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Organic matter mineralization in sediment of a coastal freshwater lake and response to salinization

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Abstract

Solid phase and pore water chemical data collected in a sediment of the Haringvliet Lake are interpreted using a multi-component reactive transport model. This freshwater lake, which was formed as the result of a river impoundment along the southwestern coast of the Netherlands, is currently targeted for restoration of estuarine conditions. The model is used to assess the present-day biogeochemical dynamics in the sediment, and to forecast possible changes in organic carbon mineralization pathways and associated redox reactions upon salinization of the bottom waters. Model results indicate that oxic degradation (55%), denitrification (21%), and sulfate reduction (17%) are currently the main organic carbon degradation pathways in the upper 30 cm of sediment. Unlike in many other freshwater sediments, methanogenesis is a relatively minor carbon mineralization pathway (5%), because of significant supply of soluble electron acceptors from the well-mixed bottom waters. Although ascorbate-reducible Fe(III) mineral phases are present throughout the upper 30 cm of sediment, the contribution of dissimilatory iron reduction to overall sediment metabolism is negligible. Sensitivity analyses show that bioirrigation and bioturbation are important processes controlling the distribution of organic carbon degradation over the different pathways. Model simulations indicate that sulfate reduction would rapidly suppress methanogenesis upon seawater intrusion in the Haringvliet, and could lead to significant changes in the sediment's solid-state iron speciation. The changes in Fe speciation would take place on time-scales of 20–100 years.

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1. Introduction

The degradation of organic matter in sediments drives the release of nutrients and pollutants from sediments to surface waters, and can profoundly influence the biogeochemical cycling of C, N, O, S, P, Fe, Mn, and trace metals in aquatic environments (Hamilton-Taylor et al., 1996; Wetzel, 2001). Organic carbon (C_{org}) oxidation in sediments is coupled to the utilization of terminal electron acceptors (TEAs), primarily O₂, NO₃⁻, Mn-(hydr)oxides, Fe-(hydr)oxides, and SO₄²⁻. When these TEAs are completely consumed, degradation of C_{org} continues via meth-

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anogenesis. The corresponding C_{org} degradation reactions, often referred to as the primary redox reactions, roughly succeed one another vertically in the order of decreasing free energy yield (Froelich et al., 1979). In sediments receiving large inputs of reactive organic matter, however, the various mineralization processes may exhibit significant overlap (Wersin et al., 1991; Canfield et al., 1993; Holmer and Storkholm, 2001). The primary redox reactions also produce reduced species (e.g., NH₄⁺, Fe²⁺, H₂S, CH₄), which can participate in other, so-called secondary, redox reactions. The network of primary and secondary redox reactions usually leads to a characteristic zonation of redox conditions in sediments.

The relative importance of the different primary redox reactions depends on the availability of both the organic matter and the TEAs. Key determining factors are the

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input fluxes of C_{org} and TEAs from the overlying water column, organic matter quality, rates of physical transport of solids and solutes in the sediment, and rates of secondary redox reactions that regenerate or consume TEAs. In eutrophic lake sediments, TEAs are frequently in low supply relative to the influx of Corg. In these depositional settings, aerobic degradation of Corg may be limited by O2 consumption due to secondary oxygenation reactions, particularly the oxidation of CH₄ (Sweerts et al., 1991). Furthermore, reactive Fe(III) mineral phases are often preserved in fresh water sediments (Wersin et al., 1991; Gallon et al., 2004; Hyacinthe and Van Cappellen, 2004), while low SO₄²⁻ concentrations in freshwater environments limit sulfate reduction (Holmer and Storkholm, 2001). As a consequence, methanogenesis is generally a dominant Corg degradation process (Capone and Kiene, 1988; Peretyazhko et al., 2005). However, efficient recycling of TEAs may increase the importance of specific primary redox pathways, as observed for sulfate reduction (Urban et al., 1994) and dissimilatory iron reduction (Thomsen et al., 2004) in oligotrophic lake sediments.

Total organic carbon mineralization rates, and the relative contributions of the different primary redox reactions, can be estimated directly via incubation experiments (Canfield et al., 1993; Dauwe et al., 2001; Thomsen et al., 2004), or they can be quantified by applying reactive transport models (RTMs) to geochemical data sets. Multi-component RTMs have been used successfully to estimate kinetic parameters and rates of primary and secondary redox reactions (Van Cappellen and Wang, 1996). These models have mostly been applied to marine sediments, and less frequently to freshwater sediments (Van Cappellen and Wang, 1995; Furrer and Wehrli, 1996; van den Berg et al., 2000).

The focus of this study is to quantify the rates of organic carbon mineralization in the sediment of Haringvliet Lake (The Netherlands). Reaction rates are determined both experimentally and with a RTM calibrated with pore water and sediment chemistry data. In addition, the RTM is used to examine how biogeochemical cycling may change in response to salinization induced by restoration of estuarine conditions in the lake.

2. Study site

Haringvliet Lake is a eutrophic freshwater lake, which was created as a result of the damming of the mouth of an estuary in 1970 (Fig. 1), as part of the Dutch Delta Project (Ferguson and Wolff, 1984). Prior to dam construction, the Haringvliet was a tidal estuary and an outlet of the Meuse-Rhine river system to the North Sea. The closure of the Haringvliet caused physical and chemical changes in the water body, including the rapid conversion to a freshwater lake, increased shore-line erosion, and the accumulation of river derived suspended matter (Ferguson and Wolff, 1984; Smit et al., 1997; van Wijngaarden et al., 2002). The latter has negatively affected the benthic fauna, because of the high pollutant loading associated with sus-

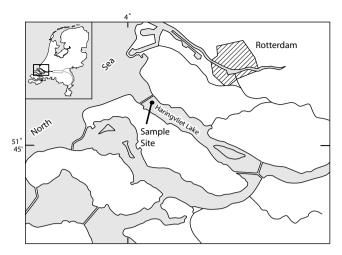


Fig. 1. The sampling location in Haringvliet Lake. The inset map shows The Netherlands with a box denoting the location of the detail section. The Rhine–Meuse river complex flows into the lake from the east, and the lake discharges through the dam at the western limit of the lake.

pended matter from the Rhine and Meuse (Reinhold-Dudok van Heel and den Besten, 1999). Thermal stratification and bottom water anoxia are not observed due to the shallow water depth and short residence time of water in the lake (Smit et al., 1997).

Current Dutch water management policy aims at the development of a broad range of tidal systems with a high ecological diversity (de Jonge and de Jong, 2002). Within the framework of this policy, a proposed partial restoration of estuarine conditions in the Haringvliet would begin in 2008 and be achieved by changing the opening and closing of the gates in the dam that separates the lake from the North Sea (Anonymous, 1998). The present study is part of a larger effort to assess how benthic biogeochemistry and ecology may respond to a possible future intrusion of seawater in the lake. We selected a location near the dam as our study site (Fig. 1), within the area that will be most impacted by salinization. This location is characterized by fine-grained sediments, which are the main reservoir of pollutants in the lake, as reported for other Rhine and Meuse-derived sediments in the Netherlands (van den Berg et al., 1999, 2001). The water depth at the sampling site is 7.5 m.

3. Methods

3.1. Sample collection

Field sampling was carried out in November 2001, September 2002, and April 2003. These sampling times are referred to in the text as fall, late-summer, and spring, respectively. Sediment was collected using a cylindrical box corer (31 cm i.d.) deployed from RV Navicula. Each box core contained approximately 40 cm of surface sediment and 30 cm of overlying water. Sub-cores were taken with polycarbonate tubes (10 cm i.d.). Sub-cores for pore water and solid phase analyses were taken from a single

box core. The sub-cores were immediately sectioned in a N_2 purged glove box on board the ship in a temperature-controlled laboratory. Sediment was centrifuged at 2500g for 10-30 min in polyethylene tubes to collect pore water.

3.2. Pore water analyses

After centrifugation, tubes were transferred to a N₂ purged glove box, the pore water was filtered through 0.2 or 0.45 µm pore size filters, and pH was measured immediately with an ion selective field effect transistor electrode (ISFET, Sentron). Pore water was then sub-divided and preserved for analysis in the laboratory. Sub-samples for NO₃⁻, NH₄⁺, Cl⁻, and SO₄²⁻ were stored frozen until analysis: NO₃⁻ and NH₄⁺ were determined colorimetrically on a nutrient auto-analyzer (Bran and Luebbe), Cl⁻ and SO₄²⁻ were determined by ion chromatography (Dionex DX-120). Sub-samples for total dissolved Mn and Fe were acidified with HNO₃ (50 µl conc. suprapur HNO₃ per ml) and stored at 4 °C until analysis by ICP-MS (Agilent 7500 series). Sub-samples for major constituents, such as Na⁺, were preserved with HNO₃ (10 μl conc. suprapur HNO₃ per ml) and stored at 4 °C until analysis by ICP-OES (Perkin Elmer Optima 3000).

During the spring and late-summer sampling, sulfide (Cline, 1969) and alkalinity (Sarazin et al., 1999) were determined on board the ship colorimeterically using a UV–Vis spectrophotometer (Unicam UV1). Sub-samples for sulfide analysis included a base preservative (10 μ l 1 M NaOH per ml). A sulfide pore water profile was also measured in late-summer using the Diffusive Gradient in Thin Films (DGT) method (Teasdale et al., 1999; Naylor et al., 2004). With this method, sulfide is determined by quantifying the color change resulting from the reaction of a AgI (yellow) containing gel with pore water sulfide, producing AgS2 (black). Sulfide concentrations in the pore water were calculated using the calibration of Naylor et al. (2004).

During fall sampling, dissolved inorganic carbon (DIC) was measured as the difference of total and organic dissolved carbon. The latter was measured with a Shimadzu TOC-5050A analyzer. Dissolved oxygen microprofiles were obtained on board using a Clark-type oxygen sensor with an internal reference and a guard cathode (Revsbech, 1989) attached to a micromanipulator. Perspex cores (4.2 cm i.d.) with 10 cm sediment and 5 cm overlying water were collected from a box core. The surface of each core was sparged with air and profiling was completed within 30 min of core retrieval.

