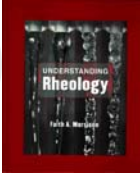


## Polymer Rheology

Rhe-  
 $\rho\epsilon\iota$  – Greek for flow

CM4650  
 Polymer Rheology  
 Michigan Tech



What is rheology anyway?

*Rheology = the study of deformation and flow.*



“What is Rheology Anyway?” Faith A. Morrison, *The Industrial Physicist*, 10(2) 29-31, April/May 2004.

1

© Faith A. Morrison, Michigan Tech U.

### What is rheology anyway?

**To the layperson, rheology is**

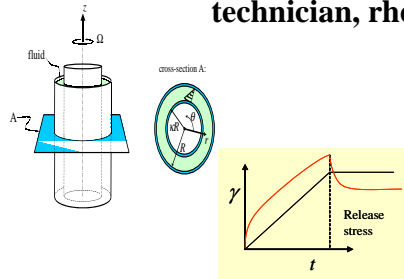
- Mayonnaise does not flow even under stress for a long time; honey always flows
- Silly Putty bounces (is elastic) but also flows (is viscous)
- Dilute flour-water solutions are easy to work with but doughs can be quite temperamental
- Corn starch and water can display strange behavior – poke it slowly and it deforms easily around your finger; punch it rapidly and your fist bounces off of the surface

2

© Faith A. Morrison, Michigan Tech U.

## What is rheology anyway?

To the scientist, engineer, or technician, rheology is



- Yield stresses
- Viscoelastic effects
- Memory effects
- Shear thickening and shear thinning

For both the layperson and the technical person, rheology is a set of problems or observations related to how the stress in a material or force applied to a material is related to deformation (change of shape) of the material.

3

© Faith A. Morrison, Michigan Tech U.

## What is rheology anyway?

Rheology affects:



- End use (food texture, product pour, motor-oil function)

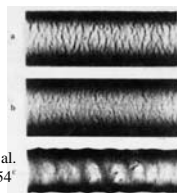
- Processing (design, costs, production rates)



[www.corrugatorman.com/pic/akron%20extruder.JPG](http://www.corrugatorman.com/pic/akron%20extruder.JPG)



[www.math.utwente.nl/mpcm/aamp/examples.html](http://www.math.utwente.nl/mpcm/aamp/examples.html)



Pomar et al.  
JNNFM 54  
143 1994

- Product quality (surface distortions, anisotropy, strength, structure development)

4

© Faith A. Morrison, Michigan Tech U.

## Goal of the scientist, engineer, or technician:

- **Understand** the kinds of flow and deformation **effects** exhibited by complex systems
- **Apply qualitative** rheological **knowledge** to diagnostic, design, or optimization problems
- In diagnostic, design, or optimization problems, **use or devise quantitative** analytical **tools** that correctly capture rheological effects

**How  
do we reach  
these goals?**

5

© Faith A. Morrison, Michigan Tech U.

## How?

By observing the behavior  
of different systems

• **Understand** the kinds of flow and deformation **effects** exhibited by complex systems

• **Apply qualitative** rheological **knowledge** to diagnostic, design, or optimization problems

• In diagnostic, design, or optimization problems, **Use or devise quantitative** analytical **tools** that correctly capture rheological effects

By making  
calculations  
with models in  
appropriate  
situations

By learning  
which  
quantitative  
models  
apply in  
what  
circum-  
stances

© Faith A. Morrison, Michigan Tech U.

## Learning Rheology (bibliography)

### Descriptive Rheology

Barnes, H., J. Hutton, and K. Walters, *An Introduction to Rheology* (Elsevier, 1989)

### Quantitative Rheology

Morrison, Faith, *Understanding Rheology* (Oxford, 2001)

Bird, R., R. Armstrong, and O. Hassager, *Dynamics of Polymeric Liquids, Volume I* (Wiley, 1987)

### Industrial Rheology

Dealy, John and Kurt Wissbrun, *Melt Rheology and Its Role in Plastics Processing* (Van Nostrand Reinhold, 1990)

### Polymer Behavior

Larson, Ron, *The Structure and Rheology of Complex Fluids* (Oxford, 1999)

Ferry, John, *Viscoelastic Properties of Polymers* (Wiley, 1980)

### Suspension Behavior

Mewis, Jan and Norm Wagner, *Colloidal Suspension* (Cambridge, 2012)

Macosko, Chris, *Rheology: Principles, Measurements, and Applications* (VCH Publishers, 1994)

7

© Faith A. Morrison, Michigan Tech U.

## The Physics Behind Rheology:

### 1. Conservation laws

mass  
momentum  
energy

### Cauchy Momentum Equation

$$\rho \left( \frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \nabla \underline{v} \right) = -\nabla p - \nabla \cdot \underline{\underline{\tau}} + \rho \underline{g}$$

### 2. Mathematics

differential equations  
vectors  
tensors

### 3. Constitutive law = law that relates **stress** to **deformation** for a particular fluid

8

© Faith A. Morrison, Michigan Tech U.

Polymer Rheology

Non-Newtonian Fluid Mechanics

Newtonian fluids:  
(fluid mechanics)

$$\tau_{21} = -\mu \frac{dv_1}{dx_2}$$

material parameter

deformation

Newton's Law of Viscosity

material parameter

deformation

- This is an empirical law (measured or observed)
- May be derived theoretically for some systems

Non-Newtonian fluids:  
(rheology)

Need a new law or new laws

Need a new law or new laws

- These laws will also either be empirical or will be derived theoretically

9

© Faith A. Morrison, Michigan Tech U.

Polymer Rheology

Non-Newtonian Fluid Mechanics

Newtonian fluids:  
(shear flow only)

$$\tau_{21} = -\mu \frac{dv_1}{dx_2}$$

Constitutive Equation

Non-Newtonian fluids:  
(all flows)

$$\underline{\underline{\tau}} = -f(\underline{\underline{\dot{\gamma}}})$$

stress tensor

Rate-of-deformation tensor

non-linear function  
(in time and position)

Rate-of-deformation tensor

non-linear function  
(in time and position)

10

© Faith A. Morrison, Michigan Tech U.

## Introduction to Non-Newtonian Behavior

*Rheological Behavior of Fluids, National  
Committee on Fluid Mechanics Films, 1964*

Velocity gradient tensor  $\dot{\gamma}$

Type of fluid	Momentum balance	Stress –Deformation relationship (constitutive equation)
Inviscid (zero viscosity, $\mu=0$ )	Euler equation (Navier-Stokes with zero viscosity)	Stress is isotropic
Newtonian (finite, constant viscosity, $\mu$ )	Navier-Stokes (Cauchy momentum equation with Newtonian constitutive equation)	Stress is a function of the <b>instantaneous</b> velocity gradient
Non-Newtonian (finite, variable viscosity $\eta$ plus <b>memory</b> effects)	Cauchy momentum equation with memory constitutive equation	Stress is a function of the <b>history</b> of the velocity gradient

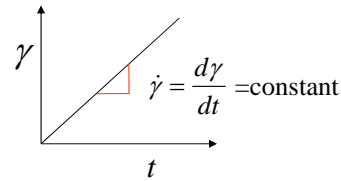
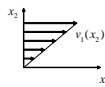
11

© Faith A. Morrison, Michigan Tech U.

