## CE3620: Water Resources Engineering Practice Final Exam

These are questions which are representative of things you may see on the final exam. Please note that you are also strongly advised to look at the sample problems posted for Exams I and II, as well as Exams I and II themselves, and be sure that you understand the homework problems assigned throughout the semester. THE EXAM WILL BE CUMULATIVE!

On the actual exam, remember to show all calculations to ensure that you receive as much partial credit as possible. If short on time, you may also summarize the solution procedure for partial credit (if correct and reasonably well explained). If you feel that not enough information is given, then assume something, clearly state your assumption(s), and proceed to solve the problem.

You will be given 2 hours to complete the exam. The exam will be closed book, but you may bring TWO crib sheets. Each sheet is to be an 8.5 " x 11 " sheet of paper. Each sheet can be two sided, but must contain handwritten material!! You will also be provided with the formula sheet at the end of this document.

## Problem 1

Given: A highway bridge is designed to just pass a discharge with an annual exceedance probability of 0.020 without overtopping the roadway.

Find: Compute the probability that the bridge will be overtopped at least once during the next 10 years.

Answer: 0.183

## Problem 2

Given: A stream bed has a rectangular cross section 5 meters wide and a slope of $.0002 \mathrm{~m} / \mathrm{m}$. The flow rate in the stream is $8.75 \mathrm{~m}^{3} / \mathrm{s}$. A dam is built across the stream, causing the water surface to rise to 2.5 meters just upstream of the dam, as shown below.
Assume $n=.015$.


Find: (a) Find the normal depth, $y_{\mathrm{n}}$, corresponding to this flow rate and channel geometry.
Ans. $\mathrm{y}_{\mathrm{n}}=1.8 \mathrm{~m}$
(b) Find the critical depth, $y_{\mathrm{c}}$.

Ans. $\mathrm{y}_{\mathrm{c}}=0.678 \mathrm{~m}$
(c) Identify the water surface profile upstream of the dam. Explain your answer for full credit.

Ans. M1 profile.
(d) Briefly explain (or list the steps) how you would compute the water surface profile (depth vs. distance along the channel).

Ans. Discuss steps of Direct-Step method.

## Problem 3

Given: An upstream hydrograph is shown below in Figure 1.


Figure 1. Upstream (inflow) hydrograph.

Find: Route the upstream hydrograph to a location downstream using the Muskingum method with $K=0.4 \mathrm{hr}, X=0.2$, and $\Delta t=0.5 \mathrm{hr}$. Assume that the initial flow downstream is zero. You only need to compute the first three ordinates of the downstream hydrograph (from time 0 to $3 \Delta t$ ).

## Answer:

| Time <br> (hrs) | Inflow <br> (cfs) | Outflow <br> (cfs) |
| :---: | :---: | :---: |
| 0 | 0 | 0 |
| 0.5 | 100 | 29.8 |
| 1.0 | 200 | 121.2 |
| 1.5 | 300 | 220.1 |

## Problem 4

Given: The outflow rate (cfs) and storage (cfs-hr) for an emergency spillway of a certain reservoir are linearly related by $O=S / 3$, where the number 3 has units of hours.

Find: Use storage-outflow relationship $O=S / 3$ and the continuity equation

$$
S_{t+1}+\frac{O_{t+1} \Delta t}{2}=\frac{\left(I_{t}+I_{t+1}\right) \Delta t}{2}+S_{t}-\frac{O_{t} \Delta t}{2}
$$

to determine the peak outflow rate from the reservoir for the following event:

| Time <br> $(\mathrm{hr})$ | $I$ <br> $(\mathrm{cfs})$ | $S$ <br> $(c f s-h r)$ | $O$ <br> $(\mathrm{cfs})$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 |
| 2 | 400 |  |  |
| 4 | 600 |  |  |
| 6 | 200 |  |  |
| 8 | 0 |  |  |

Answer: Peak outflow is 350 cfs.