3.3. Solid phase analyses

The water content and density of the sediment were determined from the weight loss upon freeze drying. Grain size was measured using a laser diffraction technique (Malvern Mastersizer S) on freeze dried sediment, after HCl and $\rm H_2O_2$ pre-treatment. Total carbon, total sulfur, and

organic carbon (following carbonate removal with 1 M HCl) were determined on freeze-dried sediments using an elemental analyzer (LECO SC-1440H). Total Mn and Fe were determined by ICP-MS after HF-HClO₄-HNO₃ digestion of freeze dried sediment as described in Hyacinthe and Van Cappellen (2004). Near-neutral pH ascorbate extractions were performed on wet sediment following the procedure of Hyacinthe and Van Cappellen (2004). This extraction releases the most chemically reactive reducible pool of Mn and Fe (Kostka and Luther, 1994; Hyacinthe and Van Cappellen, 2004).

Acid volatile sulfide (AVS) was determined by the method described in van den Berg et al. (1998), with some modifications. Approximately 1 g of wet sediment was transferred to a reaction vessel in an Ar filled glove bag. The reaction vessel was weighed and then attached to an Ar purged analysis train. Samples were acidified with 10 ml 6 M HCl and purged for 1 h. The H₂S released from the sample was trapped in a 1 M NaOH solution and determined colorimetrically (Cline, 1969).

Chloropigments were extracted from wet sediment with 90% acetone, at a 1:2 sediment to solvent ratio. Sediments were mixed with a vortex stirrer and sonicated for 10 min (Sun et al., 1991). Following sonication, the extractant was collected by centrifugation and stored at 0 °C until analysis. Determination of Chlorophyll-a (Chl-a) and Pheophytin-a (Pheo-a) in the extracts was performed spectrophotometrically (APHA, 1985). Solid phase data presented are from the late-summer sampling unless otherwise indicated.

3.4. Rate measurements

Rates of total carbon mineralization were determined by monitoring CO₂ accumulation in the headspace of oxic and anoxically incubated slurries, following the procedure of Dauwe et al. (2001). Slurries containing approximately 20 ml wet sediment and 10 ml filtered, de-oxygenated lake water were placed in 100 ml glass vials sealed with rubber septa. The vials were shaken and the headspace was purged for 10 min with either air for oxic incubations, or N₂ for anoxic incubations. The purging procedure was repeated three times for each vial. The CO₂ concentration in the headspace was monitored using gas chromatography. Potential rates of denitrification and sulfate reduction were determined using flow-through reactors (FTRs), following methods described in detail elsewhere (Roychoudhury et al., 2003; Pallud and Van Cappellen, 2006).

4. Model formulation

The model presented in this paper follows the general approach outlined in Van Cappellen and Wang (1996); this section therefore focuses on the implementation of processes described in more recent studies, and the derivation of parameter values and boundary conditions from field data. The reaction-transport model calculations were carried out

with the Biogeochemical Reaction Network Simulator (BRNS), a flexible modeling environment for one-dimensional simulations (Regnier et al., 2003; Aguilera et al., 2005; Jourabchi et al., 2005). In the BRNS, the chemical species, reaction stoichiometries, kinetic parameters, boundary conditions, and transport parameters are specified by the user through a MAPLE software or web-based interface (Chilakapati, 1995; Amberg et al., 1999; Regnier et al., 2002, 2003). An executable program, which consists of a set of standard routines for iteratively solving the reaction and transport equations, is then generated automatically. The model output consists of the species concentrations, reaction rates, and fluxes as a function of depth. Both steady-state and transient simulations can be performed.

4.1. Species and reactions

The model developed here considers 24 chemical species (Table 1) and 32 reaction pathways (Table 2). The mineralization of organic carbon is modeled using the multi-G approach (Westrich and Berner, 1984). Three pools of organic carbon are included in the model: OM1, the most reactive $C_{\rm org}$ fraction, OM2, a less reactive fraction, and OM3, the non-reactive or refractory pool. The decomposition kinetics are first-order and controlled by the rate constants, $k_{\rm OM1}$ and $k_{\rm OM2}$. To account for increased degradation efficiencies of $C_{\rm org}$ under oxic versus anoxic conditions (e.g. Hedges and Keil, 1995; Kristensen, 2000; Dauwe et al., 2001; Bastviken et al., 2004; Meile and Van Cappellen, 2005), a dimensionless acceleration factor (accel) is included (Table 2).

Total C_{org} decomposition is distributed over the different degradation pathways following the approach of Van Cappellen and Wang (1996). This approach is based on a Michaelis–Menten kinetic formulation for the utilization of the TEAs, where a set of limiting concentration values (K_m) determines the fractions (f_{TEA}) of total C_{org} occurring

Table 1 Solutes and solids included in the model and their boundary conditions at the sediment surface

$\mu \mathrm{mol}~\mathrm{cm}^{-2}~\mathrm{yr}^{-1}$
630
315
546
4.2
₃ A 14.7
2.1
₃ B 23.1
0
0
0

Solute concentrations are determined experimentally or estimated, solid fluxes are derived from model fitting (see Section 4.3).

via the various degradation pathways. The redox zonation and overlap between primary redox processes has been successfully reproduced for a variety of subsurface environments using this approach (Van Cappellen and Wang, 1995, 1996; Hunter et al., 1998; Berg et al., 2003; Fossing et al., 2004).

The rate parameters controlling $C_{\rm org}$ decomposition $(k_{\rm OM1}, k_{\rm OM2}, {\rm and accel})$ were constrained by the experimental rate measurements and the model fits (Table 3). Initial guesses of the parameter values were based on the global relationships reported by Tromp et al. (1995). The value of the acceleration factor imposed in the model calculations (accel = 25) falls in between that obtained from the ${\rm CO_2}$ production rates in oxic versus anoxic slurry incubations (oxic:anoxic = 17), and the maximum potential rates of denitrification and sulfate reduction measured in FTRs on intact sediment slices (denitrification:sulfate reduction = 34). The $K_{\rm m}$ values of Van Cappellen and Wang (1995) were used, except for dissimilatory iron reduction, for which a higher $K_{\rm m}$ value had to be imposed to reproduce the limited microbial reduction of iron in the sediment.

In sediments, the build-up of methane may result in the formation of gas bubbles. This process is simulated using the approach of Martens et al. (1998), where methanogenesis produces $CH_4(aq)$ until the pore water concentration equals the saturation concentration. Further methanogenesis then produces $CH_4(g)$. A unitless parameter, f_m , is introduced to switch between $CH_4(aq)$ and $CH_4(g)$ production (R12 and R13, Table 2):

$$f_{\rm m} = 1 - \frac{1}{(1 + {\rm e}^{\delta})}$$
 with $\delta = S_{\rm m} ({\rm CH}_4({\rm aq}) - {\rm CH}_4^*),$ (1)

where $\mathrm{CH_4}^*$ is the methane solubility (mM) and S_{m} (mM $^{-1}$) is an adjustable parameter. This formulation insures that the value of f_{m} rapidly approaches 1 when $\mathrm{CH_4}(\mathrm{aq}) > \mathrm{CH_4}^*$, and 0 when $\mathrm{CH_4}(\mathrm{aq}) < \mathrm{CH_4}^*$. The use of a continuous f_{m} function Eq. (1) avoids numerical oscillations in model output. It is assumed that $\mathrm{CH_4}(\mathrm{g})$ is transported to the sediment–water interface (SWI) without further reaction in the sediment. For the sake of simplicity, effects of gas production on porosity and compaction are not considered in the model.

All secondary redox reactions are assigned bimolecular rate laws (Table 2). As in Berg et al. (2003), two pools of reactive Mn and Fe oxides are considered. The first, or bioavailable, pool can be reduced microbially as well as chemically, while the second pool can only be reduced chemically. Chemical reduction of reactive Mn and Fe oxides by sulfide is assumed to yield SO_4^{2-} as the final oxidized S-species (R22–R25, Table 2). That is, intermediate sulfur species are assumed to be short-lived (Elsgaard and Jørgensen, 1992) and are not represented explicitly. Initial values of secondary reaction rate constants were obtained from previous studies (Table 3), and then adjusted to obtain better fits to the field data. In particular, the values of $k_{\rm tsmn}$, $k_{\rm tsfe}$, and $k_{\rm ch4so4}$ used here are lower than reported previously.

a pH units.