## Rheological Behavior of Fluids - **Newtonian**

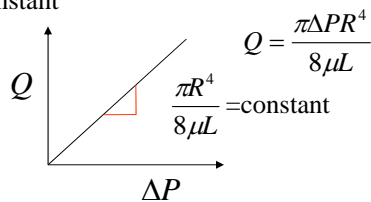
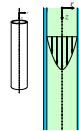
1. Strain response to imposed shear stress

•shear rate is constant



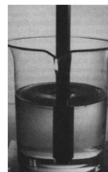
2. Pressure-driven flow in a tube (Poiseuille flow)

•viscosity is constant



3. Stress tensor in shear flow

•only two components are nonzero



$$\underline{\underline{\tau}} = \begin{pmatrix} 0 & \tau_{12} & 0 \\ \tau_{21} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}_{123}$$

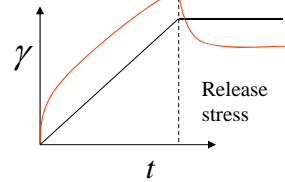
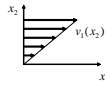
12

© Faith A. Morrison, Michigan Tech U.

# Rheological Behavior of Fluids – non-Newtonian

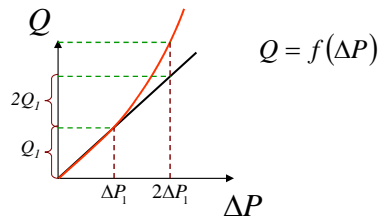
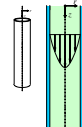
## 1. Strain response to imposed shear stress

- shear rate is variable



## 2. Pressure-driven flow in a tube (Poiseuille flow)

- viscosity is variable



## 3. Stress tensor in shear flow

Normal stresses

- all 9 components are nonzero



$$\tau = \begin{pmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{pmatrix}_{123}$$

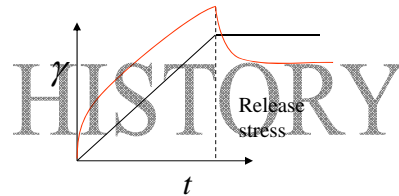
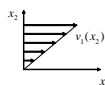
13

© Faith A. Morrison, Michigan Tech U.

# Rheological Behavior of Fluids – non-Newtonian

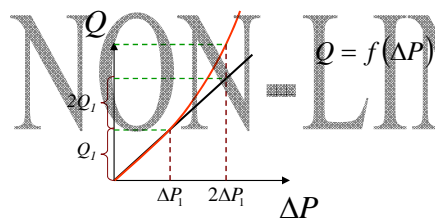
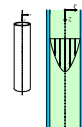
## 1. Strain response to imposed shear stress

- shear rate is variable



## 2. Pressure-driven flow in a tube (Poiseuille flow)

- viscosity is variable



Normal stresses

- all 9 components are nonzero



$$\tau = \begin{pmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{pmatrix}_{123}$$

14

© Faith A. Morrison, Michigan Tech U.

## Examples from the film of . . . .

### Dependence on the history of the deformation gradient

- Polymer fluid pours, but springs back
- Elastic ball bounces, but flows if given enough time
- Steel ball dropped in polymer solution “bounces”
- Polymer solution in concentric cylinders – has fading memory
- Quantitative measurements in concentric cylinders show memory and need a finite time to come to steady state

### Non-linearity of the function $\underline{\tau} = f(\dot{\underline{\gamma}})$

- Polymer solution draining from a tube is first slower, then faster than a Newtonian fluid
- Double the static head on a draining tube, and the flow rate does not necessarily double (as it does for Newtonian fluids); sometimes more than doubles, sometimes less
- Normal stresses in shear flow
- Die swell

15

© Faith A. Morrison, Michigan Tech U.

### Show NCFM Film on *Rheological Behavior of Fluids*

- Search for NCFMF
- [web.mit.edu/hml/ncfmf.html](http://web.mit.edu/hml/ncfmf.html)
- Also on YouTube

16

© Faith A. Morrison, Michigan Tech U.



## Chapter 2: Mathematics Review

1. Scalar – *a mathematical entity that has magnitude only*

**e.g.:** temperature  $T$   
 speed  $v$   
 time  $t$   
 density  $\rho$

– scalars may be constant or may be variable

### Laws of Algebra for Scalars:

**yes** commutative     $ab = ba$   
**yes** associative     $a(bc) = (ab)c$   
**yes** distributive     $a(b+c) = ab+ac$

17

© Faith A. Morrison, Michigan Tech U.

### Mathematics Review

Polymer Rheology

2. Vector – *a mathematical entity that has magnitude and direction*

**e.g.:** force on a surface  $\underline{f}$   
 velocity  $\underline{v}$

– vectors may be constant or may be variable

### Definitions

magnitude of a vector – a scalar associated with a vector

$$|\underline{v}| = v \quad |\underline{f}| = f$$

unit vector – a vector of unit length

$$\frac{v}{|\underline{v}|} = \hat{v}$$

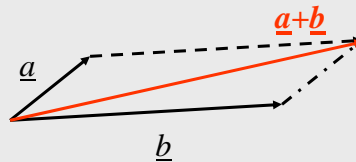
a unit vector in the direction of  $\underline{v}$

18

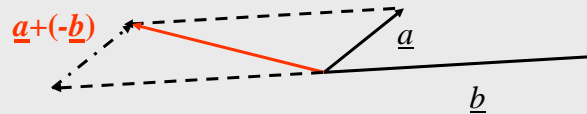
© Faith A. Morrison, Michigan Tech U.

### Laws of Algebra for Vectors:

#### 1. Addition



#### 2. Subtraction



19

© Faith A. Morrison, Michigan Tech U.

### Laws of Algebra for Vectors (continued):

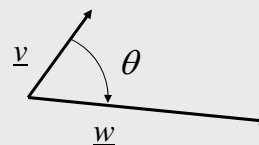
#### 3. Multiplication by scalar $\alpha \underline{v}$

- yes commutative  $\alpha \underline{v} = \underline{v} \alpha$
- yes associative  $\alpha(\beta \underline{v}) = (\alpha\beta) \underline{v} = \alpha\beta \underline{v}$
- yes distributive  $\alpha(\underline{v} + \underline{w}) = \alpha \underline{v} + \alpha \underline{w}$

#### 4. Multiplication of vector by vector

##### 4a. scalar (dot) (inner) product

$$\underline{v} \cdot \underline{w} = vw \cos \theta$$



Note: we can find magnitude with dot product

$$\underline{v} \cdot \underline{v} = vv \cos 0 = v^2$$

$$v = |\underline{v}| = \sqrt{\underline{v} \cdot \underline{v}}$$

20

© Faith A. Morrison, Michigan Tech U.

Laws of Algebra for Vectors (continued):

4a. scalar (dot) (inner) product (con't)

yes commutative  $\underline{v} \cdot \underline{w} = \underline{w} \cdot \underline{v}$

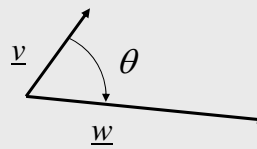
NO associative  ~~$\underline{v} \cdot \underline{w} \cdot \underline{z}$~~  no such operation

yes distributive  $\underline{z} \cdot (\underline{v} + \underline{w}) = \underline{z} \cdot \underline{v} + \underline{z} \cdot \underline{w}$

4b. vector (cross) (outer) product

$$\underline{v} \times \underline{w} = vw \sin \theta \hat{e}$$

$\hat{e}$  is a unit vector  
perpendicular to  
both  $\underline{v}$  and  $\underline{w}$   
following the  
right-hand rule



21

© Faith A. Morrison, Michigan Tech U.

