinite Slab

$$\frac{T - T_0}{T_1 - T_0} = \text{erfc} \zeta - e^{\beta(2\zeta + \beta)} \text{erfc}(\zeta + \beta)$$

$$t \geq 0$$

$$T = T_1$$

$$t > 0$$

$$T = T(x, t)$$

Answer:
 $t = 480 \text{ hours} \approx 20 \text{ days}$

25
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

Example 8: Unsteady Heat Conduction in a Finite-sized solid

- The slab is tall and wide, but of thickness $2H$
- Initially at T_0
- at time $t = 0$ the temperature of the sides is changed to T_1

26
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Unsteady State Heat Transfer

Use same microscopic energy balance eqn as before.

$$\rho \hat{C}_p \underbrace{\left(\frac{\partial T}{\partial t} + \underbrace{\underline{v} \cdot \nabla T}_{\text{convection}} \right)}_{\text{rate of change}} = \underbrace{k \nabla^2 T}_{\text{conduction (all directions)}} + \underbrace{S}_{\text{source (energy generated per unit volume per time)}}$$

see handout for component notation

© Faith A. Morrison, Michigan Tech U. ²⁷

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Microscopic Energy Equation in Cartesian Coordinates

$$\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{S}{\rho \hat{C}_p}$$

$$\alpha \equiv \frac{k}{\rho \hat{C}_p} = \text{thermal diffusivity}$$

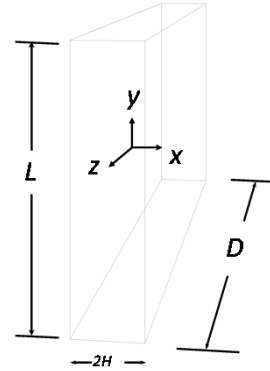
what are the boundary conditions? initial conditions?

© Faith A. Morrison, Michigan Tech U. ²⁸

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Example 8: Unsteady Heat Conduction in a Finite-sized solid

You try.

© Faith A. Morrison, Michigan Tech U. ²⁹

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Unsteady State Heat Conduction in a Finite Slab

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} \right) = \alpha \left(\frac{\partial^2 T}{\partial x^2} \right)$$

Initial condition: $t = 0, T = T_o \forall x$

Boundary conditions:

$$\left. \begin{array}{l} x = 0, \quad T = T_1 \\ x = 2H, \quad T = T_1 \end{array} \right\} \forall t > 0$$

© Faith A. Morrison, Michigan Tech U. ³⁰

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Q: How can two completely different situations give the same governing equation?

A: The boundary conditions make all the difference

For more solutions to this equation see Carslaw and Jeager, *Conduction of Heat in Solids*, 2nd Edition, Oxford, 1959

31
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Unsteady State Heat Conduction in a Finite Slab

$$\frac{\partial T}{\partial t} = \frac{k}{\rho \hat{C}_p} \left(\frac{\partial^2 T}{\partial x^2} \right) = \alpha \left(\frac{\partial^2 T}{\partial x^2} \right)$$

The solution is obtained by separation of variables.

Initial condition: $t = 0, T = T_0 \forall x$

Boundary conditions:

$$\left. \begin{array}{l} x = 0, \quad T = T_1 \\ x = 2H, \quad T = T_1 \end{array} \right\} \forall t > 0$$

32
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Unsteady State Heat Conduction in a Finite Slab: solution by separation of variables

$$\text{Let } Y \equiv \left(\frac{T_1 - T}{T_1 - T_o} \right) \quad \frac{\partial Y}{\partial t} = \alpha \left(\frac{\partial^2 Y}{\partial x^2} \right)$$

Guess: $Y = X(x)\Theta(t)$

Initial condition:

$$t = 0, T = T_o \quad \forall x \Rightarrow Y = 1$$

Boundary conditions:

$$\left. \begin{array}{l} x = 0, \quad T = T_1 \Rightarrow Y = 0 \\ x = 2H, \quad T = T_1 \Rightarrow Y = 0 \end{array} \right\} \quad \forall t > 0$$