Table 2 The reaction network and kinetic formulations used in the model

Description	Reaction	Kinetic or equilibrium formulation	Reaction number
Primary redox reactions ^{a,b}			
Aerobic respiration ^c Denitrification ^c Mn oxide reduction Fe oxide reduction Sulfate reduction Methanogenesis-(aq) ^d Methanogenesis-(g) ^d	$\begin{array}{l} OM + xO_2 + (-y + 2z)HCO_3 \rightarrow (x - y + 2z)CO_2 + yNH_4^+ + zHPO_4^{2-} + (x + 2y + 2z)H_2O \\ OM + 0.8xNO_3^- \rightarrow 0.4xN_2 + (0.2x - y + 2z)CO_2 + (0.8x + y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} + (0.6x - y + 2z)H_2O \\ OM + 2xMnO_2 + (3x + y - 2z)CO_2 + (x + y - 2z)H_2O \rightarrow 2xMn^{2+} + (4x + y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} \\ OM + 4xFe(OH)_3 + (7x + y - 2z)CO_2 \rightarrow 4xFe^{2+} + (8x + y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} + (3x + y - 2z)H_2O \\ OM + 0.5xSO_4^{2-} + (y - 2z)CO_2 + (y - 2z)H_2O \rightarrow 0.5xH_2S + (x + y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} \\ OM + (y - 2z)H_2O \rightarrow 0.5xCH_4(aq) + (0.5x - y + 2z)CO_2 + (y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} \\ OM + (y - 2z)H_2O \rightarrow 0.5xCH_4(g) + (0.5x - y + 2z)CO_2 + (y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} \\ OM + (y - 2z)H_2O \rightarrow 0.5xCH_4(g) + (0.5x - y + 2z)CO_2 + (y - 2z)HCO_3^- + yNH_4^+ + zHPO_4^{2-} \\ \end{array}$	$f_{\rm O_2} \; k_{ m OM1} \; [m OM1] \; accel$ $f_{ m NO_3} \; k_{ m OM1} \; [m OM1] \; accel$ $f_{ m MnO_2} \; k_{ m OM1} \; [m OM1]$ $f_{ m Fe(OH)_3} \; k_{ m OM1} \; [m OM1]$ $f_{ m SO_4} \; k_{ m OM1} \; [m OM1]$ $f_{ m OM} \; k_{ m OM1} \; [m OM1] f_{ m m}$ $f_{ m OM} \; k_{ m OM2} \; [m OM2] \; (1-f_{ m m})$	R1, R7 R2, R8 R3, R9 R4, R10 R5, R11 R6, R12 R13
Secondary redox reactions NH ₄ ⁺ oxidation by O ₂ H ₂ S oxidation by O ₂ FeS oxidation by O ₂ Mn ²⁺ oxidation by O ₂ Fe ²⁺ oxidation by O ₂ CH ₄ oxidation by O ₂ Fe ²⁺ oxidation by Mn oxide CH ₄ oxidation by SO ₄ ²⁻ H ₂ S oxidation by Mn oxide ^e H ₂ S oxidation by Fe oxide ^e	$\begin{array}{l} NH_4^{\ +} + 2O_2 + 2HCO_3^{\ -} \rightarrow NO_3^{\ -} + 2CO_2 + 3H_2O \\ H_2S + 2O_2 + 2HCO_3^{\ -} \rightarrow SO_4^{\ 2^-} + 2CO_2 + 2H_2O \\ FeS + 2O_2 \rightarrow SO_4^{\ 2^-} + Fe^{2+} \\ Mn^{2+} + 0.5O_2 + 2HCO_3^{\ -} \rightarrow MnO_2 + 2CO_2 + H_2O \\ Fe^{2+} + 0.25O_2 + 2HCO_3^{\ -} + 1/2H_2O \rightarrow Fe(OH)_3 + 2CO_2 \\ CH_4 + O_2 \rightarrow CO_2 + H_2O \\ 2Fe^{2+} + MnO_2 + 2HCO_3^{\ -} + 2H_2O \rightarrow 2Fe(OH)_3 + Mn^{2+} + 2CO_2 \\ CH_4 + SO_4^{\ 2^-} + CO_2 \rightarrow H_2S + 2HCO_3^{\ -} \\ H_2S + 6CO_2 + 4MnO_2 + 2H_2O \rightarrow 4Mn^{2+} + SO_4^{\ 2^-} + 6HCO_3^{\ -} \\ H_2S + 14CO_2 + 8FeOH_3 \rightarrow 8Fe^{2+} + SO_4^{\ 2^-} + 14HCO_3^{\ -} + 6H_2O \end{array}$	$k_{ m nh4ox}[{ m NH_4}^+][{ m O_2}]$ $k_{ m tsox}[{ m H_2S}][{ m O_2}]$ $k_{ m fesox}[{ m FeS}][{ m O_2}]$ $k_{ m mox}[{ m Mn}^{2+}][{ m O_2}]$ $k_{ m feox}[{ m Fe}^{2+}][{ m O_2}]$ $k_{ m ch4ox}[{ m CH_4}][{ m O_2}]$ $k_{ m ch4ox}[{ m CH_4}][{ m SO_4}^{2-}]$ $k_{ m tsmn}[{ m H_2S}][{ m MnO_2}]$ $k_{ m tsin}[{ m H_2S}][{ m MnO_2}]$ $k_{ m tsin}[{ m H_2S}][{ m CO}_3]$	R14 R15 R16 R17 R18 R19 R20 R21 R22, R23 R24, R25
Adsorption and equilibrium read	ctions		
NH ₄ ⁺ adsorption Carbonate equilibria Sulfide equilibrium	$\mathrm{NH_4}^+ \leftrightarrow \mathrm{NH_4}^+$ ads $\mathrm{H}^+ + \mathrm{HCO_3}^- \leftrightarrow \mathrm{CO_2} + \mathrm{H_2O}$ $\mathrm{CO_3}^{2-} + \mathrm{H}^+ \leftrightarrow \mathrm{HCO_3}^-$ $\mathrm{H}^+ + \mathrm{HS}^- \leftrightarrow \mathrm{H_2S}$	K _N [NH ₄ ⁺] Keqc1 Keqc2 Keqs	R26 R27 R28 R29
Precipitation and dissolution red	actions (non-redox)		
FeS dissolution ^f FeS precipitation ^g Pyrite precipitation	$FeS + 2H^{+} \rightarrow Fe^{2+} + H_{2}S$ $Fe^{2+} + H_{2}S \rightarrow FeS + 2H^{+}$ $FeS + H_{2}S \rightarrow FeS_{2} + H_{2}$	kfesdis [FeS] $(1 - \Omega \text{FeS})$ kfespre $(\Omega \text{FeS} - 1)$ Kpyrpre [FeS] [H ₂ S]	R30 R31 R32

Reaction parameters are defined in Table 3.

^a OM = $(CH_2O)_x(NH_3)_y(H_3PO_4)_z$, where x, y, z represent the CNP ratios given in Table 3. ^b For reactions R1–R6 k_{OM1} and CNP_{OM1} are used, for R7–R13 k_{OM2} and CNP_{OM2} are used; the f_{TEA} terms are the fractions of total carbon mineralization assigned to the different TEA pathways.

The term $f_{\rm m}$ is defined by Eq. (1), and controls the switching between R12 and R13, $f_{\rm m}$ is not included in R6 which does not produce methane in excess of saturation in this system.

e R23 with MnO₂B, R25 with Fe(OH)₃B.

^f $\Omega \text{FeS} = \text{Fe}^{2+} \text{H}_2 \text{S}/(\text{H}^+)^2 \text{ Kfes, R} 30 = 0 \text{ when } \Omega \text{FeS} > 1.$

g R31 = 0 when $\Omega \text{FeS} < 1$.

Table 3
Reaction parameter values used in the model

Parameter	Value	Unit	Source	Ref.	Description
Primary redox	reactions				
k_{OM1}	1	yr^{-1}	C, M		Degradation rate constant OM1
k_{OM2}	0.01	yr^{-1}	C, M		Degradation rate constant OM2
k_{OM3}	0	yr^{-1}	M		OM3 not reactive
accel	25	_	M, C		Acceleration factor: R1–R2
f_{TEA}	0-1	_	M		Fraction of total OM degradation by each TEA pathway
CNP _{OM1}	112:20:1	_	C, L	1	CNP for OM1 (highly reactive)
CNP _{OM2}	200:20:1	_	C		CNP for OM2 (less reactive)
$K_{\rm m}$ O ₂	8	μM	L	2	Limitation for oxic respiration
$K_{\rm m}~{\rm NO_3}^-$	10	μM	L	2	Limitation for denitrification
$K_{\rm m}~{\rm MnO_2}$	16	$\mu mol g^{-1}$	L	3	Limitation for Mn reduction
$K_{\rm m}$ FeOH ₃	200	$\mu mol g^{-1}$	M		Limitation for Fe reduction
$K_m SO_4^{2-}$	100	μΜ	C, L	2	Limitation for SO ₄ ²⁻ reduction
CH ₄ *	2.66	mM	I		Saturation conc. at study site
$f_{ m m}$	0-1	_	M	4	Methane switch (see Eq. (1))
$S_{ m m}$	3.0	$\mathrm{m}\mathrm{M}^{-1}$	M, L	4	Methane switch (see Eq. (1))
Secondary redo.	x reaction		Range from	1 (2,3,5,6)	
knh4ox	2×10^{1}	$\mu\mathrm{M}^{-1}~\mathrm{yr}^{-1}$	$5-7.9 \times 10^{1}$		R14, nitrification
ktsox	1×10^{3}	$\mu M^{-1} \text{ yr}^{-1}$	1.6×10^{-1}		R15, sulfide oxidation by O_2
kfesox	2×10^{1}	$\mu M^{-1} \text{ yr}^{-1}$	1.9×10^{-1}	2×10^{1}	R16, FeS oxidation by O ₂
kmnox	1.0	$\mu M^{-1} \text{ yr}^{-1}$	3.5×10^{-1}		R17, Mn^{2+} oxidation by O_2
kfeox	5×10^{1}	$\mu M^{-1} \text{ yr}^{-1}$	3.5×10^{-1}	1.6×10^4	R18, Fe^{2+} oxidation by O_2
kch4ox	1×10^{4}	$\mu M^{-1} \text{ yr}^{-1}$	1×10^{4}		R19, methane oxidation by O_2
kfemn	1×10^{-1}	$\mu M^{-1} \text{ yr}^{-1}$	2.4×10^{-3}	3	R20, Fe ²⁺ oxidation by Mn-oxides
kch4so4	1×10^{-4}	$\mu\mathrm{M}^{-1}~\mathrm{yr}^{-1}$	$1 \times 10^{-2} - 1$		R21, methane oxidation by SO_4^{2-}
ktsmn	7.5×10^{-3}	$\mu M^{-1} \text{ yr}^{-1}$	1×10^{-2} -6.	3×10^{-1}	R22, R23 sulfide oxidation by Mn-oxides
ktsfe	2.5×10^{-3}	$\mu\mathrm{M}^{-1}~\mathrm{yr}^{-1}$	$8 \times 10^{-3} - 9$.	5×10^{-2}	R24, R25 sulfide oxidation by Fe-oxides, see also (7)
Adsorption, equ	ilibrium, dissolution,	and precipitation const	ants		
$K_{\mathbf{N}}$	1.4	_	L	3	Ammonium adsorption constant
Keqc1	3.0×10^{-7}	_	I	8	Carbonate equilibrium constant
Keqc2	3.6×10^{-13}	_	I	8	Bicarbonate equilibrium constant
Keqs	6.3×10^{-8}	_	I	9	Sulfide equilibrium constant
Kfes	9.6×10^{3}	_	L	10	FeS stability constant
kfespre	1.5×10^{-3}	$\text{mol g}^{-1} \text{ yr}^{-1}$	M		FeS Precipitation rate constant
kfesdis	1.0×10^{-3}	yr^{-1}	L	3	FeS dissolution rate constant
Kpyrpre	3.3×10^{-3}	$\mu\mathrm{M}^{-1}~\mathrm{yr}^{-1}$	L	11	FeS ₂ precipitation rate constant

The source of the parameter values are indicated by the following code: C, constrained from experimental data; M, derived by model fitting; I, independently determined from field data; L, literature value, with references given at the bottom of the table. A range of literature values for the secondary reaction rate constants is provided.