Laws of Algebra for Vectors (continued):

4b. vector (cross) (outer) product (con't)

NO commutative  $\underline{v} \times \underline{w} \neq \underline{w} \times \underline{v}$

NO associative  $\underline{v} \times \underline{w} \times \underline{z} \neq (\underline{v} \times \underline{w}) \times \underline{z} \neq \underline{v} \times (\underline{w} \times \underline{z})$

yes distributive  $\underline{z} \times (\underline{v} + \underline{w}) = (\underline{z} \times \underline{v}) + (\underline{z} \times \underline{w})$

22

© Faith A. Morrison, Michigan Tech U.

### Coordinate Systems

- Allow us to make actual calculations with vectors

Rule: any three vectors that are *non-zero* and *linearly independent* (non-coplanar) may form a coordinate basis

Three vectors are linearly dependent if  $\alpha$ ,  $\beta$ , and  $\gamma$  can be found such that:

$$\alpha \underline{a} + \beta \underline{b} + \gamma \underline{c} = \underline{0}$$

for  $\alpha, \beta, \gamma \neq 0$

If  $\alpha$ ,  $\beta$ , and  $\gamma$  are found to be zero, the vectors are linearly independent.

23

© Faith A. Morrison, Michigan Tech U.

### How can we do actual calculations with vectors?

Rule: any vector may be expressed as the linear combination of three, non-zero, non-coplanar basis vectors

any vector  $\underline{a}$  = coefficient of  $\underline{a}$  in the  $\hat{e}_y$  direction

$$\underline{a} = a_x \hat{e}_x + a_y \hat{e}_y + a_z \hat{e}_z = \begin{pmatrix} a_x \\ a_y \\ a_z \end{pmatrix}_{xyz}$$

$$= a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3$$

$$= \sum_{j=1}^3 a_j \hat{e}_j$$

24

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

Trial calculation: dot product of two vectors

$$\begin{aligned}
 \underline{a} \cdot \underline{b} &= (a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3) \cdot (b_1 \hat{e}_1 + b_2 \hat{e}_2 + b_3 \hat{e}_3) \\
 &= a_1 \hat{e}_1 \cdot (b_1 \hat{e}_1 + b_2 \hat{e}_2 + b_3 \hat{e}_3) + \\
 &\quad a_2 \hat{e}_2 \cdot (b_1 \hat{e}_1 + b_2 \hat{e}_2 + b_3 \hat{e}_3) + \\
 &\quad a_3 \hat{e}_3 \cdot (b_1 \hat{e}_1 + b_2 \hat{e}_2 + b_3 \hat{e}_3) \\
 &= a_1 \hat{e}_1 \cdot b_1 \hat{e}_1 + a_1 \hat{e}_1 \cdot b_2 \hat{e}_2 + a_1 \hat{e}_1 \cdot b_3 \hat{e}_3 + \\
 &\quad a_2 \hat{e}_2 \cdot b_1 \hat{e}_1 + a_2 \hat{e}_2 \cdot b_2 \hat{e}_2 + a_2 \hat{e}_2 \cdot b_3 \hat{e}_3 + \\
 &\quad a_3 \hat{e}_3 \cdot b_1 \hat{e}_1 + a_3 \hat{e}_3 \cdot b_2 \hat{e}_2 + a_3 \hat{e}_3 \cdot b_3 \hat{e}_3
 \end{aligned}$$

If we choose the basis to be orthonormal - mutually perpendicular and of unit length - then we can simplify.

25

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

If we choose the basis to be orthonormal - mutually perpendicular and of unit length, then we can simplify.

$$\begin{aligned}
 \hat{e}_1 \cdot \hat{e}_1 &= 1 \\
 \hat{e}_1 \cdot \hat{e}_2 &= 0 \\
 \hat{e}_1 \cdot \hat{e}_3 &= 0 \\
 &\dots
 \end{aligned}$$

$$\begin{aligned}
 \underline{a} \cdot \underline{b} &= a_1 \hat{e}_1 \cdot b_1 \hat{e}_1 + a_1 \hat{e}_1 \cdot b_2 \hat{e}_2 + a_1 \hat{e}_1 \cdot b_3 \hat{e}_3 + \\
 &\quad a_2 \hat{e}_2 \cdot b_1 \hat{e}_1 + a_2 \hat{e}_2 \cdot b_2 \hat{e}_2 + a_2 \hat{e}_2 \cdot b_3 \hat{e}_3 + \\
 &\quad a_3 \hat{e}_3 \cdot b_1 \hat{e}_1 + a_3 \hat{e}_3 \cdot b_2 \hat{e}_2 + a_3 \hat{e}_3 \cdot b_3 \hat{e}_3 \\
 &= a_1 b_1 + a_2 b_2 + a_3 b_3
 \end{aligned}$$

We can generalize this operation with a technique called Einstein notation.

26

© Faith A. Morrison, Michigan Tech U.

## Einstein Notation

a system of notation for vectors and tensors that allows for the calculation of results in Cartesian coordinate systems.

$$\begin{aligned}\underline{a} &= a_1\hat{e}_1 + a_2\hat{e}_2 + a_3\hat{e}_3 \\ &= \sum_{j=1}^3 a_j\hat{e}_j \\ &= a_j\hat{e}_j = a_m\hat{e}_m\end{aligned}$$

- the initial choice of subscript letter is *arbitrary*
- the presence of a pair of like subscripts implies a missing summation sign

27

© Faith A. Morrison, Michigan Tech U.

## Einstein Notation (con't)

The result of the dot products of basis vectors can be summarized by the Kronecker delta function

$$\begin{aligned}\hat{e}_1 \cdot \hat{e}_1 &= 1 \\ \hat{e}_1 \cdot \hat{e}_2 &= 0 \\ \hat{e}_1 \cdot \hat{e}_3 &= 0 \\ \dots &\end{aligned} \quad \hat{e}_i \cdot \hat{e}_p = \delta_{ip} = \begin{cases} 1 & i = p \\ 0 & i \neq p \end{cases}$$

Kronecker delta

28

© Faith A. Morrison, Michigan Tech U.

## Einstein Notation (con't)

To carry out a dot product of two arbitrary vectors . . .

## Detailed Notation

$$\begin{aligned}
 \underline{a} \cdot \underline{b} &= (a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3) \cdot (b_1 \hat{e}_1 + b_2 \hat{e}_2 + b_3 \hat{e}_3) \\
 &= a_1 \hat{e}_1 \cdot b_1 \hat{e}_1 + a_1 \hat{e}_1 \cdot b_2 \hat{e}_2 + a_1 \hat{e}_1 \cdot b_3 \hat{e}_3 + \\
 &\quad a_2 \hat{e}_2 \cdot b_1 \hat{e}_1 + a_2 \hat{e}_2 \cdot b_2 \hat{e}_2 + a_2 \hat{e}_2 \cdot b_3 \hat{e}_3 + \\
 &\quad a_3 \hat{e}_3 \cdot b_1 \hat{e}_1 + a_3 \hat{e}_3 \cdot b_2 \hat{e}_2 + a_3 \hat{e}_3 \cdot b_3 \hat{e}_3 \\
 &= a_1 b_1 + a_2 b_2 + a_3 b_3
 \end{aligned}$$

## Einstein Notation

$$\begin{aligned}
 \underline{a} \cdot \underline{b} &= a_j \hat{e}_j \cdot b_m \hat{e}_m \\
 &= a_j \delta_{jm} b_m \\
 &= a_j b_j
 \end{aligned}$$

29

© Faith A. Morrison, Michigan Tech U.

## 3. Tensor – the indeterminate vector product of two (or more) vectors

e.g.: stress  $\underline{\underline{\tau}}$   
velocity gradient  $\underline{\underline{\gamma}}$

– tensors may be constant or may be variable

## Definitions

dyad or dyadic product – a tensor written explicitly as the indeterminate vector product of two vectors

$\underline{a} \underline{d}$  dyad  
 $\underline{\underline{A}}$  general representation  
of a tensor

30

© Faith A. Morrison, Michigan Tech U.