© Faith A. Morrison, Michigan Tech U. ³³

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Unsteady State Heat Conduction in a Finite Slab: soln by separation of variables

$$Y = X(x)\Theta(t) \quad \frac{\partial Y}{\partial t} = \alpha \left(\frac{\partial^2 Y}{\partial x^2} \right)$$

$$\frac{\partial Y}{\partial t} = \frac{\partial}{\partial t} (X(x)\Theta(t)) = X(x) \frac{d\Theta(t)}{dt}$$

$$\frac{\partial Y}{\partial x} = \frac{\partial}{\partial x} (X(x)\Theta(t)) = \frac{dX(x)}{dx} \Theta(t)$$

$$\frac{\partial^2 Y}{\partial x^2} = \frac{d^2 X(x)}{dx^2} \Theta(t)$$

© Faith A. Morrison, Michigan Tech U. ³⁴

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

$$\frac{\partial Y}{\partial t} = \alpha \left(\frac{\partial^2 Y}{\partial x^2} \right)$$

Substituting: $X(x) \frac{d\Theta(t)}{dt} = \alpha \frac{d^2 X(x)}{dx^2} \Theta(t)$

The function of two variables is separable into two functions of one variable.

$$\underbrace{\frac{1}{\Theta(t)} \frac{d\Theta(t)}{dt}}_{\text{function of time (t) only}} = \alpha \underbrace{\frac{1}{X(x)} \frac{d^2 X(x)}{dx^2}}_{\text{function of position (x) only}} \Rightarrow = \lambda$$

constant

35
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

Separates into two ordinary differential equations:

$$\frac{1}{\Theta(t)} \frac{d\Theta(t)}{dt} = \lambda$$

$$\alpha \frac{1}{X(x)} \frac{d^2 X(x)}{dx^2} = \lambda$$

The function of two variables is separable into two functions of one variable.

Solve.

Apply BCs.

Apply ICs.

36
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady Heat Conduction in a Finite Solid

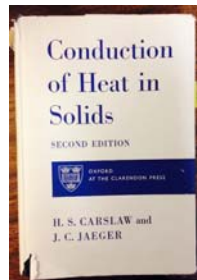
Temperature Profile for Unsteady State Heat Conduction in a Finite Slab

$$\left(\frac{T_1 - T}{T_1 - T_0}\right) = \frac{4}{\pi} \left\{ e^{-\frac{\pi^2 \alpha t}{4H^2}} \sin \frac{\pi x}{2H} + \frac{1}{3} e^{-\frac{9\pi^2 \alpha t}{4H^2}} \sin \frac{3\pi x}{2H} + \frac{1}{5} e^{-\frac{25\pi^2 \alpha t}{4H^2}} \sin \frac{5\pi x}{2H} + \dots \right\}$$

Geankoplis 4th ed., eqn 5.3-6, p363


37
© Faith A. Morrison, Michigan Tech U.

We use solutions like this in CM3215 to back calculate *h* from non-steady data:



38
© Faith A. Morrison, Michigan Tech U.

1D Heat Transfer: Unsteady State

 **Microscopic Energy Balance – is the correct physics for many problems!**

Tricky step:

solving for T field; this can be mathematically difficult

- partial differential equation in up to three variables
- boundaries may be complex
- multiple materials, multiple phases present
- may not be separable from mass and momentum balances

Strategy:

- Look up solution in literature
- solve using numerical methods (e.g. *Comsol*)

**** Or ****

- Develop correlations on complex systems by using *Dimensional Analysis*

39
© Faith A. Morrison, Michigan Tech U.

Fluid Mechanics: What did we do?

- Turbulent tube flow
- Noncircular conduits
- Drag on obstacles

}

1. Find a simple problem that allows us to identify the physics
2. Nondimensionalize
3. Explore that problem
4. Take data and correlate
5. Solve real problems

Solve. Real. Problems.

Powerful.



Works on heat transfer too.

40
© Faith A. Morrison, Michigan Tech U.

CM3110
Transport I
Part III: Heat Transfer

MichiganTech

More Complex Heat Transfer – Dimensional Analysis



Professor Faith Morrison
Department of Chemical Engineering
Michigan Technological University

© Faith A. Morrison, Michigan Tech U.⁴¹