Ref.: 1. Koelmans (1998); 2. Van Cappellen and Wang (1995); 3. Van Cappellen and Wang (1996); 4. Martens et al. (1998); 5. Berg et al. (2003); 6. Fossing et al. (2004); 7. Poulton et al. (2004); 8. Cai and Wang (1998); 9. Pilson (1998); 10. Davison et al. (1999); 11. Rickard (1997).

The rates of FeS dissolution and precipitation (R30–R31, Table 2) are dependent on the degree of FeS under- or supersaturation of the pore water, using the formulations of Van Cappellen and Wang (1996). Formation of pyrite (FeS₂) is described as a reaction of FeS and H₂S, using the bimolecular rate equation of Rickard (1997). Dissolution of pyrite is not included in the model.

Adsorption of $\mathrm{NH_4}^+$ to cation exchange sites is represented by a linear equilibrium isotherm, with a constant adsorption coefficient, K_{N} . The model further includes homogenous carbonate and sulfide equilibrium reactions (R27–R29), which are assumed to be the major aqueous pH buffers in this system. The concentration of H^+ is explicitly computed from the equilibrium conditions (Jourabchi et al., 2005). Reactions with sulfide are written with $\mathrm{H_2S}$ as the reactive species, however the inclusion of the $\mathrm{H_2S}$ dissociation equilibrium

(R29) means that both H₂S and HS⁻ species concentrations respond to sulfide producing and consuming reactions.

4.2. Transport

Solute transport processes included are molecular diffusion, bioirrigation, bioturbation, and sediment advection, while solid species are transported by bioturbation and sediment advection. Molecular diffusion coefficients at 0 °C and temperature correction factors are taken from Van Cappellen and Wang (1995), and references therein, and corrected for tortuosity effects after Boudreau (1996). Porosity, φ (cm³ cm⁻³), varies with depth as defined by the equation given in Table 4 and shown in Fig. 2. The advection velocity accounts for the variations in porosity (Berner, 1980).

Table 4
Depth distributions and parameter values for physical properties and transport processes

Depth distributions	Description
$\varphi(x) = \varphi_{\infty} + (\varphi_0 - \varphi_{\infty})e^{-(\tau x)}$	Porosity distribution (Fig. 2)
$\alpha = \begin{cases} \alpha_0 (1 - e^{(x-17)})(x \le 17 \text{ cm}) \\ 0(x > 17 \text{ cm}) \end{cases}$	Distribution of bioirrigation coefficient α (Fig. 3)
$D_{\mathbf{b}} = D_{\mathbf{b}}(0) \mathbf{e}^{-(\mathbf{x}/\lambda)}$	Distribution of bioturbation coefficient $D_{\rm b}$ (Fig. 4)

Parameter definitions and values

Parameter	Value	Unit	Source	Description
φ_0	0.89	$\mathrm{cm^3cm^{-3}}$	Measured	Porosity at SWI
$arphi_\infty$	0.79	$\mathrm{cm}^3\mathrm{cm}^{-3}$	Measured	Porosity at infinite depth
τ	0.2	cm^{-1}	Data fitting	Porosity attenuation
X	0-30	cm	Measured	Sediment depth
ω	1.0	cm yr ⁻¹	Literature ^a	Sediment accumulation rate at SWI
α	0-10	yr^{-1}	Data fitting	Bioirrigation coefficient
α_0	10	yr^{-1}	Data fitting	Value of α at SWI
D_{b}	0-5	$cm^2 yr^{-1}$	Data fitting	Bioturbation coefficient
$D_{\rm b}0$	5	$cm^2 yr^{-1}$	Data fitting	Value of D_b at SWI
λ	2.5	cm	Data fitting	$D_{\rm b}$ attenuation
ho	2.1	$\mathrm{g~cm}^{-3}$	Measured	Sediment density
Temperature	12	°C	Measured	Mean sediment temperature

^a van Wijngaarden et al. (2002).

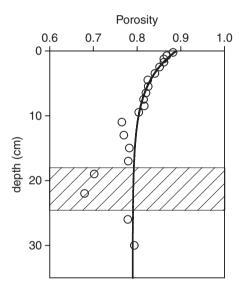


Fig. 2. Depth distribution of sediment porosity in late-summer. The solid line is the exponential fit used to represent porosity in the model (see equation in Table 4). The shaded area between approximately 18 and 24 cm depth denotes a zone of coarser-grained sediment.

The pore water profiles of many species, including the conservative ions Na⁺ and Cl⁻, show evidence of bioirrigation (Fig. 3). As can be seen in Fig. 3, the concentrations of Na⁺ and Cl⁻ increase with depth below 17 cm. It is unlikely that these concentration profiles reflect the ongoing replacement of remnant saline pore waters by freshwater. The age of the lake (created in 1970) and the sedimentation rate (~1 cm yr⁻¹, see below), imply that the sediment in the upper 30 cm was deposited in freshwater conditions. The increasing salinity in the lower half of the cores thus indicates salt diffusion from a deeper source, probably related to subterranean seawater intrusion. The near-constant

concentrations of Na⁺ and Cl⁻ in the upper 17 cm then require enhanced pore water transport to counteract the upward salt diffusion. This enhanced pore water transport is attributed to bioirrigation.

The depth distribution of the bioirrigation coefficient α (Table 4) was derived by fitting the Na⁺ and Cl⁻ profiles to the steady state diffusion-irrigation equation, with the concentrations at the SWI and at 30 cm depth fixed to the measured values. Note that this approach yields a minimum estimate of the irrigation intensity. The selected form of the depth distribution (Fig. 3c, Table 4) produced a better fit to the pore water Na⁺ and Cl⁻ profiles than a linearly or exponentially attenuating bioirrigation coefficient distribution. It is also preferred over the simpler step-function distribution, as it avoids a sharp discontinuity of α at the bottom of the irrigated zone. The value of α_0 obtained (10 yr⁻¹) is similar to irrigation coefficients reported for freshwater sediment microcosms inhabited by deposit feeding tubificid worms (5–10 yr⁻¹, Wang and Matisoff, 1997), at comparable population densities as those found by Smit et al. (1995) in fine-grained Haringvliet Lake sediments (in the order of 10^3 organisms m⁻²).

All solutes are assigned the bioirrigation coefficient distribution shown in Table 4, except Mn^{2+} and Fe^{2+} . Net vertical transport of Mn^{2+} and Fe^{2+} by irrigation is strongly impeded, because these pore water species oxidatively precipitate near flushed burrow walls, and are therefore prevented from escaping via the burrows (Berg et al., 2003; Meile et al., 2005). The value of α for Fe^{2+} is reduced by 100% (no bioirrigation) while α for Mn^{2+} is reduced by 40%. The reduced α values produce modeled pore water profiles that are consistent with the data. The variable adjustments to the irrigation coefficients of Mn^{2+} and Fe^{2+} are also in agreement with Berg et al. (2003) who found that, in contrast to Fe^{2+} , pore water distributions

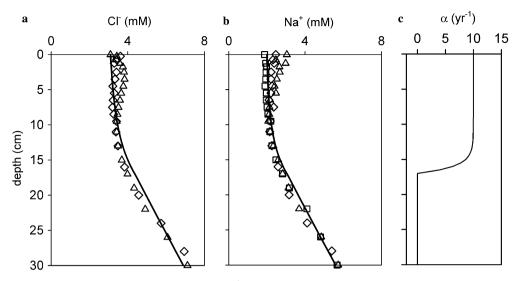


Fig. 3. Pore water profiles of Cl^- in (a) fall (\diamondsuit) and spring (\triangle), and Na^+ in (b) fall (\diamondsuit), late-summer (\square) and spring (\triangle). The solid lines represent a model fit for fixed boundary concentrations (at 0 and 30 cm), and the bioirrigation distribution given in Table 4. The depth distribution of the irrigation coefficient α is depicted in panel (c).

of Mn²⁺ show evidence of transport by irrigation, most likely because of slower oxidation rates compared to Fe²⁺.

Particle mixing is represented as a diffusion process (Berner, 1980). It results mainly from the activity of benthic macrofauna (bioturbation), although some effect of sediment resuspension cannot be excluded at the shallow water depth of the sampling site (7.5 m). The bioturbation coefficient, D_b (cm² yr⁻¹) is defined by an exponentially decaying depth distribution (Table 4; Wijsman et al., 2002). The magnitude and depth distribution of the biodiffusion coefficient were constrained by fitting the measured profiles of Pheo-a, a breakdown product of Chl-a (Fig. 4). Sediment profiles of Chl-a have been previously used to quantify sediment mixing (e.g. Sun et al., 1994; Boon and Duineveld,

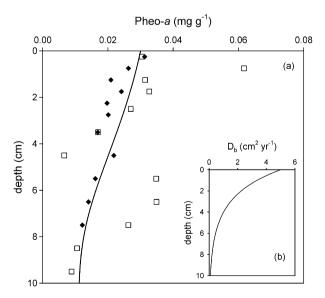


Fig. 4. Pheo-a sediment profiles for fall (\blacklozenge) and late-summer (\Box). The solid line in (a) is the modeled fall Pheo-a distribution obtained using the $D_{\rm b}$ depth distribution depicted in the inset (b). The $D_{\rm b}$ depth distribution is given in Table 4.