### Laws of Algebra for Indeterminate Product of Vectors:

NO commutative	$\underline{a} \underline{v} \neq \underline{v} \underline{a}$
yes associative	$\underline{b} (\underline{a} \underline{v}) = (\underline{b} \underline{a}) \underline{v} = \underline{b} \underline{a} \underline{v}$
yes distributive	$\underline{a} (\underline{v} + \underline{w}) = \underline{a} \underline{v} + \underline{a} \underline{w}$

31

© Faith A. Morrison, Michigan Tech U.

How can we represent tensors with respect to a chosen coordinate system?

Just follow the rules of tensor algebra

$$\begin{aligned}
 \underline{a} \underline{m} &= (a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3)(m_1 \hat{e}_1 + m_2 \hat{e}_2 + m_3 \hat{e}_3) \\
 &= a_1 \hat{e}_1 m_1 \hat{e}_1 + a_1 \hat{e}_1 m_2 \hat{e}_2 + a_1 \hat{e}_1 m_3 \hat{e}_3 + \\
 &\quad a_2 \hat{e}_2 m_1 \hat{e}_1 + a_2 \hat{e}_2 m_2 \hat{e}_2 + a_2 \hat{e}_2 m_3 \hat{e}_3 + \\
 &\quad a_3 \hat{e}_3 m_1 \hat{e}_1 + a_3 \hat{e}_3 m_2 \hat{e}_2 + a_3 \hat{e}_3 m_3 \hat{e}_3 \\
 &= \sum_{k=1}^3 \sum_{w=1}^3 a_k \hat{e}_k m_w \hat{e}_w \\
 &= \sum_{k=1}^3 \sum_{w=1}^3 a_k m_w \hat{e}_k \hat{e}_w
 \end{aligned}$$

Any tensor may be written as the sum of 9 dyadic products of basis vectors

32

© Faith A. Morrison, Michigan Tech U.



What about  $\underline{\underline{A}}$  ? Same.

$$\underline{\underline{A}} = \sum_{i=1}^3 \sum_{j=1}^3 A_{ij} \hat{e}_i \hat{e}_j$$

Einstein notation for tensors: *drop the summation sign; every double index implies a summation sign has been dropped.*

$$\underline{\underline{A}} = A_{ij} \hat{e}_i \hat{e}_j = A_{pk} \hat{e}_p \hat{e}_k$$

Reminder: the initial choice of subscript letters is arbitrary

33

© Faith A. Morrison, Michigan Tech U.

How can we use Einstein Notation to calculate dot products between vectors and tensors?

It's the same as between vectors.

$$\underline{a} \cdot \underline{b} =$$

$$\underline{a} \cdot \underline{u} \underline{v} =$$

$$\underline{b} \cdot \underline{\underline{A}} =$$

34

© Faith A. Morrison, Michigan Tech U.

### Summary of Einstein Notation

1. Express vectors, tensors, (later, vector operators) in a Cartesian coordinate system as the sums of coefficients multiplying basis vectors - each separate summation has a different index
2. Drop the summation signs
3. Dot products between basis vectors result in the Kronecker delta function because the Cartesian system is orthonormal.

#### Note:

- In Einstein notation, the presence of repeated indices implies a missing summation sign
- The choice of initial index (i, m, p, etc.) is **arbitrary** - it merely indicates which indices change together

35

© Faith A. Morrison, Michigan Tech U.

### 3. Tensor – (continued)

#### Definitions

Scalar product of two tensors

$$\begin{aligned}
 \underline{\underline{A}} : \underline{\underline{M}} &= A_{ip} \hat{e}_i \hat{e}_p : M_{km} \hat{e}_k \hat{e}_m \\
 &= A_{ip} M_{km} \overbrace{\hat{e}_i \hat{e}_p : \hat{e}_k \hat{e}_m}^{\text{carry out the dot products indicated}} \\
 &= A_{ip} M_{km} (\hat{e}_p \cdot \hat{e}_k) (\hat{e}_i \cdot \hat{e}_m) \\
 &= A_{ip} M_{km} \delta_{pk} \delta_{im} \quad \begin{array}{l} \text{"p" becomes "k"} \\ \text{"i" becomes "m"} \end{array} \\
 &= A_{mk} M_{km}
 \end{aligned}$$

36

© Faith A. Morrison, Michigan Tech U.

### But, what is a tensor really?

A tensor is a handy representation of a *Linear Vector Function*

scalar function:  $y = f(x) = x^2 + 2x + 3$

a mapping of values of  $x$  onto values of  $y$

vector function:  $\underline{w} = f(\underline{v})$

a mapping of vectors of  $\underline{v}$  into vectors  $\underline{w}$

**How do we express a  
vector function?**

37

© Faith A. Morrison, Michigan Tech U.

### What is a linear function?

*Linear, in this usage, has a precise, mathematical definition.*

Linear functions (scalar and vector) have the following two properties:

$$f(\lambda x) = \lambda f(x)$$

$$f(x + w) = f(x) + f(w)$$

It turns out . . .

Multiplying vectors and tensors is a convenient way of representing the actions of a **linear vector function** (as we will now show).

38

© Faith A. Morrison, Michigan Tech U.

Tensors are *Linear Vector Functions*

Let  $f(\underline{a}) = \underline{b}$  be a linear vector function.

↑  
We can write  $\underline{a}$  in Cartesian coordinates.

$$\underline{a} = a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3$$

$$f(\underline{a}) = f(a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3) = \underline{b}$$

Using the linear properties of  $f$ , we can distribute the function action:

$$f(\underline{a}) = a_1 \underbrace{f(\hat{e}_1)} + a_2 \underbrace{f(\hat{e}_2)} + a_3 \underbrace{f(\hat{e}_3)} = \underline{b}$$

These results are just vectors, we will name them  $\underline{v}$ ,  $\underline{w}$ , and  $\underline{m}$ .

39

© Faith A. Morrison, Michigan Tech U.

Tensors are *Linear Vector Functions* (continued)

$$f(\underline{a}) = a_1 \underbrace{f(\hat{e}_1)}_{\underline{v}} + a_2 \underbrace{f(\hat{e}_2)}_{\underline{w}} + a_3 \underbrace{f(\hat{e}_3)}_{\underline{m}} = \underline{b}$$

$$f(\underline{a}) = a_1 \underline{v} + a_2 \underline{w} + a_3 \underline{m} = \underline{b}$$

Now we note that the coefficients  $a_i$  may be written as,

$$a_1 = \underline{a} \cdot \hat{e}_1 \quad a_2 = \underline{a} \cdot \hat{e}_2 \quad a_3 = \underline{a} \cdot \hat{e}_3$$

Substituting,

$$f(\underline{a}) = \underline{a} \cdot \hat{e}_1 \underline{v} + \underline{a} \cdot \hat{e}_2 \underline{w} + \underline{a} \cdot \hat{e}_3 \underline{m} = \underline{b}$$

The  
indeterminate  
vector product  
has appeared!

40

© Faith A. Morrison, Michigan Tech U.

Using the distributive law, we can factor out the dot product with  $\underline{a}$ :

$$f(\underline{a}) = \underline{a} \cdot (\underline{e}_1 \underline{v} + \underline{e}_2 \underline{w} + \underline{e}_3 \underline{m}) = \underline{b}$$

This is just a tensor  
(the sum of dyadic  
products of vectors)

$$(\underline{e}_1 \underline{v} + \underline{e}_2 \underline{w} + \underline{e}_3 \underline{m}) \equiv \underline{\underline{M}}$$

$$f(\underline{a}) = \underline{a} \cdot \underline{\underline{M}} = \underline{b}$$

**CONCLUSION:** Tensor operations  
are convenient to use  
to express linear  
vector functions.

41

© Faith A. Morrison, Michigan Tech U.