| Time <br> $(\mathrm{hr})$ | $I$ <br> $(\mathrm{cfs})$ | $S$ <br> $(\mathrm{cfs}-\mathrm{hr})$ | $O$ <br> $(\mathrm{cfs})$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 |
| 2 | 400 | $\mathbf{3 0 0}$ | $\mathbf{1 0 0}$ |
| 4 | 600 | $\mathbf{9 0 0}$ | $\mathbf{3 0 0}$ |
| 6 | 200 | $\mathbf{1 0 5 0}$ | $\mathbf{3 5 0}$ |
| 8 | 0 | $\mathbf{6 7 5}$ | $\mathbf{2 2 5}$ |

## Problem 5

Given: A 400-acre watershed is to be developed into an industrial district with an estimated NRCS Curve Number of 90 . The distance from the watershed divide to the outlet is 3800 ft , and the average watershed slope is $75 \mathrm{ft} / \mathrm{mile}(0.0142 \mathrm{ft} / \mathrm{ft})$.

Find: (a) Compute the hourly runoff depth from a 2-hour, 4-inch rainfall event assuming the rainfall occurs at a uniform rate ( $2 \mathrm{in} / \mathrm{hr}$ for 2 hrs ).

Ans.

| Time <br> (hrs) | $\Delta \mathrm{V}_{\mathrm{R}}$ <br> (in) |
| :---: | :---: |
| 0 | 0 |
| 1 | 1.09 |
| 2 | 1.83 |

(b) Compute basin lag time $t_{L}$ (hours), time to peak $T_{P}$, and the peak unit hydrograph discharge $Q_{P}\left(\mathrm{ft}^{3} / \mathrm{s}\right)$, and sketch the 1-hr NRCS triangular unit hydrograph for the watershed.

Ans. $t_{L}=0.545 \mathrm{hrs} ; T_{P}=1.045 \mathrm{hrs} ; Q_{P}=289.5 \mathrm{cfs} ; T_{\mathrm{B}}=2.79 \mathrm{hrs}$

(c) Estimate the peak discharge ( $\mathrm{ft}^{3} / \mathrm{s}$ ) from the 4 -inch rainfall event assuming that the rainfall occurs uniformly over a 2-hour period ( $2.0 \mathrm{in} / \mathrm{hr}$ ). Use a 1-hour time interval for your calculations.

Ans.

| Time <br> $(\mathrm{hrs})$ | UH Flow <br> $(\mathrm{cfs})$ | Excess Precipitation (in) |  | 1.09 |
| :---: | :---: | :---: | :---: | :---: | | Runoff |
| :---: |
| $(\mathrm{cfs})$ |

(d) Based on the attached rainfall intensity-duration-frequency curve, what is the return period of this 2-hour storm?