1998; Wijsman et al., 2002). The depth distribution of D_b was obtained assuming steady state and a degradation rate constant of 0.05 yr^{-1} for Pheo-a (Table 4, Fig. 4b). A major source of uncertainty in this estimation is the value of the degradation rate constant imposed in the calculations. For refractory Pheo-a in marine sediments the reported values exhibit a considerable range, from 0.002 to 0.15 yr^{-1} (Stephens et al., 1997). Bioturbation is described as a diffusion process for the sake of simplicity; however, actual sediment mixing processes may be more complex as evidenced by the pigment data from late-summer (Fig. 4) which suggests non-local sediment transport.

4.3. Boundary conditions

Upper boundary conditions for solutes and solids at the SWI are summarized in Table 1. All chemical species are assigned a zero concentration gradient as lower boundary condition. The model depth (100 cm) extends well below the depth interval examined in this study (0–30 cm), to minimize computational artifacts associated with the lower boundary conditions.

In the absence of direct measurements, initial estimates of particulate depositional fluxes were derived from suspended matter concentrations and the sedimentation rate. The latter was estimated at 1 cm yr⁻¹, based on the radiometric age determinations of van Wijngaarden et al. (2002). The initial flux estimates were then adjusted by trial and error to fit measured concentration profiles. The deposition fluxes of Mn and Fe oxides were adjusted to optimize the simultaneous fit of the concentration distributions of both solid-phase and pore water Mn and Fe. The model-calculated pore water O₂ distribution is particularly sensitive to the deposition flux of the most reactive organic matter, OM1. Hence, the measured O₂ microprofiles were used primarily to constrain the flux of OM1. The pore water

profiles of NH₄⁺ and DIC were used in a similar manner to determine the flux of OM2. Once the fluxes of OM1 and OM2 were fixed, the flux of non-reactive organic matter, OM3, was adjusted to reproduce the measured total organic carbon concentrations.

5. Results

Sediment porosity approached 90% at the SWI, and decreased near-exponentially with depth to values of around 80% (Fig. 2). The anomalously low porosities in depth interval 18–24 cm corresponded to an increase in sediment grain size (not shown). This change in sediment grain size may be the result of lake shore erosion. Concentrations of $C_{\rm org}$, total Fe, and total Mn were also lower in the 18–24 cm depth range due to dilution by coarser grained sediment (Figs. 5 and 6).

The particulate C_{org} concentration profile shows little change with depth in the upper 18 cm of sediment, suggesting that the major part of organic matter is refractory (Fig. 5). The profiles of total Mn and Fe do not exhibit distinct changes with depth. However, the concentrations of easily reducible Mn_{asc} and Fe_{asc} pools were highest near the SWI and declined with depth (Fig. 6). Reactive Mn_{asc} represented approximately 45% of the total Mn concentration near the SWI, while Fe_{asc} represented less than 20% of total Fe near the SWI. AVS concentrations were lower in spring than in late-summer in depth interval 4–15 cm. In late-summer, AVS accounted for 22–48% of the total sulfur measured below 4 cm depth (Fig. 7).

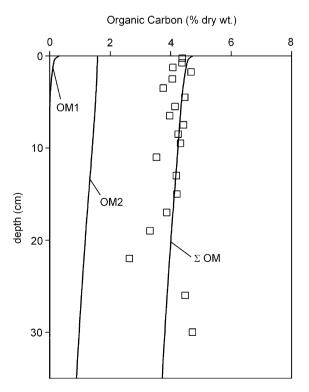


Fig. 5. Depth distribution of the measured total organic carbon (\square), and model distributions of the reactive organic carbon pools OM1, OM2, and the sum of the three OM pools (Σ OM) (solid lines).

Pore water O2 and NO3 were depleted within the uppermost centimeter of sediment (Fig. 8), implying high rates of oxygen and nitrate reduction. Dissolved Mn concentrations exhibited a subsurface peak at approximately 3 cm. The peak in dissolved Mn concentrations was greater in spring than at the other two sampling dates. The concentrations of dissolved Fe were fairly constant in the upper 13 cm and then increased steadily with depth. Measurable pore water concentrations of sulfate persisted down to 20 cm depth in fall. In spring and late-summer, the penetration depth of $SO_4^{\ 2-}$ was shallower, although in late-summer concentrations of approximately 60 µM were measured between 5 and 17 cm depth. Colorimetric sulfide analysis of centrifuged pore water never resulted in detectable concentrations. The sulfide pore water profile obtained with the AgI DGT probe gave S(-II) concentrations in the range of 5-10 μM in the 2-10 cm depth interval. Concentrations of NH₄⁺ and alkalinity increased with depth, providing evidence that Corg mineralization occurred at least down to 30 cm. Pore water pH was most variable in the upper 10 cm of sediment; below this depth pH values displayed a gradually decreasing trend with depth.

Experimentally determined rates of carbon mineralization in oxic slurries were systematically higher than those of anoxic slurries (Table 5). The average rate of CO₂ production observed in anoxic slurries was 17 times less than that found in oxic slurries. Potential rates of denitrification were approximately 34 times greater than potential rates of sulfate reduction measured with FTRs from the upper 4 cm of sediment. All methods yielded rates that varied with the sampling date, and depth, but also between duplicates. Despite the observed variability (Table 5), the data implied that aerobic respiration and denitrification produced much higher rates of carbon mineralization than other, anoxic degradation pathways.

6. Discussion

A fully transient simulation of the seasonal variations in sediment biogeochemistry proved unfeasible, primarily because the temporal evolution of the boundary conditions at the SWI could not be accurately constrained. This particularly holds for the input fluxes of reactive organic matter (OM1, OM2) and reactive Fe and Mn phases. In addition, with the notable exceptions of Mn²⁺ and SO₄²⁻, the overall trends of the pore water profiles did not vary greatly among the sampling times (Fig. 8). Therefore, we opted for a modeling strategy aimed at reproducing the general features of the solid-phase and pore water distributions.

The solid curves in Figs. 5–8 represent the output of a steady-state solution of the model fitted to match the entire set of chemical data collected. As can be seen, the model is able to simultaneously reproduce the majority of observed trends in the concentration profiles. It is important to note that in the model calculations, the transport rates are obtained independently from the fitted data set in Figs. 5–8 (Section 4.2). Taken together, the model appears to provide a reasonable,

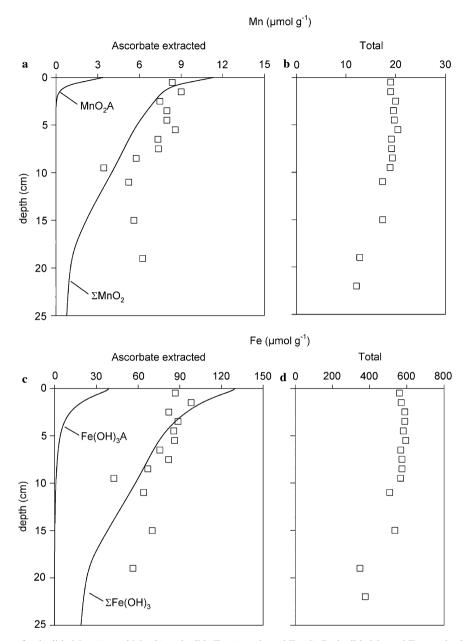


Fig. 6. Depth distributions of reducible Mn (a), total Mn (b), reducible Fe (c), and total Fe (d). Reducible Mn and Fe are obtained by chemical extraction with ascorbate at near-neutral pH. This method releases the reactive fractions of oxidized Mn and Fe (Hyacinthe and Van Cappellen, 2004). Also shown are the model distributions of MnO₂A, MnO₂A + MnO₂B (Σ MnO₂), Fe(OH)₃A, and Fe(OH)₃A + Fe(OH)₃B (Σ Fe(OH)₃). Model distributions are depicted as solid lines, extraction data are indicated with (\square) symbols.

time-averaged representation of the important biogeochemical processes taking place in the sediment.

Discrepancies between model calculated and measured concentration profiles may arise from the fact that the system is not at steady state. Especially for the solid-phase constituents (Figs. 5–7), some of the variability in the concentrations reflects historical fluctuations in deposition fluxes. Discrepancies may also result from processes that are not included in the reaction network of the model. For example, the model systematically under-predicts pore water pH and alkalinity at depth in the sediment (Fig. 8). This can be explained by additional buffering by carbonate mineral dissolution, a process which is not included in the model version used here (Jourabchi et al., 2005).

In contrast to the other pore water species, large differences in the depth profiles of dissolved $\rm Mn^{2+}$ and $\rm SO_4^{2-}$ are observed between the individual sampling times (Fig. 8). The elevated pore water $\rm Mn^{2+}$ values in spring could be the result of a temporarily increased input of reactive Mn oxides at the SWI. The model simulation likely under-predicts the rate of manganese reduction for the spring sampling time. The highly variable shape of the $\rm SO_4^{2-}$ profiles also makes it difficult to define an average pore water profile that can be compared to the model calculated depth distribution. Possible reasons for the observed $\rm SO_4^{2-}$ profile shapes are explored in Section 6.4.

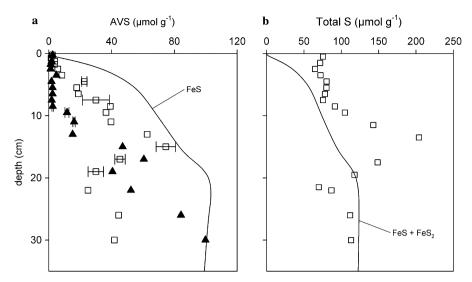


Fig. 7. Acid volatile sulfide (AVS) distributions for late-summer (\square) and spring (\blacktriangle); the solid line represents the modeled FeS concentrations (a). Total sulfur distribution for late-summer (\square), the solid line represents the sum of modeled FeS and FeS₂ concentrations (b). Errors bars are \pm one standard deviations on duplicate or triplicate analyses.