### 3. Tensor – (continued)

#### More Definitions

Identity Tensor

$$\begin{aligned} \underline{\underline{I}} &= \underline{e}_i \underline{e}_i = \underline{e}_1 \underline{e}_1 + \underline{e}_2 \underline{e}_2 + \underline{e}_3 \underline{e}_3 \\ &= \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123} \end{aligned}$$

$$\begin{aligned} \underline{\underline{A}} \cdot \underline{\underline{I}} &= A_{ip} \underline{e}_i \underline{e}_p \cdot \underline{e}_k \underline{e}_k \\ &= A_{ip} \underline{e}_i \delta_{pk} \underline{e}_k \\ &= A_{ik} \underline{e}_i \underline{e}_k \\ &= \underline{\underline{A}} \end{aligned}$$

42

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 3. Tensor – (continued)

## More Definitions

Zero Tensor

$$\underline{\underline{0}} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}_{123}$$

Magnitude of a Tensor

$$|\underline{\underline{A}}| \equiv +\sqrt{\frac{\underline{\underline{A}} : \underline{\underline{A}}}{2}}$$

$$\begin{aligned} \underline{\underline{A}} : \underline{\underline{A}} &= A_{ip} \hat{e}_i \hat{e}_p : A_{km} \hat{e}_k \hat{e}_m \\ &= A_{ip} A_{km} (\hat{e}_p \cdot \hat{e}_k) (\hat{e}_i \cdot \hat{e}_m) \\ &= A_{mk} A_{km} \end{aligned}$$

products  
across the  
diagonal

43

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 3. Tensor – (continued)

## More Definitions

Tensor Transpose

$$\underline{\underline{M}}^T = (M_{ik} \hat{e}_i \hat{e}_k)^T = M_{ik} \hat{e}_k \hat{e}_i$$

Exchange the  
coefficients across the  
diagonal

CAUTION:

$$\begin{aligned} (\underline{\underline{A}} \cdot \underline{\underline{C}})^T &= (A_{ik} \hat{e}_i \hat{e}_k \cdot C_{pj} \hat{e}_p \hat{e}_j)^T = (A_{ik} C_{pj} \hat{e}_i \hat{e}_j \delta_{kp})^T \\ &= (A_{ip} C_{pj} \hat{e}_i \hat{e}_j)^T \\ &= A_{ip} C_{pj} \hat{e}_j \hat{e}_i \end{aligned}$$

It is **not** equal to:  $(\underline{\underline{A}} \cdot \underline{\underline{C}})^T = (A_{ip} C_{pj} \hat{e}_i \hat{e}_j)^T$   
 $\neq A_{pi} C_{jp} \hat{e}_i \hat{e}_j$

I recommend you  
always interchange the  
indices on the basis  
vectors rather than on  
the coefficients.

44

© Faith A. Morrison, Michigan Tech U.

## 3. Tensor – (continued)

## More Definitions

Symmetric Tensor

e.g.

$$\underline{\underline{M}} = \underline{\underline{M}}^T$$

$$M_{ik} = M_{ki}$$

$$\begin{pmatrix} 1 & 2 & 3 \\ 2 & 4 & 5 \\ 3 & 5 & 6 \end{pmatrix}_{123}$$

Antisymmetric Tensor

e.g.

$$\underline{\underline{M}} = -\underline{\underline{M}}^T$$

$$M_{ik} = -M_{ki}$$

$$\begin{pmatrix} 0 & -2 & -3 \\ 2 & 0 & -5 \\ 3 & 5 & 0 \end{pmatrix}_{123}$$

45

© Faith A. Morrison, Michigan Tech U.

## 3. Tensor – (continued)

## More Definitions

Tensor order

Scalars, vectors, and tensors may all be considered to be tensors (entities that exist independent of coordinate system). They are tensors of different **orders**, however.

order = degree of complexity

scalars	0 <sup>th</sup> -order tensors	3 <sup>0</sup>
vectors	1 <sup>st</sup> -order tensors	3 <sup>1</sup>
tensors	2 <sup>nd</sup> -order tensors	3 <sup>2</sup>
higher-order tensors	3 <sup>rd</sup> -order tensors	3 <sup>3</sup>

Number of coefficients needed to express the tensor in 3D space

46

© Faith A. Morrison, Michigan Tech U.

## 3. Tensor – (continued)

## More Definitions

## Tensor Invariants

Scalars that are associated with tensors; these are numbers that are independent of coordinate system.

vectors:  $|\underline{v}| = v$  The magnitude of a vector is a scalar associated with the vector

It is independent of coordinate system, i.e. it is an invariant.

tensors:  $\underline{\underline{A}}$  There are three invariants associated with a second-order tensor.

47

© Faith A. Morrison, Michigan Tech U.

## Tensor Invariants

$$I_{\underline{\underline{A}}} \equiv \text{trace} \underline{\underline{A}} = \text{tr} \underline{\underline{A}}$$

For the tensor written in Cartesian coordinates:

$$\text{trace} \underline{\underline{A}} = A_{pp} = A_{11} + A_{22} + A_{33}$$

$$II_{\underline{\underline{A}}} \equiv \text{trace}(\underline{\underline{A}} \cdot \underline{\underline{A}}) = \underline{\underline{A}} : \underline{\underline{A}} = A_{pk} A_{kp}$$

$$III_{\underline{\underline{A}}} \equiv \text{trace}(\underline{\underline{A}} \cdot \underline{\underline{A}} \cdot \underline{\underline{A}}) = A_{pj} A_{jh} A_{hp}$$

Note: the definitions of invariants written in terms of coefficients are only valid when the tensor is written in Cartesian coordinates.

48

© Faith A. Morrison, Michigan Tech U.



## 4. Differential Operations with Vectors, Tensors

Scalars, vectors, and tensors are differentiated to determine rates of change (with respect to time, position)

- To carryout the differentiation with respect to a *single variable*, differentiate each coefficient individually.
- There is no change in order (vectors remain vectors, scalars remain scalars, etc).

$$\frac{\partial \alpha}{\partial t} \quad \frac{\partial \underline{w}}{\partial t} = \begin{pmatrix} \frac{\partial w_1}{\partial t} \\ \frac{\partial w_2}{\partial t} \\ \frac{\partial w_3}{\partial t} \end{pmatrix}_{123} \quad \frac{\partial \underline{B}}{\partial t} = \begin{pmatrix} \frac{\partial B_{11}}{\partial t} & \frac{\partial B_{21}}{\partial t} & \frac{\partial B_{31}}{\partial t} \\ \frac{\partial B_{21}}{\partial t} & \frac{\partial B_{22}}{\partial t} & \frac{\partial B_{23}}{\partial t} \\ \frac{\partial B_{31}}{\partial t} & \frac{\partial B_{32}}{\partial t} & \frac{\partial B_{33}}{\partial t} \end{pmatrix}_{123}$$

49

© Faith A. Morrison, Michigan Tech U.

## 4. Differential Operations with Vectors, Tensors (continued)

- To carryout the differentiation with respect to *3D spatial variation*, use the del (nabla) operator.