Ans. T = 10 years


## EQUATIONS AND CONVERSION FACTORS

| $\sum F_{x}=\beta \rho Q\left(V_{2}-V_{1}\right)$ | $\frac{P_{1}}{\gamma}+z_{1}+\frac{\alpha V_{1}^{2}}{2 g}+E_{p}=\frac{P_{2}}{\gamma}+z_{2}+\frac{\alpha V}{2 g}$ | $H_{L}+H_{M}$ |
| :---: | :---: | :---: |
| $Q=N_{p} A \sqrt{\frac{2 g H_{L}}{K_{e n}+K_{f}+1}}$ | $Q=N_{p} A_{e} C_{o} \sqrt{2 g(H-D / 2)}$ | $x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}$ |
| $Q=V A$ | $\mathrm{y}_{1}+\mathrm{z}_{1}+\frac{\mathrm{V}_{1}^{2}}{2 \mathrm{~g}}=\mathrm{y}_{2}+\mathrm{z}_{2}+\frac{\mathrm{V}_{2}^{2}}{2 \mathrm{~g}}+\mathrm{H}_{\mathrm{L}}$ | $Q=\frac{C_{m}}{n} A R^{2 / 3} S_{o}^{1 / 2}$ |
| $F r=\frac{V}{\sqrt{g D}}$ | $\frac{d E}{d y}=1-\frac{Q^{2}}{g A^{3}} \frac{d A}{d y}$ | $\frac{d y}{d x}=\frac{S_{o}-S_{f}}{1-F r^{2}}$ |
| $\mathrm{y}_{2}=\frac{\mathrm{y}_{1}}{2}\left(-1+\sqrt{1+8 \mathrm{Fr}_{1}^{2}}\right)$ | $\mathrm{P}_{\text {water }}=\gamma \mathrm{QE}_{\mathrm{p}}$ | $\mathrm{P}_{\text {shaft }}=\mathrm{P}_{\text {water }} / \eta$ |
| $H_{L}=f \frac{L}{D} \frac{V^{2}}{2 g}$ | $H_{M}=K \frac{V^{2}}{2 g}$ | $H_{L}=\frac{n^{2} V^{2} L}{C_{m}^{2} R^{4 / 3}}$ |
| $A=y(B+S S y)$ | $\mathrm{P}=\mathrm{B}+2 \mathrm{y} \sqrt{1+\mathrm{SS}^{2}}$ | $\mathrm{T}=\mathrm{B}+2 \mathrm{ySS}$ |
| $\mathrm{A}=\mathrm{By}$ | $\mathrm{P}=\mathrm{B}+2 \mathrm{y}$ | $\mathrm{D}=\mathrm{A} / \mathrm{T}$ |
| $\mathrm{R}=\mathrm{A} / \mathrm{P}$ | $Q=C i A$ | $i=\frac{a}{(t+b)^{c}}$ |
| $T_{P}=D / 2+t_{L}$ | $T_{B}=5 T_{p}$ | $T_{B}=2.667 T_{p}$ |
| $Q_{P}=484 A / T_{P}$ | $Q_{P}=2.08 A / T_{P}$ |  |
| $t_{L}=\frac{l^{0.8}(1000-9 C N)^{0.7}}{1900 C N^{0.7} Y^{0.5}}$ | $t_{L}=\frac{l^{0.8}(2540-22.86 C N)^{0.7}}{1410 C N^{0.7} Y^{0.5}}$ | $t_{C}=\frac{5}{3} t_{L}$ |
| $V_{R}=\frac{(P-0.2 S)^{2}}{P+0.8 S}$ | $S=\frac{2540}{C N}-25.4$ | $S=\frac{1000}{C N}-10$ |
| $\mathrm{I}_{\mathrm{A}}=0.2 \mathrm{~S}$ | $\mathrm{R}=1-(1-\mathrm{P})^{\mathrm{N}}$ | $\mathrm{T}=1 / \mathrm{P}$ |
| $S=K[X I+(1-X) O]$ | $\mathrm{O}_{\mathrm{t}+1}=\mathrm{C}_{1} \mathrm{I}_{\mathrm{t}+1}+\mathrm{C}_{2} \mathrm{I}_{\mathrm{t}}+\mathrm{C}_{3} \mathrm{O}_{\mathrm{t}}$ | $\frac{d S}{d t}=I-O$ |
| $C_{1}=\frac{0.5 \Delta t-K X}{K-K X+0.5 \Delta t}$ | $C_{2}=\frac{0.5 \Delta t+K X}{K-K X+0.5 \Delta t}$ | $C_{3}=\frac{K-K X-0.5 \Delta t}{K-K X+0.5 \Delta t}$ |
| $1 \mathrm{mile}=5280 \mathrm{ft}$ | 1 inch $=2.54 \mathrm{~cm}$ | $1 \mathrm{ft}^{3}=7.48$ gallons |
| 1 acre $=43,560 \mathrm{ft}^{2}$ | $1 \mathrm{mi}^{2}=640$ acres |  |
| $g=32.2 \mathrm{ft} / \mathrm{s}^{2}=9.81 \mathrm{~m} / \mathrm{s}^{2}$ | $\gamma=62.4 \mathrm{lb} / \mathrm{ft}^{3}=9.79 \mathrm{kN} / \mathrm{m}^{3}$ |  |