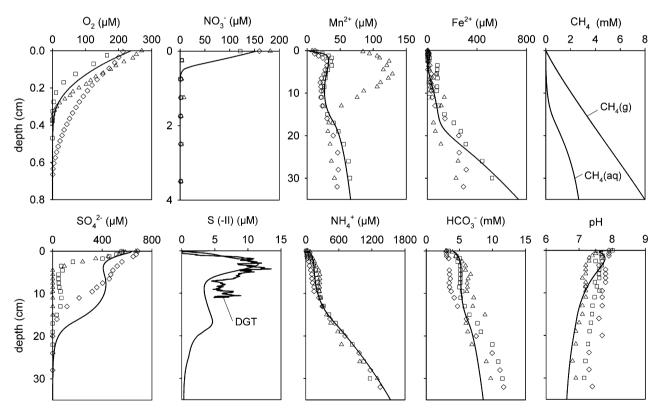


Fig. 8. Pore water profiles for fall (\diamondsuit) , late-summer (\Box) , and spring (\triangle) of dissolved species; solid lines are modeled profiles. The line marked DGT in the S(-II) plot is the AgI DGT derived sulfide profile measured in the upper 10 cm of the sediment. In the HCO_3^- plot, model results correspond to HCO_3^- concentrations, while the data points correspond to measurements of DIC (fall) or alkalinity (late-summer and spring). Note different depth scales in the O_2 and NO_3^- plots.

6.1. Carbon mineralization rates

High rates of organic matter degradation in the upper millimeters of sediment are needed to reproduce the observed O_2 and NO_3^- profiles (Fig. 8). This is achieved by including a highly reactive fraction (OM1) in the deposited

organic matter, but also by explicitly accounting for the enhanced efficiency of O₂ and NO₃⁻ as TEAs of organic carbon oxidation. Together aerobic respiration and denitrification are responsible for about 90% of OM1 degradation (Table 6). In contrast, the most important decomposition pathways for the less reactive organic matter pool,

Table 5
Comparison of maximum model derived rates and experimental rates

Model derived maximum rates		Experimental rates					
Pathway	$(\mu \text{mol cm}^{-3} \text{ yr}^{-1})$	Method	Mean (μmol cm ⁻³ yr ⁻¹)	SD ^a (μmol cm ⁻³ yr ⁻¹)	No. experiments	Depth range (cm)	Date ^b
Oxic respiration	1492	Oxic slurry	1426	704	9	0–20	LS
Denitrification	713	Denitrification FTR	783	547	12	0-4	S, LS, F
Sulfate reduction	25	Sulfate reduction FTR	23	16	8	2-4, 8-10	LS
Anoxic pathways ^c	220	Anoxic slurry	85	86	19	0–20	LS, F

^a Standard deviation.

Table 6
Depth integrated rates of carbon mineralization and secondary redox reactions in the upper 30 cm of sediment

Primary redox reactions					
Reaction	TEA	OM1 (μmol cm ⁻² yr ⁻¹)	OM2 (μmol cm ⁻² yr ⁻¹)	% total	
R1, R7	O_2	422	1.2	55	
R2, R8	NO_3	149	15	21	
R3, R9	Mn(IV)	1.4	0.2	0.2	
R4, R10	Fe(III)	5.1	1.3	0.8	
R5. R11	SO_4	57	74	17	
R6, R12	OM^a	0.0	34	4.4	
R13	OM^a	_	4.3	0.6	
Total		634	130		

Secondary redox reactions

Reaction	Code	μmol cm ⁻² yr ⁻¹	μ mol O ₂ cm ⁻² yr ⁻¹
R14	nh4ox	19	39
R15	tsox	1.5	3.1
R16	fesox	26	51
R17	mnox	0.1	0.05
R18	feox	9.3	2.3
R19	ch4ox	12	12
R20	femnox	1.1	
R21	ch4so4ox	0.1	
R22, R23	tsmnox	0.5	
R24, R25	tsfeox	2.5	

Primary reaction rates are given in units of carbon equivalents, secondary reaction rates refer to the reaction formulas in Table 2. For secondary oxygenation reactions, rates are also expressed as O₂ consumption rates.

OM2, are sulfate reduction, methanogenesis and, to a lesser extent, denitrification. The OM1 pool is nearly completely degraded (99%) in the upper 2 cm of the sediment, while only 39% of OM2 is degraded within the upper 30 cm. Dissimilatory Fe and Mn-oxide reduction do not contribute significantly to total $C_{\rm org}$ mineralization. Limited methane gas formation is predicted to occur in the upper 30 cm of sediment (Table 6).

The total depth-integrated carbon mineralization rate $(764 \, \mu \text{mol cm}^{-2} \, \text{yr}^{-1})$ is at the high end of the range derived by den Heyer and Kalff (1998) from DIC and CH₄ accumulation rates in sediment core incubations of nine lakes in Québec (maximum value for profundal cores: $876 \, \mu \text{mol cm}^{-2} \, \text{yr}^{-1}$). The relatively high rates at our site

reflect the large input of degradable organic matter from the water column, but also the high concentrations of oxygen and nitrate in the bottom waters. Both the modeling results and the direct rate measurements imply order-of-magnitude higher rates of organic carbon degradation by aerobic respiration and denitrification than by the other pathways, in particular sulfate reduction (Table 5). The large contributions of aerobic respiration (55%) and denitrification (21%) to total organic carbon oxidation limit the transfer of potentially degradable organic matter to the deeper sediment. Combined with the relatively high concentration of sulfate in the overlying water, this explains why methanogenesis is not a major pathway of organic matter breakdown at the site studied.

The inferred fraction of total organic carbon oxidation that is due to aerobic respiration (55%) is much larger than found in the model studies by Van Cappellen and Wang (1995) and van den Berg et al. (2000) of freshwater sediments deposited under oxygenated waters. These authors report contributions in the range 3-12%. In these studies, however, only a single degradable organic carbon pool is included (the so-called 1-G model), hence limiting how accurately carbon mineralization with depth can be described. In particular, the 1-G model approach poorly reproduces the presence of a thin surface layer exhibiting much higher rates of carbon mineralization than the underlying sediment. Additionally, van den Berg et al. (2000) note that their modeled CH4 concentrations exceed saturation values, which may have caused an over-estimation of methane oxidation by O2. Using the STEADYQL model Furrer and Wehrli (1996) estimate that 65% of total organic carbon mineralization in sediment of eutrophic Lake Sempach (Switzerland) occurs via aerobic respiration. While this estimate is similar to that obtained here, it should be noted that STEADYQL does not account for secondary oxygenation reactions, and thus overestimates the contribution of oxic respiration.

In Fig. 9, the model predicted depth distribution of the rate of sulfate reduction is compared to rates measured with FTRs and a depth distribution derived from an inverse model optimization (Meile et al., 2001). FTR rate measurements were made with sediment from two different depth intervals (2–4 cm and 8–10 cm) collected in late summer. FTRs yield potential rates, because SO_4^{2-} is the only

^b S, spring; LS, late-summer; F, fall.

^c Anoxic sediment simulated by setting the upper boundary concentration of O₂ and NO₃⁻ to zero.

^a Methanogenesis.

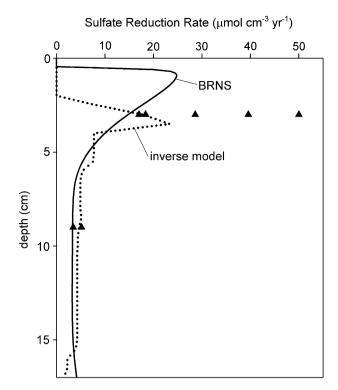


Fig. 9. Sulfate reduction rates in late-summer. The solid line is the rate distribution obtained with the multi-component reaction-transport model (R5+R11) and the dotted line corresponds to the rate distribution obtained by inverse modeling of the sulfate concentration distribution (Meile et al., 2001). Potential sulfate reduction rates measured in FTR experiments for depth intervals 2–4 and 8–9 cm are marked with (\blacktriangle) symbols.

external TEA supplied to the sediment via the inflow during the experiments (Pallud and Van Cappellen, 2006). Potential rates should therefore provide upper estimates of in situ rates. This can be seen for the 2-4 cm sediment interval, where the lowest potential rates approach the model predicted in situ rates. In the 8–10 cm depth interval, potential rates from FTR experiments are close to modeled rates, suggesting that at these depths sulfate reducing activity is mainly limited by the availability of electron donors. This is consistent with the inferred near-complete degradation of the most reactive organic matter (OM1) in the topmost centimeters. Inverse modeling yields the rate of net SO₄²⁻ removal after accounting for diffusion and irrigation. The near-zero values for the net sulfate removal rate in the upper 2 cm reflect the production of sulfate by sulfide oxidation (Section 6.3) in the top sediment. At greater depths, where sulfide oxidation becomes negligible, the inverse model and the reactive transport model predict similar rates.

The results in Fig. 9 suggest that the model-derived sulfate reduction rates are within the correct order of magnitude and approximately reproduce the vertical distribution. Nonetheless, the seasonal variations in the concentration profiles of SO_4^{2-} , but also of other reactive pore water solutes, such as O_2 , NH_4^+ and DIC, serve as a reminder that rates of organic matter degradation in the sediment are

time-dependent. The observed variations in the concentrations of AVS in the zone of most active sulfate reduction (Fig. 7a) further provide evidence that sulfate reduction rates are changing throughout the year (Leonard et al., 1993).