## Del Operator

- This is a vector operator
- Del may be applied in three different ways
- Del may operate on scalars, vectors, or tensors

This is written in  
Cartesian  
coordinates

{

$$\nabla \equiv \hat{e}_1 \frac{\partial}{\partial x_1} + \hat{e}_2 \frac{\partial}{\partial x_2} + \hat{e}_3 \frac{\partial}{\partial x_3} = \begin{pmatrix} \frac{\partial}{\partial x_1} \\ \frac{\partial}{\partial x_2} \\ \frac{\partial}{\partial x_3} \end{pmatrix}_{123}$$

$$= \sum_{p=1}^3 \hat{e}_p \frac{\partial}{\partial x_p} = \hat{e}_p \frac{\partial}{\partial x_p}$$

Einstein notation for del

50

© Faith A. Morrison, Michigan Tech U.

**Mathematics Review**

Polymer Rheology

---

4. Differential Operations with Vectors, Tensors (continued)

**A. Scalars - gradient**

Gibbs notation  $\nabla \beta \equiv \mathbf{e}_1 \frac{\partial}{\partial x_1} \beta + \mathbf{e}_2 \frac{\partial}{\partial x_2} \beta + \mathbf{e}_3 \frac{\partial}{\partial x_3} \beta = \begin{pmatrix} \frac{\partial \beta}{\partial x_1} \\ \frac{\partial \beta}{\partial x_2} \\ \frac{\partial \beta}{\partial x_3} \end{pmatrix}_{123}$

This is written in Cartesian coordinates

Gradient of a scalar field  $= \mathbf{e}_p \frac{\partial \beta}{\partial x_p}$

The gradient of a scalar field is a vector

The gradient operation captures the total spatial variation of a scalar, vector, or tensor field.

•gradient operation increases the order of the entity operated upon

51

© Faith A. Morrison, Michigan Tech U.

**Mathematics Review**

Polymer Rheology

---

4. Differential Operations with Vectors, Tensors (continued)

**B. Vectors - gradient**

The basis vectors can move out of the derivatives because they are constant (do not change with position)

$$\begin{aligned} \nabla \mathbf{w} &\equiv \mathbf{e}_1 \frac{\partial}{\partial x_1} \mathbf{w} + \mathbf{e}_2 \frac{\partial}{\partial x_2} \mathbf{w} + \mathbf{e}_3 \frac{\partial}{\partial x_3} \mathbf{w} \\ &= \mathbf{e}_1 \frac{\partial}{\partial x_1} (w_1 \mathbf{e}_1 + w_2 \mathbf{e}_2 + w_3 \mathbf{e}_3) \\ &\quad + \mathbf{e}_2 \frac{\partial}{\partial x_2} (w_1 \mathbf{e}_1 + w_2 \mathbf{e}_2 + w_3 \mathbf{e}_3) \\ &\quad + \mathbf{e}_3 \frac{\partial}{\partial x_3} (w_1 \mathbf{e}_1 + w_2 \mathbf{e}_2 + w_3 \mathbf{e}_3) \\ &= \mathbf{e}_1 \mathbf{e}_1 \frac{\partial w_1}{\partial x_1} + \mathbf{e}_1 \mathbf{e}_2 \frac{\partial w_2}{\partial x_1} + \mathbf{e}_1 \mathbf{e}_3 \frac{\partial w_3}{\partial x_1} + \mathbf{e}_2 \mathbf{e}_1 \frac{\partial w_1}{\partial x_2} + \\ &\quad \mathbf{e}_2 \mathbf{e}_2 \frac{\partial w_2}{\partial x_2} + \mathbf{e}_2 \mathbf{e}_3 \frac{\partial w_3}{\partial x_2} + \mathbf{e}_3 \mathbf{e}_1 \frac{\partial w_1}{\partial x_3} + \mathbf{e}_3 \mathbf{e}_2 \frac{\partial w_2}{\partial x_3} + \mathbf{e}_3 \mathbf{e}_3 \frac{\partial w_3}{\partial x_3} \end{aligned}$$

This is all written in Cartesian coordinates (basis vectors are constant)

52

© Faith A. Morrison, Michigan Tech U.

Mathematics Review

Polymer Rheology

4. Differential Operations with Vectors, Tensors (continued)

B. Vectors - gradient (continued)

Gradient of a vector field

$$\nabla \mathbf{w} \equiv \sum_{j=1}^3 \sum_{k=1}^3 \hat{e}_j \hat{e}_k \frac{\partial w_k}{\partial x_j} = \hat{e}_j \hat{e}_k \frac{\partial w_k}{\partial x_j} = \frac{\partial w_k}{\partial x_j} \hat{e}_j \hat{e}_k$$

constants may appear on either side of the differential operator

The gradient of a vector field is a tensor

Einstein notation for gradient of a vector

53

© Faith A. Morrison, Michigan Tech U.

Mathematics Review

Polymer Rheology

4. Differential Operations with Vectors, Tensors (continued)

C. Vectors - divergence

Divergence of a vector field

$$\begin{aligned} \nabla \cdot \mathbf{w} &\equiv \left( \hat{e}_1 \frac{\partial}{\partial x_1} + \hat{e}_2 \frac{\partial}{\partial x_2} + \hat{e}_3 \frac{\partial}{\partial x_3} \right) \cdot w_1 \hat{e}_1 + w_2 \hat{e}_2 + w_3 \hat{e}_3 \\ &= \frac{\partial w_1}{\partial x_1} + \frac{\partial w_2}{\partial x_2} + \frac{\partial w_3}{\partial x_3} \\ &= \sum_{i=1}^3 \frac{\partial w_i}{\partial x_i} = \frac{\partial w_i}{\partial x_i} \end{aligned}$$

The Divergence of a vector field is a scalar

Einstein notation for divergence of a vector

54

© Faith A. Morrison, Michigan Tech U.

Mathematics Review

Polymer Rheology

4. Differential Operations with Vectors, Tensors (continued)

C. Vectors - divergence (continued)

Using Einstein notation

constants may appear on either side of the differential operator

This is all written in Cartesian coordinates (basis vectors are constant)

$$\begin{aligned}\nabla \cdot \underline{w} &\equiv \underline{e}_m \frac{\partial}{\partial x_m} \cdot w_j \underline{e}_j = \frac{\partial w_j}{\partial x_m} \underline{e}_m \cdot \underline{e}_j = \frac{\partial w_j}{\partial x_m} \delta_{mj} \\ &= \frac{\partial w_j}{\partial x_j}\end{aligned}$$

•divergence operation decreases the order of the entity operated upon

55

© Faith A. Morrison, Michigan Tech U.

Mathematics Review

Polymer Rheology

4. Differential Operations with Vectors, Tensors (continued)

D. Vectors - Laplacian

Using Einstein notation:

$$\begin{aligned}\nabla \cdot \nabla \underline{w} &\equiv \underline{e}_m \frac{\partial}{\partial x_m} \cdot \underline{e}_p \frac{\partial}{\partial x_p} w_j \underline{e}_j = \frac{\partial}{\partial x_m} \frac{\partial}{\partial x_p} w_j (\underline{e}_m \cdot \underline{e}_p) \underline{e}_j \\ &= \frac{\partial}{\partial x_m} \frac{\partial}{\partial x_p} w_j (\delta_{mp}) \underline{e}_j \\ &= \frac{\partial}{\partial x_p} \frac{\partial}{\partial x_p} w_j \underline{e}_j \\ &= \left( \frac{\partial^2 w_1}{\partial x_1^2} + \frac{\partial^2 w_1}{\partial x_2^2} + \frac{\partial^2 w_1}{\partial x_3^2} \right) \underline{e}_1 + \left( \frac{\partial^2 w_2}{\partial x_1^2} + \frac{\partial^2 w_2}{\partial x_2^2} + \frac{\partial^2 w_2}{\partial x_3^2} \right) \underline{e}_2 + \left( \frac{\partial^2 w_3}{\partial x_1^2} + \frac{\partial^2 w_3}{\partial x_2^2} + \frac{\partial^2 w_3}{\partial x_3^2} \right) \underline{e}_3\end{aligned}$$

The Laplacian of a vector field is a *vector*

•Laplacian operation does not change the order of the entity operated upon

56

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 4. Differential Operations with Vectors, Tensors (continued)

- E. Scalar - divergence  $\nabla \times \alpha$  (impossible; cannot decrease order of a scalar)
- F. Scalar - Laplacian  $\nabla \cdot \nabla \alpha$
- G. Tensor - gradient  $\nabla \underline{\underline{A}}$
- H. Tensor - divergence  $\nabla \cdot \underline{\underline{A}}$
- I. Tensor - Laplacian  $\nabla \cdot \nabla \underline{\underline{A}}$

57

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates

Cylindrical  $\bar{r}, \theta, z$   $\hat{e}_{\bar{r}}, \hat{e}_{\theta}, \hat{e}_z$

Spherical  $r, \theta, \phi$   $\hat{e}_r, \hat{e}_{\theta}, \hat{e}_{\phi}$

See  
figures  
2.11 and  
2.12

These coordinate systems are ortho-normal, *but they are not constant* (they vary with position).

This causes some non-intuitive effects when derivatives are taken.

58

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates (continued)

$$\underline{v} = v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z$$

$$\nabla \cdot \underline{v} = \nabla \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z)$$

$$= \left( \frac{\partial}{\partial x} \hat{e}_x + \frac{\partial}{\partial y} \hat{e}_y + \frac{\partial}{\partial z} \hat{e}_z \right) \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z)$$

First, we need to write this  
in cylindrical coordinates.

solve for  
Cartesian  
basis  
vectors and  
substitute  
above

$$\begin{cases} \hat{e}_r = \cos \theta \hat{e}_x + \sin \theta \hat{e}_y \\ \hat{e}_\theta = -\sin \theta \hat{e}_x + \cos \theta \hat{e}_y \\ \hat{e}_z = \hat{e}_z \end{cases}$$

$$\begin{cases} x = r \cos \theta \\ y = r \sin \theta \\ z = z \end{cases}$$

substitute above  
using chain rule  
(see next slide for  
details)

59

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

$$\begin{aligned} \hat{e}_x &= \cos \theta \hat{e}_r - \sin \theta \hat{e}_\theta \\ \hat{e}_y &= \sin \theta \hat{e}_r + \cos \theta \hat{e}_\theta \end{aligned}$$

$$\begin{aligned} x &= r \cos \theta & r &= \sqrt{x^2 + y^2} \\ y &= r \sin \theta & \theta &= \tan^{-1} \left( \frac{y}{x} \right) \\ z &= z \end{aligned}$$

$$\nabla \psi = \left( \frac{\partial \psi}{\partial x} \hat{e}_x + \frac{\partial \psi}{\partial y} \hat{e}_y + \frac{\partial \psi}{\partial z} \hat{e}_z \right)$$

$$\frac{\partial \psi}{\partial x} = \frac{\partial \psi}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial \psi}{\partial \theta} \frac{\partial \theta}{\partial x} + \frac{\partial \psi}{\partial z} \frac{\partial z}{\partial x} = \frac{\partial \psi}{\partial r} \cos \theta + \frac{\partial \psi}{\partial \theta} \left( \frac{-\sin \theta}{r} \right)$$

$$\frac{\partial \psi}{\partial y} = \frac{\partial \psi}{\partial r} \frac{\partial r}{\partial y} + \frac{\partial \psi}{\partial \theta} \frac{\partial \theta}{\partial y} + \frac{\partial \psi}{\partial z} \frac{\partial z}{\partial y} = \frac{\partial \psi}{\partial r} \sin \theta + \frac{\partial \psi}{\partial \theta} \left( \frac{\cos \theta}{r} \right)$$

60

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates (continued)

**Result:**  $\nabla = \left( \frac{\partial}{\partial x} \hat{e}_x + \frac{\partial}{\partial y} \hat{e}_y + \frac{\partial}{\partial z} \hat{e}_z \right)$

$$= \hat{e}_r \frac{\partial}{\partial r} + \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \hat{e}_z \frac{\partial}{\partial z}$$

Now, proceed:

(We cannot use Einstein notation because these are not Cartesian coordinates)

$$\begin{aligned} \nabla \cdot \underline{v} &= \left( \hat{e}_r \frac{\partial}{\partial r} + \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \hat{e}_z \frac{\partial}{\partial z} \right) \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) \\ &= \hat{e}_r \frac{\partial}{\partial r} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\ &\quad \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\ &\quad \hat{e}_z \frac{\partial}{\partial z} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) \end{aligned}$$

61

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates (continued)

$$\begin{aligned} \nabla \cdot \underline{v} &= \hat{e}_r \frac{\partial}{\partial r} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\ &\quad \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\ &\quad \hat{e}_z \frac{\partial}{\partial z} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) \end{aligned}$$

$$\begin{aligned} \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} \cdot v_r \hat{e}_r &= \hat{e}_\theta \cdot \frac{1}{r} \frac{\partial v_r \hat{e}_r}{\partial \theta} \\ &= \hat{e}_\theta \cdot \frac{1}{r} \left( v_r \frac{\partial \hat{e}_r}{\partial \theta} + \hat{e}_r \frac{\partial v_r}{\partial \theta} \right) \end{aligned}$$

$$\begin{aligned} \frac{\partial \hat{e}_r}{\partial \theta} &= \frac{\partial}{\partial \theta} (\cos \theta \hat{e}_x + \sin \theta \hat{e}_y) \\ &= -\sin \theta \hat{e}_x + \cos \theta \hat{e}_y \\ &= \hat{e}_\theta \end{aligned}$$

62

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates (continued)

$$\begin{aligned}
 \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} \cdot v_r \hat{e}_r &= \hat{e}_\theta \cdot \frac{1}{r} \frac{\partial v_r \hat{e}_r}{\partial \theta} \\
 &= \hat{e}_\theta \cdot \frac{1}{r} \left( v_r \frac{\partial \hat{e}_r}{\partial \theta} + \hat{e}_r \frac{\partial v_r}{\partial \theta} \right) \\
 &= \hat{e}_\theta \cdot \frac{1}{r} \left( v_r \hat{e}_\theta + \hat{e}_r \frac{\partial v_r}{\partial \theta} \right) \\
 &= \frac{1}{r} v_r
 \end{aligned}$$

This term is not intuitive,  
and appears because the  
basis vectors in the  
curvilinear coordinate  
systems vary with position.

63

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

## 5. Curvilinear Coordinates (continued)

Final result for divergence of a  
vector in cylindrical coordinates:

$$\begin{aligned}
 \nabla \cdot \underline{v} &= \hat{e}_r \frac{\partial}{\partial r} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\
 &\quad \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) + \\
 &\quad \hat{e}_z \frac{\partial}{\partial z} \cdot (v_r \hat{e}_r + v_\theta \hat{e}_\theta + v_z \hat{e}_z) \\
 \nabla \cdot \underline{v} &= \frac{\partial v_r}{\partial r} + \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_r}{r} + \frac{\partial v_z}{\partial z}
 \end{aligned}$$

64

© Faith A. Morrison, Michigan Tech U.