6.2. Secondary reactions

According to the model calculations, secondary oxygenation reactions account for in the order of 20% of total sediment oxygen consumption, mainly through the oxidation of FeS, NH₄⁺, and CH₄(aq) (Table 6). The oxidation of NH₄⁺ and FeS regenerate NO₃⁻ and SO₄²⁻, which in turn help sustain denitrification and sulfate reduction. Abiotic Fe(III) reduction by sulfide (19 μ mol Fe cm⁻² yr⁻¹) and dissimilatory Fe(III) reduction (25 μ mol Fe cm⁻² yr⁻¹) are of comparable magnitude. The oxidation of Fe²⁺ by O₂ (9 μ mol Fe cm⁻² yr⁻¹) exceeds that by MnO₂ (2 μ mol Fe cm⁻² yr⁻¹). Reduction of MnO₂ by Fe²⁺ is responsible for 18% of total manganese reduction. Apart from reaction with Fe²⁺, the cycling of Mn does not play an important role in the major elemental cycles at the site (Table 6).

Methane oxidation is predicted to occur primarily via reaction with O_2 (12 µmol cm⁻² yr⁻¹), with a negligible contribution of anaerobic methane oxidation (0.1 µmol cm⁻² yr⁻¹). Because, in the model, $CH_4(g)$ generated in the sediment is assumed to be non-reactive, the calculated rate of methane oxidation represents a conservative estimate. The potential error introduced by neglecting the possible redissolution of gaseous methane in the surface sediment, followed by oxidation, is assessed by running a simulation where all methanogenesis yields $CH_4(aq)$ production. This nearly doubles the methane oxidation rate, from 12 to 22 µmol cm⁻² yr⁻¹. The increased methane oxidation rate still has little impact on total oxygen consumption, as the O_2 consumption due to methane oxidation rises from 2 to 4%.

6.3. Fe-S cycling

Iron and sulfur cycling are linked in the reaction network through the formation of FeS and FeS₂, reaction of sulfide with Fe-oxides, and the oxidation of FeS (Fig. 10). Most of the Fe²⁺ and S(-II) produced in the sediment forms FeS. Although sulfate reduction is quantitatively a far more important electron sink than iron reduction, the amounts of S(-II) and Fe²⁺ produced are relatively similar due to the 8-fold difference in reaction stoichiometry (Fig. 10 and Table 2). Because of efficient sulfur recycling, the depth-integrated sulfate reduction rate equals nearly twice the ${\rm SO_4}^{2-}$ influx at the SWI.

Only about 10% of the FeS produced in the sediment is converted into pyrite. According to the model calculations, FeS represents the main burial sink for reactive iron and sulfur (Fig. 10). The simulation, however, tends to overestimate the AVS concentrations (Fig. 7a), implying that the FeS sink could be somewhat lower than indicated on

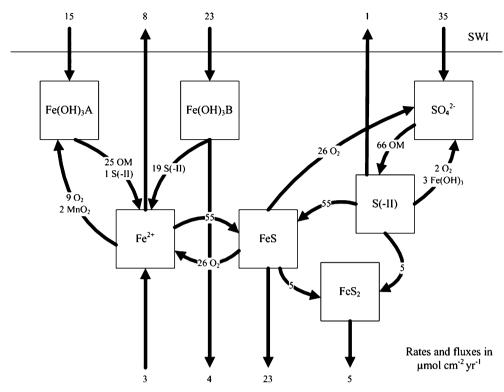


Fig. 10. The Fe–S cycle as simulated by the multi-component model. All rate and flux values are presented in units of μ mol cm⁻² yr⁻¹, and rounded to the nearest whole number. Rate values are integrated over the upper 30 cm of sediment. Transport fluxes are indicated at the beginning or ends of the arrows. Values on the arrows are reaction rates; for redox reactions the oxidant or reductant is identified to the right of the rate values. Note that rate values are presented for the reaction stoichiometries listed in Table 2. Fe(OH)₃A is the bioavailable Fe-oxide pool, the Fe(OH)₃B pool is only reduced chemically by sulfide.

Fig. 10. Nonetheless, authigenically formed iron sulfides may account for most solid-phase sulfur in the deeper sediment (Fig. 7b). Excess sulfur in the surface sediment may represent particulate sulfur pools not included in the model, such as organically bound S and elemental S.

Both the chemical extraction data and the model calculations indicate that substantial amounts of reactive Fe(III) are buried below 30 cm (Figs. 6 and 10). As reported in a number of studies, a fraction of the chemically reducible Fe(III) mineral phases is unavailable for microbial respiration (e.g., Wersin et al., 1991; Berg et al., 2003; Hyacinthe and Van Cappellen, 2004). One important biogeochemical consequence of future seawater intrusion in Haringvliet Lake could be the enhanced reductive dissolution of this Fe(III) pool by sulfide generated by sulfate reduction (Section 6.5).

6.4. Transport—bioirrigation and bioturbation

Diffusion and non-local transport (bioirrigation) are both important modes of solute transport in the upper 15 cm of sediment. Bioirrigation increases the fluxes of O_2 , NO_3^- , and SO_4^{2-} into the sediment (Table 7), causing more $C_{\rm org}$ mineralization to be coupled to the soluble TEAs. Overall, increased influx of O_2 and enhanced removal of reduced solutes by bioirrigation (Table 7) decreases the fraction of total O_2 consumption due to secondary

Table 7
Rates of solute exchange by diffusion and bioirrigation at the SWI

	0,	C	
Solute	Diffusion (μmol cm ⁻² yr ⁻¹)	Bioirrigation (μmol cm ⁻² yr ⁻¹)	Contribution of bioirrigation (%)
O_2	-500	-31	6
NO_3^-	-92	-20	18
$NO_3^ Mn^{2+}$	4	2	36
SO_4^{2-}	-5	-30	86
CH ₄ (aq)	0	19	100
NH_4^+	91	27	23
HCO ₃ -	104	165	62

Negative values denote fluxes into sediment.

redox reactions. In a simulation where all bioirrigation coefficients are set to zero, the contribution of secondary redox reactions to total O_2 consumption increases from 19% to 24%. In the same simulation, methanogenesis increases from 5% to 15% of total $C_{\rm org}$ decomposition.

Recent work has cautioned against the use of a single depth distribution of the irrigation coefficient for all pore water solutes (Aller, 2001; Berg et al., 2003; Grigg et al., 2005; Meile et al., 2005). Following the suggestions of Berg et al. (2003) and Meile et al. (2005), we therefore reduced the α values for Fe²⁺ and Mn²⁺, relative to those of the conservative ions Na⁺ and Cl⁻ (Section 4.2). Note that although the model assumes that aqueous Fe²⁺ is not subject to transport by irrigation ($\alpha = 0$), the Fe²⁺ profile is

affected by the enhanced pore water mixing (Fig. 8). The lack of significant build-up of pore water Fe²⁺ in the upper 15 cm is due in part to the enhanced downward transport of oxygenated bottom water, fueling oxidation of Fe²⁺ in the irrigated zone.

To some degree, the irrigation coefficients of all reactive solute species should deviate from those of conservative tracers (Meile et al., 2005). This could be particularly important for SO_4^{2-} , whose supply from the water column is strongly affected by irrigation (Table 7). According to Meile et al. (2005), SO_4^{2-} exhibits lower than average irrigation coefficients. This could help explain the mismatch between measured and computed SO_4^{2-} profiles. The sensitivity of the SO₄²⁻ pore water distribution to the irrigation intensity is illustrated in Fig. 11a. As can be seen, reducing the irrigation coefficient of $SO_4^{\ 2-}$ yields pore water profiles that more closely resemble those observed during spring and late summer. The fall data, however, suggests a possible enhancement of the irrigation intensity. Uncertainties in the transport properties of the pore water solutes directly affect the estimated reaction rates. For instance, reductions of α_0 for SO_4^{2-} by 50% and 100% cause the calculated integrated rate of sulfate reduction to decrease by 6.1% and 32%, respectively.

Changes in the particle mixing regime also affect the rates of primary and secondary redox reactions. Some of the effects are examined by changing the value of $D_{\rm b}0$ in the equation for the biodiffusion coefficient distribution listed in Table 4. The reactive iron and sulfur species are particularly sensitive to the degree of sediment mixing (Figs. 11b and c). Increasing $D_{\rm b}0$ increases sulfate removal from the pore waters (Fig. 11b), as the highly reactive organic matter (OM1) is transported deeper into the sediment where it is utilized by sulfate reduction. Lowering

 D_b0 has the opposite effects on the SO_4^{2-} concentrations and sulfate reduction rates. In the low mixing simulation ($D_b0=1~\rm cm^2~\rm yr^{-1}$), a significant build-up of reactive Fe(III) precipitates is observed in the upper 5 cm of the sediment, causing the appearance of a subsurface concentration maximum (Fig. 11c). Such an accumulation of Fe(III) oxides at the oxic–suboxic interface has been observed in lake sediments, and may increase the importance of dissimilatory iron reduction (Thomsen et al., 2004).

6.5. Estuarine restoration

The model is used to examine potential changes in benthic biogeochemistry that could result from the restoration of estuarine conditions at our study site. In particular, we examine how the primary and secondary redox reaction dynamics would respond to changes in bottom water chemistry, deposition of organic matter and the bioturbation regime. The sensitivity to these changes is initially assessed using steady state solutions of the model (Table 8). Then, a transient simulation is performed to illustrate the time scales over which sediment biogeochemistry is expected to respond to a switch from lacustrine to estuarine conditions (Fig. 12).

Some of the environmental forcings that will change upon the (regulated) intrusion of seawater in the Haringv-liet are predictable, while others are more speculative. For instance, water column salinization will undoubtedly increase the SO_4^{2-} concentration at the SWI. However, while increased salinity stratification is expected to result in lower bottom water O_2 concentrations, it is not known to what extent O_2 may be depleted. The same is true for the OM deposition fluxes, which are likely to decrease, as increased exchange of water with the adjacent coastal zone will

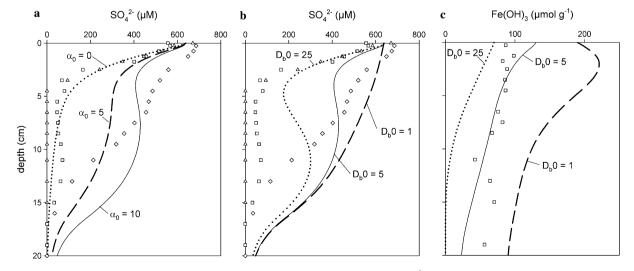


Fig. 11. Model sensitivity to bioirrigation is shown with the concentration distribution of SO_4^{2-} (a) where the solid line is the baseline simulation $(\alpha_0 = 10 \text{ yr}^{-1})$, the dashed line is with $\alpha_0 = 5 \text{ yr}^{-1}$, and the dotted line is with $\alpha_0 = 0 \text{ yr}^{-1}$. Model sensitivity to the particle mixing intensity (D_b0) is shown using the concentration distributions of SO_4^{2-} (b) and $\Sigma Fe(OH)_3$ (c). The dotted lines correspond to simulations with $D_b0 = 25 \text{ cm}^2 \text{ yr}^{-1}$, the solid lines with $D_b0 = 5 \text{ cm}^2 \text{ yr}^{-1}$ and the dashed lines with $D_b0 = 1 \text{ cm}^2 \text{ yr}^{-1}$. Field data are presented with the following symbols: fall (\diamondsuit) , late-summer (\Box) , and spring (\triangle) .

Table 8
Responses of sediment biogeochemistry to possible changes in site conditions resulting from estuarine restoration

Scenario ^a	Oxic respiration (µmol cm ⁻² yr ⁻¹)	Sulfate reduction $(\mu mol cm^{-2} yr^{-1})$	FeS oxidation $(\mu \text{mol cm}^{-2} \text{ yr}^{-1})$	Fe-oxide reduction by sulfide $(\mu mol cm^{-2} yr^{-1})$
Existing conditions	423	131	26	2.5
$+SO_4^{2-}$	421	170	32	3.0
$+SO_4^{2-}, -O_2$	327	209	26	3.3
$+SO_4^{2-}, -OM$	271	24	1.3	0.2
$+SO_4^{2-}, +D_b0$	348	239	43	3.8
$+SO_4^{2-}, +\lambda$	414	177	35	3.0
$+SO_4^{2-}, -O_2, -OM, +D_b0, +\lambda$	155	90	25	0.9

The depth-integrated rates are derived from steady-state model simulations.

^a +SO₄²⁻, SWI concentration increased to 10 mM; -O₂, SWI concentration decreased to 120 μM; -OM, input flux of OM1 and OM2 reduced by 50%; +D_bO, value at SWI increased to 25 cm² yr⁻¹ (increased mixing intensity); $+\lambda$, value increased to 5 cm (increased mixing depth).

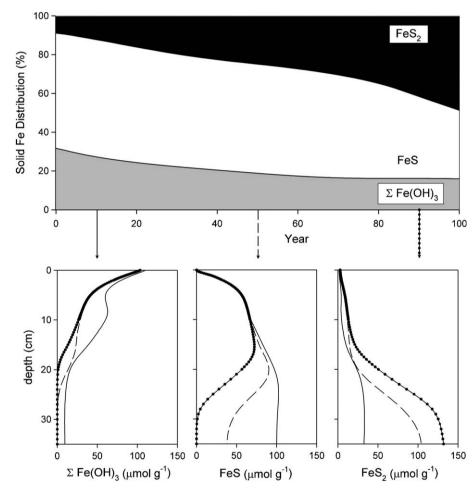


Fig. 12. Transient simulation of solid-phase iron speciation in the sediment following an increase in the bottom water SO_4^{2-} concentration from 0.6 to 10 mM. The upper plot displays the concentrations of the Σ Fe(OH)₃, FeS, and FeS₂ pools, integrated over the upper 30 cm of sediment. The lower plots show the depth profiles of the three solid Fe pools for simulation times of 10 years (solid line), 50 years (dashed line), and 90 years (dotted line).

enhance the export of nutrients and particulate matter from the Haringvliet.

Increasing the sulfate concentration at the SWI to 10 mM from the current 0.6 mM, effectively suppresses methanogenesis in the upper 30 cm of sediment. The increase in sulfate reduction rate with higher SO_4^{2-} availability is further enhanced by lowering the O_2 concentration in the overlying water (Table 8). Nevertheless, the

relative increases in the rate of sulfate reduction are relatively small, given the large imposed changes in bottom water chemistry. This reflects the overall limitation of sediment respiration by the supply of degradable organic matter. Hence, a reduction of the OM influx by 50% causes a drop in the sulfate reduction rate by nearly an order of magnitude, even when the SO_4^{2-} concentration in the bottom water is maintained at 10 mM (Table 8). Under these

conditions, the relative contributions of aerobic respiration and denitrification to total $C_{\rm org}$ degradation increase at the expense of that of sulfate reduction. The lower input of OM also results in a reduced redox cycling of Fe and S in the sediment (Wijsman et al., 2002), as illustrated by the much lower rates of FeS oxidation and Fe(III) oxide reduction by sulfide (Table 8).

The current benthic fauna in the Haringvliet can be characterized as poor (Smit et al., 1997). Restoration of estuarine conditions is expected to increase the density and diversity of the macroinvertebrate community in the downstream portion of the Haringvliet. Most likely this will intensify and deepen bioturbation of the sediment. In the model simulations, bioturbation was modified by either increasing the value of D_b0 , which controls the intensity of mixing, or by extending the depth of mixing by increasing the depth attenuation parameter, λ . Enhanced mixing promotes sulfate reduction over aerobic degradation (Table 8), as reactive OM is mixed below the oxygen penetration depth (see also Section 6.4). The rates of FeS oxidation and Fe-oxide reduction by sulfide also increase with greater mixing, as the latter intensifies the exchanges between the oxidized and reduced portions of the sediment. Overall, increasing D_b0 has a greater impact on sediment biogeochemistry than increasing the mixing depth.

The simulation results in Table 8 illustrate the broad range of responses that can be expected upon estuarine restoration. To use the model for environmental forecasting thus depends critically on accurately constraining future changes in benthic forcing functions. An important aspect of the model is its ability to simulate the coupled effects of multiple environmental changes. This is illustrated by the last scenario in Table 8, which combines the various postulated changes in bottom water chemistry, OM deposition and bioturbation regime. This scenario results in lower mineralization rates, due to the decrease in OM input (Table 8). However, the integrated rates of sulfate reduction, FeS oxidation, and sulfide oxidation of Fe-oxides are greater in the combined scenario than expected when only the OM input is reduced, because of the counteracting effect of enhanced mixing.

The results summarized in Table 8 provide no information on the time required for the benthic system to adjust to changing environmental conditions. The temporal response of sediment processes to salinization is addressed with a transient simulation using the steady-state model solution for the present conditions as initial condition. As a perturbation, we impose an instantaneous increase of the SO_4^{2-} concentration at the SWI from 0.6 to 10 mM, while all other conditions are kept the same. This perturbation is selected, because estuarine restoration will definitely lead to a significant increase of the SO_4^{2-} levels in the bottom water at the site.

The transient calculations indicate that increased SO_4^{2-} availability at the SWI allows sulfate reduction to immediately suppress methanogenesis in the upper 30 cm of sediment (results not shown). The integrated rates of organic

matter degradation by O_2 , NO_3^- , and $SO_4^{\ 2-}$ adjust to their new steady state values within the first few years. The enhanced production of sulfide by sulfate reduction also leads to further transformation of reactive Fe(III) oxides to iron sulfides. However, the changes in solid-phase Fe speciation require time scales of several decades and more (Fig. 12). During the first 50 years of the simulation the reactive Fe-oxide concentrations in the sediment decline, while those of pyrite increase. After the reactive Fe(III) oxide content reaches its new steady state, conversion of FeS to pyrite continues, gradually increasing the amount of pyrite accumulating in the sediment. As shown by Fig. 12, the conversion of FeS to FeS2 is still ongoing 100 years after the imposed increase in SO_4^{2-} concentration at the SWI. Thus, the simulation results imply that the changes in sediment biogeochemistry caused by the planned restoration of estuarine conditions may occur over a wide range of temporal scales. In particular, the predicted changes in solid-state Fe speciation may have long-term consequences for the biogeochemical cycling of phosphorus (Caraco et al., 1990; Gunnars and Blomqvist, 1997) and trace metals (Huerta-Diaz et al., 1998) in the Haringvliet.

7. Conclusions

Interpretation of chemical sediment and pore water data with a reaction transport model allows us to quantify the rates of primary and secondary redox reactions in sediment of the coastal Haringvliet Lake. The model simultaneously reproduces the depth-dependent trends of multiple constituents, providing strong evidence that it captures the essence of the important reaction and transport processes taking place at the site.

Oxic degradation and denitrification occur at high rates in a shallow zone near the sediment–water interface, and oxidize most (76%) of the degradable organic carbon input. Below this zone, sulfate reduction and methanogenesis are the dominant primary reaction pathways, but proceed at much slower rates due to lower reactivity of $C_{\rm org}$ and less efficient degradation under anoxic conditions. Secondary redox reactions account for only 20% of the total O_2 consumption, which contrasts with many other eutrophic lakes where methanogenesis is the dominant degradation pathway. Dissimilatory Mn(IV) and Fe(III) reduction are not important pathways of $C_{\rm org}$ decomposition, despite the presence of chemically reducible Mn and Fe mineral phases.

Bioirrigation and bioturbation have a major impact on primary and secondary reaction rates and chemical distributions, emphasizing the link between biogeochemical cycling and the activity of benthic fauna. Better representations and parameterizations of biologically mediated transport processes in reactive transport models remain crucial for improving our quantitative understanding of sediment biogeochemical processes.

Model simulations illustrate the wide range of potential consequences of estuarine restoration for sediment

biogeochemistry. The results imply that, as a result of increased concentrations of sulfate in the bottom water, sulfate reduction will rapidly suppress methanogenesis at the site studied. Other changes in benthic biogeochemical dynamics, however, will depend on how the production and deposition of degradable organic matter respond to the restoration of estuarine conditions. In addition, the establishment of a new benthic infaunal community adapted to the increased salinity will most likely modify the transport regime and, hence, the biogeochemical cycling in the sediments.

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