## 5. Curvilinear Coordinates (continued)

## Curvilinear Coordinates (summary)

- The basis vectors are ortho-normal
- The basis vectors are non-constant (vary with position)
- These systems are convenient when the flow system mimics the coordinate surfaces in curvilinear coordinate systems.
- *We cannot use Einstein notation* – must use Tables in Appendix C2 (pp464-468).

65

© Faith A. Morrison, Michigan Tech U.

## 6. Vector and Tensor Theorems and definitions

In Chapter 3 we review Newtonian fluid mechanics using the vector/tensor vocabulary we have learned thus far. We just need a few more theorems to prepare us for those studies. These are presented without proof.

## Gauss Divergence Theorem

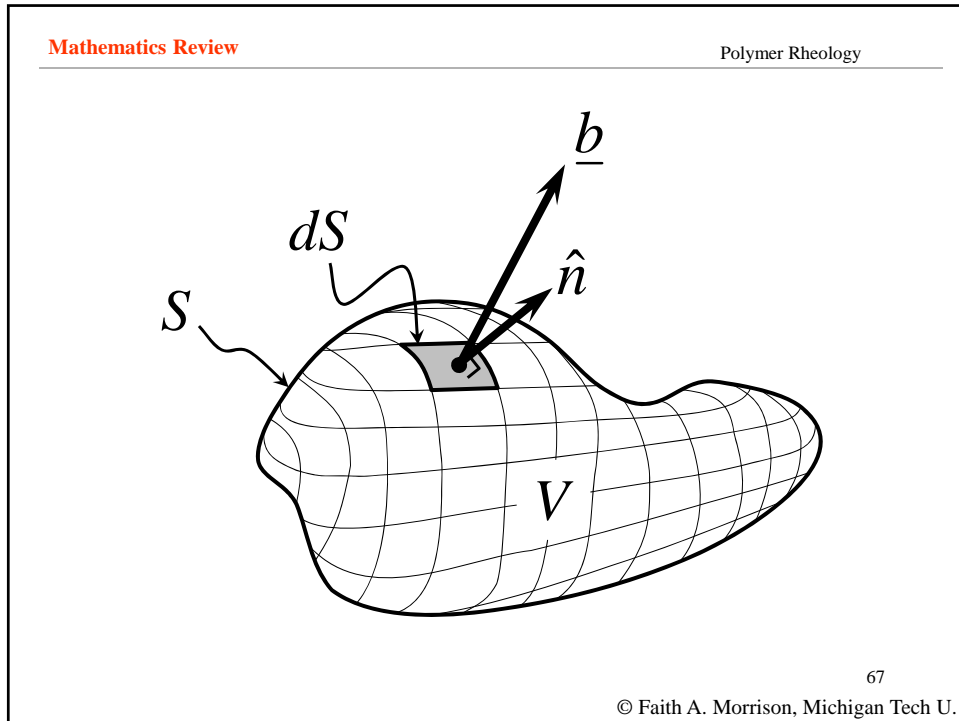
$$\iiint_V \nabla \cdot \underline{b} \, dV = \iint_S \hat{n} \cdot \underline{b} \, dS$$

outwardly  
directed unit  
normal

This theorem establishes the utility of the divergence operation. The integral of the divergence of a vector field over a volume is equal to the net outward flow of that property through the bounding surface.

66

© Faith A. Morrison, Michigan Tech U.



Mathematics Review Polymer Rheology

6. Vector and Tensor Theorems (*continued*)

**Leibnitz Rule** for differentiating integrals

constant limits  $\left\{ \begin{array}{l} I = \int_{\alpha}^{\beta} f(x, t) dx \\ \frac{dI}{dt} = \frac{d}{dt} \int_{\alpha}^{\beta} f(x, t) dx \\ = \int_{\alpha}^{\beta} \frac{\partial f(x, t)}{\partial t} dx \end{array} \right. \left. \begin{array}{l} \text{one} \\ \text{dimension,} \\ \text{constant} \\ \text{limits} \end{array} \right\}$

68  
© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

6. Vector and Tensor Theorems (*continued*)**Leibnitz Rule** for differentiating integrals

$$J = \int_{\alpha(t)}^{\beta(t)} f(x, t) dx$$

variable limits

$$\frac{dJ}{dt} = \frac{d}{dt} \int_{\alpha(t)}^{\beta(t)} f(x, t) dx$$

$$= \int_{\alpha(t)}^{\beta(t)} \frac{\partial f(x, t)}{\partial t} dx + \frac{d\beta}{dt} f(\beta, t) - \frac{d\alpha}{dt} f(\alpha, t)$$

one  
dimension,  
variable  
limits

69

© Faith A. Morrison, Michigan Tech U.

## Mathematics Review

Polymer Rheology

6. Vector and Tensor Theorems (*continued*)**Leibnitz Rule** for differentiating integrals

$$J = \iiint_{V(t)} f(x, y, z, t) dV$$

$$\frac{dJ}{dt} = \frac{d}{dt} \iiint_{V(t)} f(x, y, z, t) dV$$

$$= \iiint_{V(t)} \frac{\partial f(x, y, z, t)}{\partial t} dV + \iint_{S(t)} f(\mathbf{v}_{\text{surface}} \cdot \hat{\mathbf{n}}) dS$$

velocity of the surface element  $dS$

three  
dimensions,  
variable  
limits

70

© Faith A. Morrison, Michigan Tech U.

6. Vector and Tensor Theorems (continued)

**Substantial Derivative**

Consider a function  $f(x, y, z, t)$

true for any path:  $df \equiv \left(\frac{\partial f}{\partial x}\right)_{yzt} dx + \left(\frac{\partial f}{\partial y}\right)_{xzt} dy + \left(\frac{\partial f}{\partial z}\right)_{xyt} dz + \left(\frac{\partial f}{\partial t}\right)_{xyz} dt$

choose special path:  $\frac{df}{dt} \equiv \left(\frac{\partial f}{\partial x}\right)_{yzt} \frac{dx}{dt} + \left(\frac{\partial f}{\partial y}\right)_{xzt} \frac{dy}{dt} + \left(\frac{\partial f}{\partial z}\right)_{xyt} \frac{dz}{dt} + \left(\frac{\partial f}{\partial t}\right)_{xyz}$

time rate of change of  $f$  along a chosen path

$x$ -component of velocity along that path

When the chosen path is the path of a fluid particle, then these are the components of the particle velocities.

71

© Faith A. Morrison, Michigan Tech U.

6. Vector and Tensor Theorems (continued)

**Substantial Derivative**

When the chosen path is the path of a fluid particle, then the space derivatives are the components of the particle velocities.

$$\frac{df}{dt} \equiv \left(\frac{\partial f}{\partial x}\right)_{yzt} \frac{dx}{dt} + \left(\frac{\partial f}{\partial y}\right)_{xzt} \frac{dy}{dt} + \left(\frac{\partial f}{\partial z}\right)_{xyt} \frac{dz}{dt} + \left(\frac{\partial f}{\partial t}\right)_{xyz}$$

$$\left(\frac{df}{dt}\right)_{\text{along a particle path}} \equiv \left(\frac{\partial f}{\partial x}\right)_{yzt} v_x + \left(\frac{\partial f}{\partial y}\right)_{xzt} v_y + \left(\frac{\partial f}{\partial z}\right)_{xyt} v_z + \left(\frac{\partial f}{\partial t}\right)_{xyz}$$

$$\underline{v} \cdot \nabla f$$

**Substantial Derivative**

$$\left(\frac{df}{dt}\right)_{\text{along a particle path}} \equiv \frac{Df}{Dt} = \frac{\partial f}{\partial t} + \underline{v} \cdot \nabla f$$

72

© Faith A. Morrison, Michigan Tech U.